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Executive Vice President  
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January 30, 2004

Ernest Johnson  
Director, Utilities Division  
ARIZONA CORPORATION COMMISSION  
1200 West Washington Street  
Phoenix, Arizona 85007

**HAND DELIVERED**

Arizona Corporation Commission  
**DOCKETED**

JAN 30 2004

DOCKETED BY	
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**RE: 10-Year Plan And Related Studies**  
**Docket No. E-00000D-03-0047**

Dear Mr. Johnson:

In compliance with A.R.S. § 40-360.02 and pursuant to Arizona Corporation Commission (“Commission”) Decision Nos. 63876 (July 25, 2001) and 65154 (September 10, 2002), enclosed please find Arizona Public Service Company’s (“APS” or “Company”) 2004-2013 Ten-Year Plan for major transmission facilities, along with associated system studies, system ratings, and also the Company’s Reliability Must Run Report for 2004-2013.

The 2004-2013 Ten-Year Plan describes planned transmission lines of 115 kV or higher that APS may construct over the next 10 years. This Ten-Year Plan includes approximately 205 miles of new 500 kV transmission lines, 194 miles of new 230 kV transmission lines, and 14 new bulk transformers. The total investment needed to construct these projects is currently estimated to exceed \$1.1 billion. When completed, these projects are expected to add approximately 2,000 MW of additional Extra-High Voltage scheduling capability, as well as 2,500 MW of import capability into the Metropolitan Phoenix Area and 250 MW of import capability into Yuma.

These new transmission projects, coupled with additional distribution and sub-transmission investments, will support reliable power delivery in both APS’ service area and in the Western United States. However, the Ten-Year Plan, as well as other APS reliability-related infrastructure investments, is premised on a number of assumptions concerning the Company’s future financial condition, the regulatory treatment of such investments by the Commission and the Federal Energy Regulatory Commission, other state and federal policies affecting transmission, and, of course, APS’ ability to finance large investments of this nature on commercially-reasonable terms.

Ernest Johnson  
January 30, 2004  
Page 2

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Please contact me if you have any questions or desire additional information concerning this filing.

Sincerely,



Steven M. Wheeler

SMW:DN

Enclosures

cc/encl: Docket Control (Original, plus 13 copies)

Commissioner Marc Spitzer, Chairman

Commissioner Bill Mundell

Commissioner Jeff Hatch-Miller

Commissioner Mike Gleason

Commissioner Kristin Mayes

Laurie Woodall, Assistant Attorney General

**ARIZONA PUBLIC SERVICE COMPANY**  
**2004–2013**  
**TEN-YEAR PLAN**

Prepared for the  
**Arizona Corporation Commission**



January 2004

**ARIZONA PUBLIC SERVICE COMPANY  
2004 - 2013  
TEN-YEAR PLAN**

**CONTENTS**

<u>GENERAL INFORMATION</u> .....	1
----------------------------------	---

**PLANNED TRANSMISSION MAPS**

Arizona EHV and Outer Divisions .....	6
Phoenix Metropolitan (West) area.....	7
Phoenix Metropolitan (East) area .....	8

**PLANNED TRANSMISSION DESCRIPTIONS**

Gavilan Peak loop-in of Pinnacle Peak-Prescott 230-kV line (2005) .....	9
Rudd-TS3-TS4 230-kV line (2006) .....	10
Flagstaff 345/69-kV Interconnection (2006) .....	11
Hassayampa-Jojoba-Pinal West 500-kV line (2006).....	12
Pinal West-Santa Rosa-Browning 500-kV line (2007 & 2011).....	13
Palo Verde-TS5 500-kV line (2007) .....	14
TS5-TS1 230-kV line (2007) .....	15
TS3-TS2-TS1 230-kV line (2008) .....	16
Raceway-Avery 230-kV line (2008).....	17
Pinnacle Peak-TS6-Avery 230-kV lines (2009).....	18
Second Knoll loop-in of Coronado-Silver King 500-kV line (2009).....	19
Raceway loop-in of Navajo-Westwing 500-kV line (2010) .....	20

TS5-Raceway 500-kV line (2010) .....	21
Westwing-Raceway 230-kV line (2010) .....	22
Gila Bend-TS8 230-kV line (2012) .....	23
Westwing-El Sol 230-kV line (2013).....	24
Mazatzal loop-in of Cholla-Pinnacle Peak 345-kV line (TBD) .....	25
Palo Verde-Pinal West-Saguaro 500-kV line (TBD).....	26

**ARIZONA PUBLIC SERVICE COMPANY**  
**2004–2013**  
**TEN-YEAR PLAN**

**GENERAL INFORMATION**

Pursuant to A.R.S. § 40-360.02, Arizona Public Service Company (“APS”) submits its 2004-2013 Ten-Year Plan. Additionally, pursuant to Arizona Corporation Commission (“Commission”) Decision No. 63876 (July 25, 2001) concerning the first Biennial Transmission Assessment, APS is including with this filing its Transmission Planning Process and Guidelines and maps showing system ratings on APS’ transmission system. The Transmission Planning Process and Guidelines outline generally APS’ internal planning for its high voltage and extra-high voltage transmission system, including a discussion of APS’ planning methodology, planning assumptions, and its guidelines for system performance. The system ratings maps show emergency and continuous system ratings on APS’ extra-high voltage system, and on its Metro, Northern, and Southern 230 kV systems.

This 2004–2013 Ten-Year Plan describes planned transmission lines of 115 kV or higher voltage that APS may construct over the next ten-year period. Pursuant to A.R.S. § 40-360(10), underground facilities are not included. There are approximately 205 miles of 500-kV transmission line, 194 miles of 230-kV transmission line, and 14 bulk transformers contained in the projects in this Ten-Year Plan filing. The total investment for the projects, as they are modeled in this filing, is estimated to be in excess of \$1.115 billion and the projects will add 2000 MW of additional EHV scheduling capability, 2500 MW of import capability into the Phoenix area, and 247 MW of import capability into the Yuma area. The following table shows a breakdown of the projects contained in this Ten-Year Plan.

	<u>Projects in Ten-Year Plan</u>
<b>500-kV transmission line</b>	205 miles
<b>230-kV transmission line</b>	194 miles
<b>Bulk Transformers</b>	14
<b>Total Investment</b>	\$1.115 billion
<b>EHV Scheduling Capability</b>	+2000 MW (+20 %) <sup>1</sup>
<b>Total Phoenix Area Import</b>	+2500 MW (+29 %) <sup>1</sup>
<b>Yuma Area Import</b>	+247 MW (+151 %) <sup>1</sup>

<sup>1</sup> Based on 2003 values.

Also, previously reported facilities that have been completed, canceled, or deferred beyond the upcoming ten-year period are not included. This Ten-Year Plan is tentative information only and, pursuant to A.R.S. § 40-360.02(F), is subject to change without notice at the discretion of APS, based on land usage, growth pattern changes, regulatory or legal developments, or for other reasons. A summary of changes from last year's plan is provided below.

For the convenience of the reader, APS has included system maps showing the general location and in-service date for all overhead transmission lines planned by APS for Arizona and the Phoenix Metropolitan Area. Written descriptions of each proposed transmission line are provided on subsequent pages in the currently expected chronological order of each project. The line routings shown on the system maps and the descriptions of each transmission line are intended to be general and are subject to revision. Specific routing is determined by the Arizona Power Plant and Transmission Line Siting Committee when issuing a Certificate of Environmental Compatibility and through subsequent right-of-way acquisition. Pursuant to the amendments to A.R.S. § 40-360.02, this filing also includes technical study results for the projects identified. The technical study results show project needs which are generally based on either security (contingency performance) or adequacy (generator interconnection or increasing transfer capability) or both.

APS believes that the projects identified in this 2004-2013 Ten-Year Plan, with their associated in-service dates, will ensure that APS' transmission system meets all applicable reliability criteria. However, changes in regulatory requirements or underlying assumptions such as load forecasts, generation expansion, financial condition, and other utilities' plans, may substantially impact this Ten-Year Plan and could result in changes to anticipated in-service dates or project scopes. Additionally, the future formation and role of the WestConnect Regional Transmission Organization (RTO), or other federal and regional mandates, may impact this Ten-Year Plan and the transmission planning process generally.

#### **Changes From 2003-2012 Ten-Year Plan**

The following is a list of projects that were changed or removed from the Ten Year plan filed last year, along with a brief description of why the change was made.

- **Projects removed from plan**

The Buckeye loop-in of Gila Bend-Liberty 230-kV line is no longer in the plan, along with the Silver King loop-in of Cholla-Saguaro 500-kV and the Gila Bend-Pinal West 230-kV line. It was determined that the objectives of these projects can be met by other system additions.

Along with those projects the Rudd loop-in of the Jojoba-Kyrene 500-kV line is no longer in the plan. It was determined that this project would reduce system performance and the Phoenix area import capability. The technical study can be referenced in the Technical Study Report which is also part of this filing.

- **Table Mesa replaced by Raceway**

The Table Mesa substation has been replaced by a 500-kV substation at Raceway with a 500/230-kV transformer. The Navajo-Westwing 500-kV line

will be looped-in to Raceway instead of Table Mesa and the loop-in will be delayed from 2009 to 2010. The TS5-Table Mesa 500-kV line will now be TS5-Raceway 500-kV. Also, because of the replacement of Table Mesa with Raceway the Table Mesa-Raceway 230-kV lines and the Table Mesa loop-in of Gavilan Peak-Prescott 230-kV line have been deleted.

- South East Valley Project

The project has changed to include a Santa Rosa substation with a 500/230-kV transformer. As a result, the Pinal West-Santa Rosa 230-kV line has been deleted. The Pinal West-Santa Rosa-SEV portion has been delayed from 2006 to 2007.

- Northern Area Interconnections

The Flagstaff loop-in of Cholla-Coconino 230-kV line has been replaced with a 345/69-kV interconnection at the WAPA Flagstaff substation.

The Cholla-Second Knoll 230-kV line has been replaced with a 500/69-kV interconnection of SRP's Coronado-Silver King 500-kV line into Second Knoll.

These changes result in interconnections that are more cost-effective and a better use of the existing transmission system.

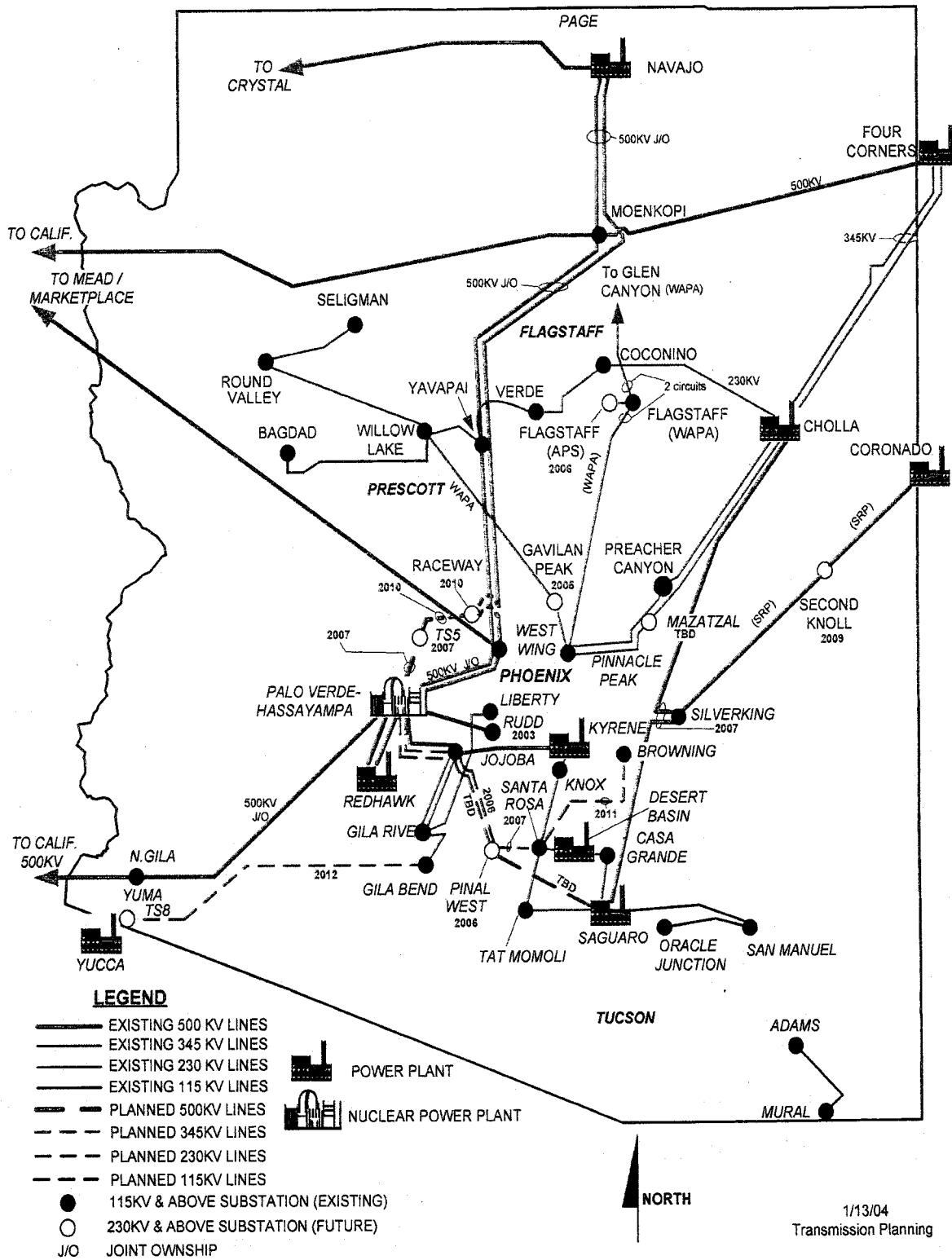
- Timing Changes and Name Changes

The Gavilan Peak loop-in of the Pinnacle Peak-Prescott 230-kV line has been delayed from 2004 to 2005. The West Valley South Project will now terminate at the TS4 substation instead of the Liberty substation. The Palo Verde-TS5 500-kV line has been advanced from 2008 to 2007. Trilby Wash is now named TS1 and the TS5-TS1 230-kV portion of West Valley North has been advanced from 2008 to 2007. The proposed 230-kV substation in Yuma will be named TS8 and the Gila Bend-TS8 230-kV line has been delayed from 2010 to 2012. Also, the name

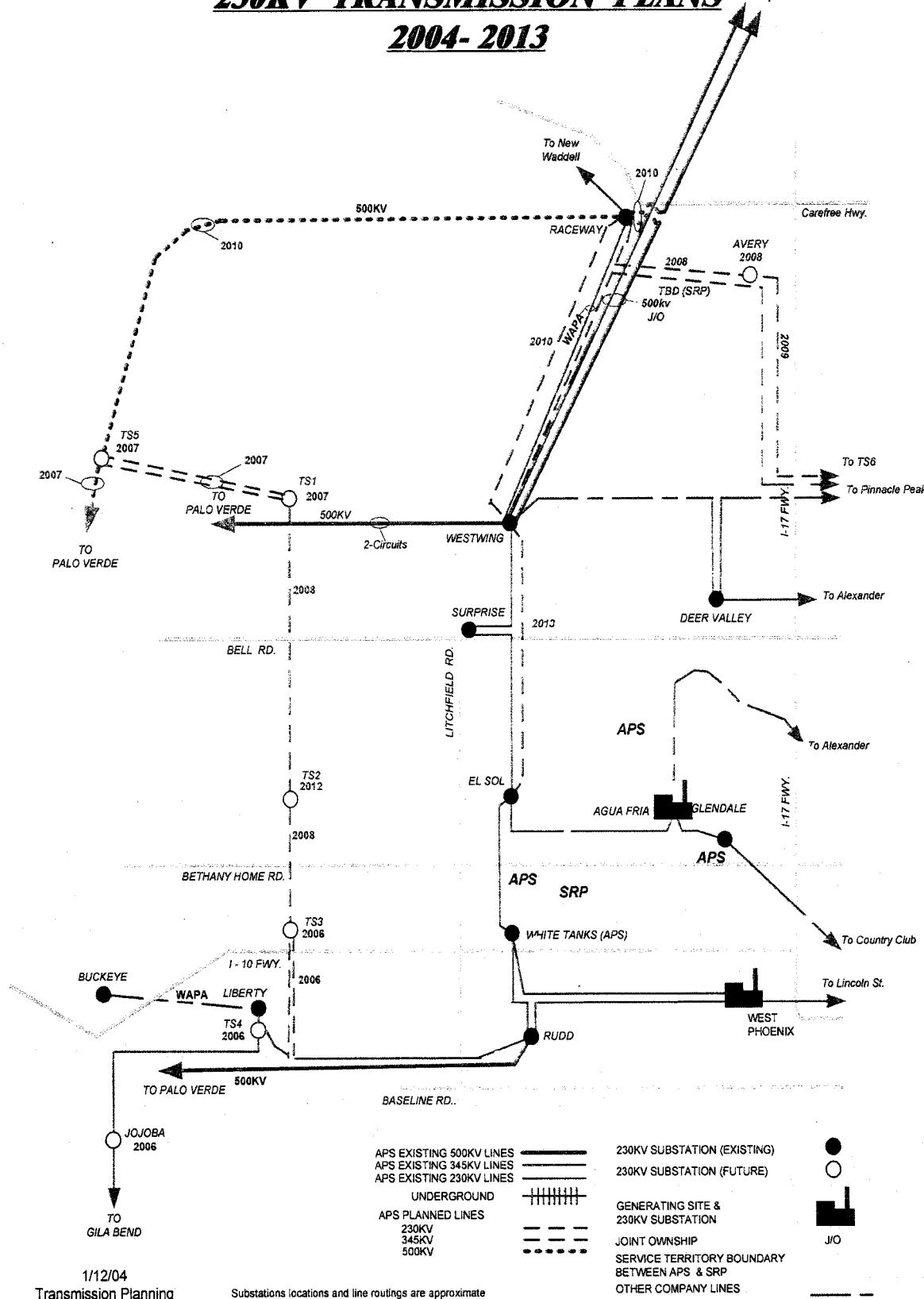
of the proposed Misty Willow 230-kV substation has changed to TS6. The Westwing-El Sol 230-kV line has been delayed from 2012 to 2013.

# APS EHV & OUTER DIVISION 115/230 KV

## TRANSMISSION PLANS 2004 - 2013



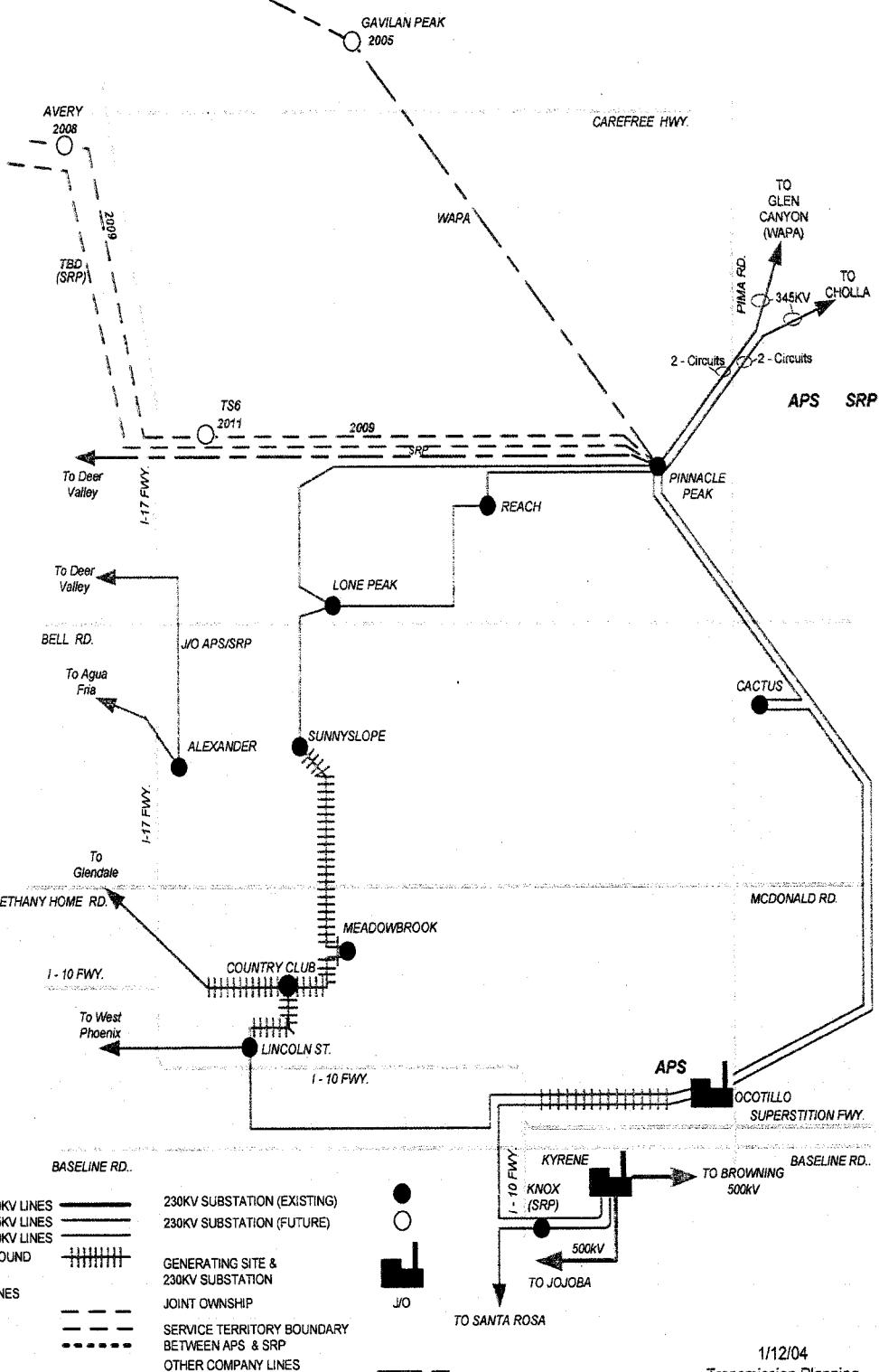
**PHOENIX METROPOLITAN (WEST) AREA**  
**230KV TRANSMISSION PLANS** To Navajo  
**2004- 2013**



# PHOENIX METROPOLITAN (EAST) AREA

## 230KV TRANSMISSION PLANS

2004- 2013



1/12/04  
Transmission Planning

**Arizona Public Service Company  
2004 —2013  
Ten-Year Plan**

**Planned Transmission Description  
2005**

Line Designation Gavilan Peak loop-in of Pinnacle Peak-Prescott 230-kV line.

Size

- (a) Voltage 230-kV AC.
- (b) Capacity 150MW
- (c) Point of Origin Pinnacle Peak-Prescott 230-kV line near 12<sup>th</sup> Street and Desert Hills Drive; Sec. 28, T6N, R3E.
- (d) Intermediate Point None.
- (e) Point of Termination Gavilan Peak 230/69-kV substation to be built in 2005, 1/4 mile south of the intersection of 12<sup>th</sup> Street and Desert Hills Drive; within the northeast quarter of Sec. 28, T6N, R3E.
- (f) Length Approximately 1 span each of two single-circuit lines.

Routing

Gavilan Peak 230-kV substation will be adjacent to the Pinnacle Peak-Prescott 230-kV line so it will just be one or two spans.

Purpose

This substation will be needed to serve projected need for electric energy in the area immediately north of the Phoenix Metropolitan area. Additionally, improved reliability and continuity of service will result for the growing communities in the areas of Desert Hills, Anthem, and New River.

Date

- (a) Construction Start 2003
- (b) Estimated In Service 2005

*A Certificate of Environmental Compatibility is not needed for this project.*

**Arizona Public Service Company**  
**2004 —2013**  
**Ten-Year Plan**  
**Planned Transmission Description**  
**2006**

<u>Line Designation</u>	Rudd – TS3 – TS4 230-kV line.
<u>Size</u>	
(a) Voltage	230-kV AC.
(b) Capacity	1200 MVA.
(c) Point of Origin	Rudd-Liberty 230-kV transmission line near the intersection of Broadway Road and Perryville Road; within Sec. 28, T1N, R1W.
(d) Intermediate Point	TS3 230/69-kV substation to be constructed in 2006 near the corner of Camelback Rd. and Cotton Ln.; Sec. 24, T2N, R2W.
(e) Point of Termination	A new TS4 230kV substation located just south of the WAPA Liberty substation, Sec. 19, T1N, R2W.
(f) Length	Approximately 7 miles of double-circuit 230-kV.
<u>Routing</u>	North and east from the existing Rudd-Liberty 230-kV transmission line approximately 7 miles to the TS3 substation and returning south and west to the existing line. Then the termination of the line will be moved from the Liberty substation to the TS4 substation.
<u>Purpose</u>	This 230-kV line will provide a source for the TS3 230/69-kV substation and 69-kV substations planned in the western and southwestern Phoenix Metropolitan area. Increased reliability and quality of service will result for customers served by the 230/69-kV substation.
<u>Date</u>	
(a) Construction Start	2002 (The component that was already certificated in Case No. 115, Decision No. 64473, Rudd-Liberty was in-service for the summer of 2003.) Construction for the double-circuit to TS3 will start in 2004.
(b) Estimated In Service	2006

*Certificate of Environmental Compatibility issued 2/12/02 (Case No. 115, Decision No. 64473, Southwest Valley Project). Revised on 4/9/02, Decision No. 64704. This CEC is for the 230-kV line, Rudd-Liberty, running east and west on the same poles as the Palo Verde-Rudd 500-kV line. Certificate of Environmental Compatibility issued 12/24/03 (Case No. 122, Decision No. 66646, West Valley South Project). This CEC is for the 230-kV component running from the existing Rudd-Liberty line to the TS3 substation and for the TS4 substation.*

**Arizona Public Service Company  
2004 —2013  
Ten-Year Plan**

**Planned Transmission Description  
2006**

<u>Line Designation</u>	345/69-kV interconnection at WAPA's Flagstaff 345-kV bus.
<u>Size</u>	
(a) Voltage	345-kV AC.
(b) Capacity	150 MW.
(c) Point of Origin	WAPA's Flagstaff 345-kV substation; Sec. 24, T21N, R9E.
(d) Intermediate Point	None.
(e) Point of Termination	A new 69-kV substation to be built in 2006 adjacent to WAPA's Flagstaff substation; Sec. 24, T21N, R9E.
(f) Length	Approximately 1 span.
<u>Routing</u>	A 345/69-kV transformer will interconnect into WAPA's Flagstaff substation.
<u>Purpose</u>	This substation will serve projected need for electric energy in the APS' northern service area. The project will improved reliability and continuity of service for the growing communities in northern Arizona.
<u>Date</u>	
(a) Construction Start	2004
(b) Estimated In Service	2006

*A Certificate of Environmental Compatibility is not needed for this project.*

**Arizona Public Service Company**  
**2004 —2013**  
**Ten-Year Plan**

**Planned Transmission Description**  
**2006**

<u>Line Designation</u>	Hassayampa – Jojoba – Pinal West 500-kV line.
<u>Size</u>	
(a) Voltage	525-kV AC.
(b) Capacity	To be determined.
(c) Point of Origin	Hassayampa substation or another nearby 500-kV substation; Sec. 3, T1S, R6W.
(d) Intermediate Point	Jojoba 500-kV substation; Sec. 25, T2S, R4W.
(e) Point of Termination	Pinal West 500/345-kV substation to be constructed in 2006, in the vicinity of the town of Mobile; Sec. 18, T5S, R2E
(f) Length	Approximately 60 miles of single-circuit 500-kV
<u>Routing</u>	South and east from Hassayampa, following the existing 500-kV line to Jojoba, then continuing on to the proposed Pinal West 500-kV substation in the vicinity of the town of Mobile.
<u>Purpose</u>	This project is a result of the CATS study. When combined with the rest of the Southeast Valley project the line will increase import capability to the Phoenix Metropolitan area as well as increase the export capability from the Palo Verde/Hassayampa area. It is anticipated the line will be a joint participation project with SRP as the project manager.
<u>Date</u>	
(a) Construction Start	2005
(b) Estimated In Service	2006

*An application for a Certificate of Environmental Compatibility was filed by SRP on 12/16/03, Case No. 124.*

**Arizona Public Service Company  
2004 —2013  
Ten-Year Plan**

**Planned Transmission Description  
2007**

<u>Line Designation</u>	Pinal West – Santa Rosa – Browning 500-kV line.
<u>Size</u>	
(a) Voltage	525-kV AC.
(b) Capacity	To be determined.
(c) Point of Origin	Pinal West 500/345-kV substation to be constructed in 2006, in the vicinity of the town of Mobile; Sec. 18, T5S, R2E
(d) Intermediate Point	Santa Rosa 500-kV substation to be constructed in 2007 near the existing Santa Rosa 230-kV substation; Sec. 30, T5S, R4E.
(e) Point of Termination	Browning 500/230-kV substation; Sec. 12, T1S, R8E.
(f) Length	Approximately 60 miles of single-circuit 500-kV
<u>Routing</u>	South and east from Pinal West to the Santa Rosa 500-kV substation. Then east and north to the Browning 500/230-kV substation.
<u>Purpose</u>	This project is a result of the CATS study. The line will increase import capability to the Phoenix Metropolitan area as well as increase the export capability from the Palo Verde/Hassayampa area. It is anticipated the line will be a joint participation project with SRP as the project manager.
<u>Date</u>	
(a) Construction Start	2005
(b) Estimated In Service	Pinal West-Santa Rosa in 2007. Santa Rosa-Browning in 2011

*An application for a Certificate of Environmental Compatibility has not yet been filed.*

**Arizona Public Service Company  
2004—2013  
Ten-Year Plan**

**Planned Transmission Description  
2007**

<u>Line Designation</u>	Palo Verde-TS5 500-kV line.
<u>Size</u>	
(a) Voltage	525-kV AC.
(b) Capacity	To be determined.
(c) Point of Origin	Palo Verde Power Plant or nearby 500-kV substation.
(d) Intermediate Point	None.
(e) Point of Termination	TS5 500/230-kV substation to be constructed in 2007. Location to be determined, approximately in the north Buckeye/Sun Valley area.
(f) Length	Approximately 45 miles of single-circuit line.
<u>Routing</u>	Generally north from Palo Verde/Hassayampa for approximately 45 miles.
<u>Purpose</u>	This line will serve projected need for electric energy in the area immediately north and west of the Phoenix Metropolitan area. It will increase the import capability to the Phoenix Metropolitan area as well as increase the export capability from the Palo Verde/Hassayampa area.
<u>Date</u>	
(a) Construction Start	2006
(b) Estimated In Service	2007

*An application for a Certificate of Environmental Compatibility is expected to be filed during 2004.*

**Arizona Public Service Company**  
**2004 — 2013**  
**Ten-Year Plan**

**Planned Transmission Description**  
**2007**

<u>Line Designation</u>	TS5-TS1 230-kV line.
<u>Size</u>	
(a) Voltage	230-kV AC.
(b) Capacity	To be determined.
(c) Point of Origin	TS5 500/230-kV substation to be constructed in 2007. Location to be determined, approximately in the north Buckeye/Sun Valley area.
(d) Intermediate Point	None.
(e) Point of Termination	TS1 230/69-kV substation to be constructed in 2007 approximately 11 miles west of Westwing substation; Sec. 23, T4N, R2W.
(f) Length	Approximately 15 miles of single-circuit line.
<u>Routing</u>	East from TS5 substation to TS1 substation for approximately 15 miles.
<u>Purpose</u>	This line is required to serve the increasing need for electric energy in the western Phoenix Metropolitan area, providing more capability to import power into the Phoenix Metropolitan area along with improved reliability and continuity of service for growing communities such as El Mirage, Surprise, and Youngtown.
<u>Date</u>	
(a) Construction Start	2006
(b) Estimated In Service	2007

*The TS5-TS1 230-kV line will be sited as part of the West Valley North project. An application for the Certificate of Environmental Compatibility for the West Valley North project is planned for 2004.*

**Arizona Public Service Company  
2004 — 2013  
Ten-Year Plan**

**Planned Transmission Description  
2008**

<u>Line Designation</u>	TS3-TS2-TS1 230-kV line.
<u>Size</u>	
(a) Voltage	230-kV AC.
(b) Capacity	To be determined.
(c) Point of Origin	TS3 230/69-kV substation to be constructed in 2006 near the corner of Camelback Rd. and Cotton Ln.; Sec. 24, T2N, R2W.
(d) Intermediate Point	TS2 230/69-kV substation to be constructed in 2012; Sec. 25, T3N, R2W.
(e) Point of Termination	TS1 230/69-kV substation to be constructed in 2007 approximately 11 miles west of Westwing substation; Sec. 23, T4N, R2W.
(f) Length	Approximately 12 miles of single-circuit line.
<u>Routing</u>	North from the TS3 substation, generally following the Loop 303, to the TS1 substation passing the location of the future TS2 substation which is currently projected to be in-service in 2012.
<u>Purpose</u>	This line is required to serve the increasing need for electric energy in the western Phoenix Metropolitan area, providing more capability to import power into the Phoenix Metropolitan area along with improved reliability and continuity of service for growing communities such as El Mirage, Surprise, and Youngtown.
<u>Date</u>	
(a) Construction Start	2007
(b) Estimated In Service	2008

*The TS3-TS2 230-kV line portion was sited as part of the West Valley South project and a Certificate of Environmental Compatibility was issued 12/24/03 (Case No. 122, Decision No. 66646). The TS1-TS2 230-kV line portion will be sited as part of the West Valley North project. An application for the Certificate of Environmental Compatibility for the West Valley North project is planned for 2004.*

**Arizona Public Service Company  
2004—2013  
Ten-Year Plan**

**Planned Transmission Description  
2008**

<u>Line Designation</u>	Raceway-Avery 230-kV line.
<u>Size</u>	
(a) Voltage	230-kV AC.
(b) Capacity	1200 MVA.
(c) Point of Origin	Raceway substation located along the Westwing-New Waddell 230-kV line, approximately 3 miles south of the New Waddell Dam; Sec. 4, T5N, R1E.
(d) Intermediate Point	None.
(e) Point of Termination	A new Avery substation near Dove Valley Road and 39 <sup>th</sup> Avenue; Sec. 10, T5N, R2E.
(f) Length	Approximately 10 miles of double-circuit line.
<u>Routing</u>	South from Raceway substation approximately 1 mile, paralleling existing transmission lines, then east approximately 9 miles to the new Avery substation.
<u>Purpose</u>	This line will serve projected need for electric energy in the area immediately north of the Phoenix Metropolitan area. Additionally, improved reliability and continuity of service will result for the area's growing communities such as Anthem, Desert Hills and New River.
<u>Date</u>	
(a) Construction Start	2004
(b) Estimated In Service	2008

*Certificate of Environmental Compatibility issued 6/18/03 (Case No. 120, Decision No. 64473, North Valley Project).*

**Arizona Public Service Company  
2004 —2013  
Ten-Year Plan**

**Planned Transmission Description  
2009**

<u>Line Designation</u>	Pinnacle Peak-TS6-Avery 230-kV lines.
<u>Size</u>	
(a) Voltage	230-kV AC.
(b) Capacity	1200 MVA.
(c) Point of Origin	Pinnacle Peak substation; Sec. 25, T4N, R3E.
(d) Intermediate Point	TS6 substation to be constructed in 2011; Sec. 12, T4N, R3E.
(e) Point of Termination	Avery substation near Dove Valley Road and 39 <sup>th</sup> Avenue; Sec. 10, T5N, R2E.
(f) Length	Approximately 16 miles of double-circuit line.
<u>Routing</u>	Along the existing 230-kV right-of-way, west 10 miles from Pinnacle Peak substation to approximately Interstate 17, generally parallel to and south of Happy Valley Road; then north 5 miles, generally parallel to Interstate 17, to Dove Valley Road, then west to the new Avery substation.
<u>Purpose</u>	These lines will serve projected need for electric energy in the area immediately north of the Phoenix Metropolitan area. Additionally, improved reliability and continuity of service will result for the growing communities in the areas of Anthem, Desert Hills, and New River.
<u>Date</u>	
(a) Construction Start	2004
(b) Estimated In Service	2009

*Certificate of Environmental Compatibility issued 6/18/03 (Case No. 120, Decision No. 64473, North Valley Project).*

**Arizona Public Service Company  
2004—2013  
Ten-Year Plan**

**Planned Transmission Description  
2009**

Line Designation Second Knoll loop-in of Coronado-Silver King 500-kV line.

Size

- (a) Voltage 525-kV AC.
- (b) Capacity To be determined.
- (c) Point of Origin Coronado-Silver King 500-kV line; T15N, R20E.
- (d) Intermediate Point None.
- (e) Point of Termination Second Knoll 500/69-kV substation to be built in 2009; T15N, R20E.
- (f) Length Only 1 span of single-circuit line.

Routing

The Second Knoll substation will be built adjacent to the Coronado-Silver King 500-kV line, therefore limiting the distance to 1 or 2 spans.

Purpose

This line will be needed to serve projected need for electric energy in Show Low and the surrounding communities.

Date

- (a) Construction Start 2008
- (b) Estimated In Service 2009

*A Certificate of Environmental Compatibility is not needed for this project.*

**Arizona Public Service Company  
2004 —2013  
Ten-Year Plan**

**Planned Transmission Description  
2010**

Line Designation

Raceway loop-in of Navajo-Westwing 500-kV line.

Size

- (a) Voltage 525-kV AC.
- (b) Capacity To be determined.
- (c) Point of Origin Navajo-Westwing 500-kV line; Sec. 4, T5N, R1E.
- (d) Intermediate Point Raceway 500-kV substation to be constructed in 2010 adjacent to the Navajo-Westwing 500-kV line and approximately 1 mile from the existing Raceway 230kV substation; Sec. 4, T5N, R1E.
- (e) Point of Termination Raceway 230-kV substation; Sec. 4, T5N, R1E.
- (f) Length One span of double-circuit 500-kV line from the Navajo-Westwing 500-kV line to the Raceway 500-kV substation. Approximately 1 mile of double-circuit 230-kV lines to the Raceway 230-kV substation.

Routing

Navajo-Westwing 500-kV line will be adjacent to the Raceway 500-kV substation. From the 500/230-kV transformers at the Raceway 500-kV substation, 230-kV lines would run south to the Raceway 230-kV substation.

Purpose

The loop-in of Raceway 500-kV line will be needed to provide contingency support to Raceway, increase system reliability, and increase the import capability to the Phoenix Metropolitan area.

Date

- (a) Construction Start 2009
- (b) Estimated In Service 2010

*An application for a Certificate of Environmental Compatibility has not yet been filed.*

**Arizona Public Service Company  
2004—2013  
Ten-Year Plan**

**Planned Transmission Description  
2010**

<u>Line Designation</u>	TS5 – Raceway 500-kV line.
<u>Size</u>	
(a) Voltage	525-kV AC.
(b) Capacity	To be determined.
(c) Point of Origin	TS5 500/230-kV substation to be constructed in 2007. Location to be determined, approximately in the north Buckeye/Sun Valley area.
(d) Intermediate Point	None.
(e) Point of Termination	Raceway 500-kV substation to be constructed in 2010 adjacent to the Navajo-Westwing 500-kV line and approximately 1 mile from the existing Raceway 230kV substation; Sec. 4, T5N, R1E.
(f) Length	Approximately 40 miles of single-circuit line.
<u>Routing</u>	North from TS5 substation and then in a northeasterly direction to the Raceway substation.
<u>Purpose</u>	This line will be needed to serve projected need for electric energy in the area immediately north and west of the Phoenix Metropolitan area. It will increase the import capability to the Phoenix Metropolitan area as well as increase the export capability from the Palo Verde/Hassayampa area.
<u>Date</u>	
(a) Construction Start	2008
(b) Estimated In Service	2010

*An application for a Certificate of Environmental Compatibility has not yet been filed.*

**Arizona Public Service Company  
2004 —2013  
Ten-Year Plan**

**Planned Transmission Description  
2010**

<u>Line Designation</u>	Westwing – Raceway 230kV Line.
<u>Size</u>	
(a) Voltage	230-kV AC.
(b) Capacity	1200 MVA.
(c) Point of Origin	Westwing substation; Sec 12, T4N, R1W.
(d) Intermediate Point	None.
(e) Point of Termination	Raceway substation located along the Westwing-New Waddell 230-kV line, approximately 3 miles south of the Waddell Dam; Sec. 4, T5N, R1E.
(f) Length	Approximately 7 miles of line on double-circuit poles.
<u>Routing</u>	Northeast from Westwing substation paralleling existing transmission lines to the Raceway substation which will be adjacent to the existing transmission lines.
<u>Purpose</u>	The 230-kV line will serve increasing loads in the far north and northwest parts of the Phoenix Metropolitan area and provide contingency support for multiple Westwing 500/230-kV transformer outages.
<u>Date</u>	
(a) Construction Start	2007
(b) Estimated In Service	2010

*Certificate of Environmental Compatibility issued 6/18/03 (Case No. 120, Decision No. 64473, North Valley Project).*

**Arizona Public Service Company**  
**2004 —2013**  
**Ten-Year Plan**

**Planned Transmission Description**  
**2012**

<u>Line Designation</u>	Gila Bend-TS8 230-kV line.
<u>Size</u>	
(a) Voltage	230-kV AC.
(b) Capacity	To be determined.
(c) Point of Origin	Gila Bend substation; Sec. 36, T2N, R1W.
(d) Intermediate Point	None.
(e) Point of Termination	TS8 230-kV substation to be built in or near Yuma, Arizona
(f) Length	Approximately 115 mile of single-circuit line.
<u>Routing</u>	West from Gila Bend to Yuma, generally parallel to Interstate 8.
<u>Purpose</u>	As a new transmission path to Yuma area, this 230-kV line will provide transmission capacity required to supplement limited transmission and generation resources in the Yuma area. This 230-kV line will also provide another source for the Gila Bend area.
<u>Date</u>	
(a) Construction Start	2010
(b) Estimated In Service	2012

*An application for a Certificate of Environmental Compatibility has not yet been filed.*

**Arizona Public Service Company**  
**2004—2013**  
**Ten-Year Plan**

**Planned Transmission Description**  
**2013**

<u>Line Designation</u>	Westwing-El Sol 230-kV line.
<u>Size</u>	
(a) Voltage	230-kV AC.
(b) Capacity	1200 MVA.
(c) Point of Origin	Westwing substation; Sec. 12, T4N, R1W.
(d) Intermediate Point	None.
(e) Point of Termination	El Sol substation; Sec. 30, T3N, R1E.
(f) Length	Approximately 11 miles of single-circuit line.
<u>Routing</u>	
<u>Purpose</u>	This line will increase system capacity to serve growing demand for electric energy in the Phoenix Metropolitan area, while maintaining system reliability and integrity for delivery of bulk power from Westwing south into the APS Phoenix Metropolitan area 230-kV transmission system.
<u>Date</u>	
(a) Construction Start	2012
(b) Estimated In Service	2013

*Certificate of Environmental Compatibility issued 7/26/73 (Case No. 9, docket No. U-1345). Note that this Certificate authorizes two double-circuit lines. Construction of the first double-circuit line was completed in March 1975. Construction of the second line, planned to be built with double-circuit capability but initially operated with a single circuit, is described above.*

**Arizona Public Service Company**  
**2004 —2013**  
**Ten-Year Plan**

**Planned Transmission Description**  
**TBD**

<u>Line Designation</u>	Mazatzal loop-in of Cholla-Pinnacle Peak 345-kV line.
<u>Size</u>	
(a) Voltage	345-kV AC.
(b) Capacity	To be determined.
(c) Point of Origin	Cholla-Pinnacle Peak 345-kV line; near Sec. 3, T8N, R10E.
(d) Intermediate Point	None.
(e) Point of Termination	Mazatzal 345/69-kV substation; approximately Sec. 3, T8N, R10E.
(f) Length	Approximately 1 span each of two single-circuit lines.
<u>Routing</u>	The Mazatzal substation will be built adjacent to the Cholla-Pinnacle Peak 345-kV line so it will be just one or two spans.
<u>Purpose</u>	This substation will serve projected need for electric energy in the area of Payson and the surrounding communities. Additionally, improved reliability and continuity of service will result for the growing communities in the Payson area.
<u>Date</u>	
(a) Construction Start	TBD
(b) Estimated In Service	TBD

*A Certificate of Environmental Compatibility is not needed for this project.*

**Arizona Public Service Company  
2004—2013  
Ten-Year Plan**

**Planned Transmission Description  
TBD**

Line Designation      Palo Verde - Pinal West - Saguaro 500-kV line.

Size

- (a) Voltage      525-kV AC.
- (b) Capacity      To be determined.
- (c) Point of Origin      Palo Verde Power Plant; Sec. 34, T1N, R6W.
- (d) Intermediate Point      Pinal West substation in the Casa Grande area. Hassayampa and Jojoba substations are also possible interconnection points.
- (e) Point of Termination      Saguaro substation; Sec. 14, T10S, R10E.
- (f) Length      Approximately 130 miles of new line to be built on single-circuit poles or towers. Some sections may be built on double-circuit structures.

Routing

South and east from the Palo Verde switchyard, paralleling existing transmission lines for part of the route. The approved corridor is defined in the CEC identified below.

Purpose

This line is the result of the joint participation CATS study. The line will be needed to increase the adequacy of the existing EHV transmission system and permit increased power delivery throughout the state. It is anticipated the line will be a joint participation project.

Date

- (a) Construction Start      TBD
- (b) Estimated In Service      TBD

*Certificate of Environmental Compatibility issued 01/23/1976 (Case No. 24, Decision No. 46802).*



*A subsidiary of Pinnacle West Capital Corporation*

# **TRANSMISSION PLANNING PROCESS AND GUIDELINES**

**APS Transmission Planning  
January 2004**

## **TRANSMISSION PLANNING PROCESS AND GUIDELINES**

I.	INTRODUCTION .....	1
II.	PLANNING METHODOLOGY	
A.	General.....	1
B.	230kV Long Range System .....	2
C.	Ten Year System Expansion Plans .....	3
D.	Facilities Keyed to Generation/Resource Additions.....	4
E.	Generation Schedules.....	4
F.	Study Period.....	5
G.	Regional Coordination Planning	
1.	Western Electricity Coordinating Council.....	5
2.	Joint Studies.....	6
H.	Load Projections .....	6
I.	Alternative Evaluations	
1.	General.....	6
2.	Power Flow Analyses .....	6
3.	Transient Stability Studies .....	7
4.	Short Circuit Studies.....	7
5.	Losses Analyses .....	7
6.	Transfer Capability Studies.....	7
7.	Subsynchronous Resonance (SSR).....	7
8.	Economic Evaluation .....	7

### **III. PLANNING ASSUMPTIONS**

#### **A. General**

1. Loads.....	8
2. Generation and Other Resources .....	8
3. Nominal Voltage Levels .....	8
4. Source of Data Bases .....	8
5. Voltage Control Devices.....	8
6. Phase Shifters.....	8
7. Conductor Sizes .....	8
8. 69kV System Modeling .....	9
9. Substation Transformers .....	9
10. Switchyard Arrangements	

a. 500kV & 345kV Substations .....	10
b. 230kV Substations .....	11

11. Series Capacitor Application .....	11
12. Shunt and Tertiary Reactor Application .....	11

#### **B. Power Flow Studies**

1. System Stressing .....	11
2. Displacement.....	12

#### **C. Transient Stability Studies**

1. Fault Simulation.....	12
2. Margin.....	12
3. Unit Tripping .....	12
4. Machine Reactance Representation .....	12
5. Fault Damping .....	12
6. Series Capacitor Switching.....	12

#### **D. Short Circuit Studies**

1. Generation Representation.....	13
2. Machine Reactance Representation .....	13
3. Line Representation .....	13
4. Transformer Representation.....	13

## **IV. SYSTEM PERFORMANCE**

### **A. Power Flow Studies**

1. Normal (Base Case Conditions)	
a. Voltage Levels	
1) General.....	13
2) Specific Buses.....	14
b. Facilities Loading Limits	
1) Transmission Lines .....	14
2) Underground Cable.....	14
3) Transformers.....	14
4) Series Capacitors.....	14
c. Interchange of VARs .....	14
d. Distribution of Flow.....	15
2. Single Contingency Outages	
a. Voltage Levels .....	15
b. Facilities Loading Limits	
1) Transmission Lines .....	15
2) Underground Cable.....	15
3) Transformers.....	15
4) Series Capacitors.....	15
c. Generator Units.....	15
d. Impact on Interconnected Systems .....	15
B. Transient Stability Studies	
1. Fault Simulation.....	16
2. Series Capacitor Switching.....	16
3. System Stability .....	16
4. Reclosing.....	16
C. Short Circuit Studies.....	16

## **I. INTRODUCTION AND PURPOSE**

The Transmission Planning Process and Guidelines (Guidelines) are used by Arizona Public Service Company (APS) to assist in planning its Extra High Voltage (EHV) transmission system (345kV and above) and High Voltage transmission system (230kV and 115kV). In addition to these Guidelines, APS follows the Western Electricity Coordinating Council's (WECC) regional planning reliability criteria for system disturbance and performance levels. These WECC Reliability Criteria, which can be found in their entirety on the WECC website, are (1) WECC/NERC Reliability Criteria for Transmission System Planning ([http://www.wecc.biz/WECC-NERC\\_Planning%20Standards\\_9-18-02.pdf](http://www.wecc.biz/WECC-NERC_Planning%20Standards_9-18-02.pdf)) and (2) Minimum Operating Reliability Criteria ([http://www.wecc.biz/MORC\\_Pages\\_9-02.pdf](http://www.wecc.biz/MORC_Pages_9-02.pdf)). These Guidelines are for internal use by APS and may be changed or modified at any time without notice. Thus, others should not use these Guidelines without consultation with APS.

## **II. PLANNING METHODOLOGY**

### **A. General**

APS uses a deterministic approach for transmission system planning. Under this approach, system performance should meet certain specific criteria under normal conditions (all lines in-service) and for any single contingency condition (any one element out-of-service). In general, an adequately planned transmission system will:

- Provide an acceptable level of service at the lowest cost for normal and single contingency operating conditions.
- Not result in the loss of load for any single contingency outage.
- Not result in cascading, overloaded equipment, or unacceptable voltage conditions for any single contingency outage.
- Work in compliment with local generation in load constrained areas.

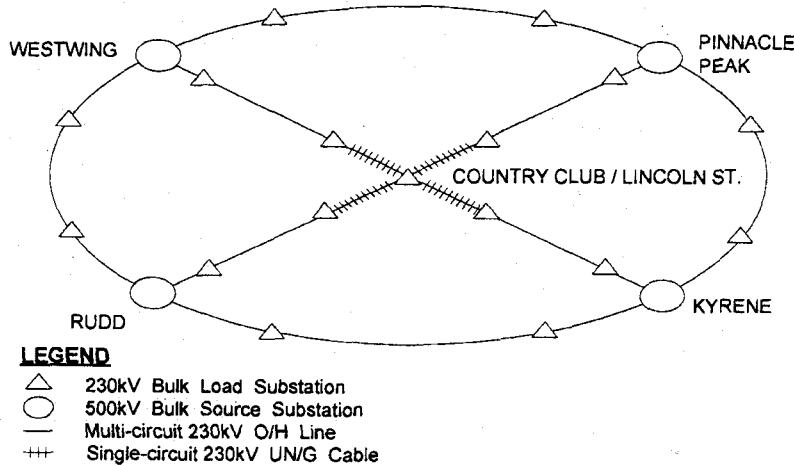
At present, probabilistic computational techniques are not directly used in the transmission planning process. However, system reliability performance is examined in the solution of switchyard circuit breaker arrangements, transformer reserve capacity, and in the choice of using single contingency outages for reserve transmission capacity. Further, deterministic guidelines generally provide some margin. The WECC is developing and plans to phase in probabilistic performance criteria in its planning criteria, which APS generally follows.

These planning methodologies, assumptions, and guidelines are used as the basis for the development of future transmission facilities. Additionally, consideration of potential alternatives to transmission facilities (such as distributed generation or new technologies) is evaluated on a case-specific basis. As the system grows and changes, and as more planning tools become available to the transmission planning engineer, revisions or additions to these guidelines will be made as appropriate.

#### B. 230kV Long-Range System

APS' planning process begins with the review of the major long-range 230kV system requirements. APS' philosophy regarding long-range 230kV transmission planning for the Phoenix Metropolitan Area has been to develop four major source points (Westwing, Pinnacle Peak, Kyrene, and Rudd) in the Valley; see *Figure 1*. In the future, other major source points may become necessary.

FIGURE 1  
APS VALLEY LONG RANGE  
230KV TRANSMISSION PHILOSOPHY



The Long-Range Substation Development Master Plan for the Phoenix Metropolitan Area will be utilized in determining the location of future 230/69kV and 69/12.5kV substations. This Master Plan considered future land use plans that were developed by government agencies, Landis aerial photo maps, and master plans that were provided by private developers. Other factors considered in developing the Master Plan included (1) APS' long-range forecasted load densities per square mile for residential, commercial, and industrial loads, (2) the 12.5kV service areas and associated number of 69/12.5kV substations, and (3) the 69kV service areas and associated 230/69kV substations for the Phoenix area.

#### C. Ten Year System Expansion Plans

The next step is to conduct detailed 230kV facility studies to develop APS' ten-year 230kV system expansion plans. In developing these plans, the 230kV and 69kV system requirements are coordinated to minimize future expansion of facilities, while at the same time achieving the long range 230kV and 69kV substation expansion plans set forth in the Master Plan. Consideration is given to load growth patterns due to master planned developments, new housing developments, shopping centers, high/mid rise buildings, and industrial parks. Also considered, are other system changes affected by right-of-way,

facilities siting constraints, routing of future transportation corridors, and joint planning with neighboring utilities and governmental entities.

**D. Facilities Keyed to Generation/Resource Additions**

New EHV transmission facilities are also required in conjunction with generation resources due to (1) a “merchant” request by an Independent Power Producer (IPP) for generator interconnection to the APS system, (2) a “merchant” request for point-to-point transmission service from the generator (receipt point) to the designated delivery point, or (3) designation of new resources or redesignation of existing units to serve APS network load (including removal of an older units’ native load designation).

If an interconnection or transmission service request is made by an IPP to interconnect into or deliver power over the APS system, APS will perform the study work and enter into appropriate agreements pursuant to applicable FERC regulations and APS’ Open Access Transmission Tariff. At present, FERC is reviewing and standardizing the interconnection process and agreements. APS may design and construct, at the IPP’s expense, transmission facilities identified in the Facilities Study that are needed to accommodate the interconnection or transmission service request.

**E. Generation Schedules**

For planning purposes, economic dispatches of network resources are determined for APS’ system peak load in the following manner:

- a. Determine base generation available and schedule these units at maximum output.
- b. Determine resources purchased from other utilities, IPPs, or power marketing agencies.
- c. Determine APS’ spinning reserve requirements.

- d. Schedule intermediate generation (oil/gas steam units) such that the spinning reserve requirements in section (c) above are met.
- e. Determine the amount of peaking generation (combustion turbine units) required to supply the remaining system peak load.

Phoenix area network resources are dispatched based on economics and any existing import limitations. When possible, spinning reserve will be carried on higher cost Phoenix area network generating units.

Generation output schedules for interconnected utilities and IPPs are based upon consultation with the neighboring utilities and IPPs or as modeled in the latest data in WECC coordinated study cases.

#### F. Study Period

Transmission plans are updated on a continuing basis to determine the projected facilities needed for each year over a ten-year period. These plans then become a basis for the transmission capital budget and future facility construction. Each year the plans for the next ten years are developed by first determining the requirements for the tenth year, and then defining the additions required for each of the preceding nine years. Needs for specific projects are incorporated in these ten-year plans.

#### G. Regional Coordinated Planning

##### 1. Western Electricity Coordinating Council (WECC)

APS is a member of the Western Electricity Coordinating Council. The focus of the WECC is on promoting the reliability of the interconnected bulk electric system. The WECC provides the means for:

- Developing regional planning and operating criteria.
- Coordinating future plans.
- Compiling regional data banks for use by the member systems and the WECC in conducting technical studies.
- Assessing and coordinating operating procedures and solutions to regional problems.

- Establishing an open forum with interested non-project participants to review the plan of service for a project.

## 2. Joint Studies

In many instances, EHV projects can serve the needs of several utilities, IPPs, or both. To this end, joint study efforts may be undertaken. Such joint study efforts endeavor to develop a plan that will meet the needs and desires of all individual companies involved.

## H. Load Projections

APS substation load projections are based on the APS Corporate Load Forecast. Substation load projections for neighboring interconnected utilities or power agencies operating in the WECC area are based on the latest data in WECC coordinated study cases. Heavy summer loads are used for the studies.

## I. Alternative Evaluations

### 1. General

In evaluating several alternative plans, comparisons of power flows, transient stability tests, and fault levels are made first. After the alternatives are found that meets the system performance criteria in each of these three areas comparisons may be made of the losses, transfer capability, impact on system operations, and reliability of each of the plans. Finally, the costs of facility additions (capital cost items), costs of losses, and relative costs of transfer capabilities are determined. A brief discussion of each of these considerations follows.

### 2. Power Flow Analyses

Power flows of base case (all lines in-service) and single contingency conditions are tested and should conform to the system performance criteria set forth in Section IV of these Guidelines. Double or multiple contingencies are examined, but in general, no facilities are planned for such conditions. Normal system voltages, voltage deviations, and voltage extreme limitations are based upon operating experience resulting in acceptable voltage levels to

the consumer. Power flow limits are based upon the thermal ratings and/or sag limitations of conductors or equipment, as applicable.

3. Transient Stability Studies

Stability guidelines are established to maintain system stability for single contingency, three-phase fault conditions. Double or multiple contingencies are examined, but in general, no facilities are planned for such conditions.

4. Short Circuit Studies

Three-phase and single-phase-to-ground fault studies are performed to ensure the adequacy of system protection equipment to clear and isolate faults.

5. Losses Analyses

A comparison of individual element and overall transmission system losses are made for each alternative plan being studied. The losses computed in the power flow program consist of the  $I^2R$  losses of lines and transformers and the core losses in transformers, where represented.

6. Transfer Capability Studies

In evaluating the relative merits of one or more EHV transmission plans, both simultaneous and non-simultaneous transfer capability studies are performed to determine the magnitude of transfer capabilities between areas or load centers.

7. Subsynchronous Resonance (SSR)

SSR phenomenon result from the use of series capacitors in the network where the tuned electrical network exchanges energy with a turbine generator at one or more of the natural frequencies of the mechanical system. SSR countermeasures are applied to prevent damage to machines as a result of transient current or sustained oscillations following a system disturbance.

SSR studies are not used directly in the planning process. SSR countermeasures are determined after the transmission plans are finalized.

8. Economic Evaluation

In general, an economic evaluation of alternative plans consists of a cumulative present worth or equivalent annual cost comparison of capital costs.

### **III. PLANNING ASSUMPTIONS**

#### **A. General**

##### **1. Loads**

Loads used for the APS system originate from the latest APS Corporate Load Forecast. In most cases, the corrected power factor of APS loads is 99.5% at 69kV substations.

##### **2. Generation and Other Resources**

Generation dispatch is based on firm power and/or transmission wheeling contracts including network resources designations.

##### **3. Normal Voltage Levels**

- a. Nominal EHV design voltages are 500kV, 345kV, 230kV, and 115kV.
- b. Nominal EHV operating voltages are 535kV, 348kV, 239kV, and 119kV.

##### **4. Sources of Databases**

WECC Heavy Summer base cases are the sources of the databases. Loop flow (unscheduled flow), of a reasonable amount and direction, will be allowed for use in planning studies.

##### **5. Voltage Control Devices**

Devices which can control voltages are shunt capacitors, shunt reactors, tap-changing-under-load (TCUL) and fixed-tap transformers, static VAR compensators, and machine VAR capabilities. If future voltage control devices are necessary, these devices will be evaluated based upon economics and the equipment's ability to obtain an adequate voltage profile on the EHV and HV systems.

##### **6. Phase Shifters**

In general, where phase shifters are used, schedules are held across the phase shifter in base case power flows and the phase shifter angle is held in the outage cases.

##### **7. Conductor Sizes**

Existing EHV voltages utilized by APS are 230kV, 345kV, and 500kV. It is presently planned that the 345kV transmission system will not be expanded,

thus all future APS EHV lines will be 500kV or 230kV. Planned 500kV lines will initially be modeled using tri-bundled 1780 kCM ACSR conductor (Chukar) with a flat phase spacing of 32 ft./32 ft./64 ft. between phases, unless otherwise specified. Preferred construction for 230kV lines consists of 954 ACSS conductor on steel poles.

#### 8. 69kV System Modeling

230kV facility outages may result in problems to the underlying 69kV system due to the interconnection of those systems. For this reason, power flow cases include a detailed 69kV system representation. Solutions to any problems encountered on the 69kV system are coordinated with the subtransmission planning engineers.

#### 9. Substation Transformers

- a. Bulk substation transformer banks may be made up of one three-phase or three single-phase auto-transformers, depending upon bank size and economics. For larger banks where single-phase transformers are used, a fourth (spare) single-phase transformer will be used in a jack-bus arrangement to improve reliability and facilitate connection of the spare in the event of an outage of one of the single-phase transformers. TCUL will be considered in the high voltage windings, generally with a range of plus or minus 10%. High voltage ratings will be 500kV or 345kV class and low voltage windings will be 230kV, 115kV, or 69kV class.
- b. For high-density load areas, both 230/69kV and 69/12.5kV transformers can be utilized. 230/69kV transformers will be rated at 113/150/188 MVA with a 65°C temperature rise, unless otherwise specified. 69/12.5kV transformers will be rated at 25/33/41 MVA with a 65°C temperature rise, unless otherwise specified. 188 MVA transformers are utilized in future 230/69kV substations up to a 200 MVA load level. Beyond the 200 MVA load level, the economic sizes of 230/69kV transformers to serve the load are as follows:

- 1) Add the third 188 MVA transformer if the load potential is expected to be 400 MVA or less.
- 2) If the load potential is expected to exceed 400 MVA then another 230/69kV substation will be built.

With all elements in service, a transformer may be loaded up to its top Forced Oil Air (FOA) rating without sustaining any loss of service life. For a single contingency outage (loss of one transformer) the remaining transformer or transformers may be loaded up to 20% above their top FOA rating, unless heat test data indicate a different overload capability. The loss of service life sustained will depend on the transformer pre-loading and the outage duration. Tap setting adjustment capabilities on 230/69kV transformers will be  $\pm 5\%$  from the nominal voltage setting (230/69kV) at  $2\frac{1}{2}\%$  increments.

## 10. Switchyard Arrangements

### a. 500kV and 345kV Substations

Existing 345kV switchyard arrangements use breaker-and-one-half, main-and-transfer, or modified paired-element circuit breaker switching schemes. Because of the large amounts of power transferred via 500kV switchyards and the necessity of having adequate reliability, all 500kV circuit breaker arrangements are planned for an ultimate breaker-and-one-half scheme. If only three or four elements are initially required, the circuit breakers are connected in a ring bus arrangement, but physically positioned for a breaker-and-one-half scheme. The maximum number of elements to be connected in the ring bus arrangement is six. System elements such as generators, transformers, and lines will be arranged in breaker-and-one-half schemes such that a failure of a center breaker will not result in the loss of two lines routed in the same general direction and will minimize the impact of losing two elements.

b. 230kV Substations

Future 230/69kV substations should be capable of serving up to 564 MVA of load. 400 MVA has historically been the most common substation load level in the Phoenix Metropolitan area. Future 230/69kV substations should accommodate up to four 230kV line terminations and up to three 230/69kV transformer bays. Based upon costs, as well as reliability and operating flexibility considerations, a breaker-and-one-half layout should be utilized for all future 230/69kV Metropolitan Phoenix Area substations, with provision for initial development to be a ring bus. Any two 230/69kV transformers are to be separated by two breakers so that a stuck breaker will not result in an outage of both transformers.

11. Series Capacitor Application

Series capacitors may be used on EHV lines to increase system stability, for increased transfer capability, and/or for control of power flow. The series capacitors may be lumped at one end of a line because of lower cost; however, the capacitors are generally divided into two banks, one at either end of a line, for improved voltage profile.

12. Shunt and Tertiary Reactor Application

Shunt and/or tertiary reactors may be installed to prevent open end line voltages from being excessive, in addition to voltage control. The open end line voltage must not be more than 0.05 per unit voltage greater than the sending end voltage. Tertiary reactors may also be used for voltage and VAR control as discussed above.

B. Power Flow Studies

1. System Stressing

Realistic generation capabilities and schedules should be used to stress the transmission system in order to maximize the transfer of resources during the maximum load condition.

## 2. Displacement

In cases where displacements (due to power flow opposite normal generation schedules) may have an appreciable effect on transmission line loading, a reasonable amount of displacement (Generation Units) may be removed.

## C. Transient Stability Studies

### 1. Fault Simulation

When studying system disturbances caused by faults, two conditions will be simulated:

- a. Three-phase-to-ground faults, and
- b. Single-line-to-ground faults with a stuck circuit breaker in one phase with back-up delayed clearing.

### 2. Margin

- a. Generation margin may be applied for the contingencies primarily affected by generation, or
- b. Power flow margin may be applied for the contingencies primarily affected by power flow.

### 3. Unit Tripping

Generator unit tripping may be allowed in-order to increase system stability performance.

### 4. Machine Reactance Representation

For transient stability studies, the unsaturated transient reactance of machines with full representation will be used.

### 5. Fault Damping

Fault damping will be applied to the generating units adjacent to faults.

Fault damping will be determined from studies that account for the effect of generator amortisseur windings and the SSR filters.

### 6. Series Capacitor Switching

Series capacitors, locations to be determined from short circuit studies, will be flashed and reinserted as appropriate.

#### D. Short Circuit Studies

Three-phase and single-phase-to-ground faults will be evaluated.

##### 1. Generation Representation

All generation will be represented.

##### 2. Machine Reactance Representation

The saturated subtransient reactance ( $X''_d$ ) values will be used.

##### 3. Line Representation

The transmission line zero sequence impedance ( $X_0$ ) is assumed to be equal to three times the positive sequence impedance ( $X_1$ ).

##### 4. Transformer Representation

The transformer zero sequence impedance ( $X_0$ ) is assumed to be equal to the positive sequence impedance ( $X_1$ ). Bulk substation transformers are modeled as auto-transformers. The two-winding model is that of a grounded-wye transformer. The three-winding model is that of a wye-delta-wye with a solid ground.

### IV. SYSTEM PERFORMANCE

#### A. Power Flow Studies

##### 1. Normal (Base Case Conditions)

###### a. Voltage Levels

###### 1) General

(a) 500kV bus voltages will be maintained between 1.05 and 1.08 p.u. on a 500kV base.

(b) 345kV bus voltages will range between .99 and 1.04 p.u. on the 345kV system.

(c) 500kV and 345kV system voltages are used to maintain proper 230kV bus voltages.

- (d) Voltage on the 230kV and 115kV system should be between 1.01 p.u. and 1.05 p.u.
  - (e) Tap settings for 230/69kV and 345/69kV transformers should be used to maintain low side (69kV) voltages of 1.03 to 1.04 p.u. Seasonal tap changes may be required.
- 2) Specific Buses
- (a) APS Pinnacle Peak 230kV bus voltage should be between 1.025 p.u. and 1.035 p.u.
  - (b) APS Westwing 230kV bus voltage should be between 1.04 p.u. and 1.05 p.u.
  - (c) Saguaro 115kV bus voltage will be approximately 1.035 p.u.
  - (d) Voltage at the Prescott (DOE) 230kV bus should be approximately 1.02 p.u.

b. Facility Loading Limits

1) Transmission Lines

Transmission line loading cannot exceed 100% of the continuous rating, which is based upon established conductor temperature limit or sag limitation.

2) Underground Cable

Underground cable loading should not exceed 100% of the continuous rating with all elements in service. This rating is based on a cable temperature of 85°C with no loss of cable life.

3) Transformers

Transformers cannot exceed 100% of top FOA, 65°C rise, nameplate ratings.

4) Series Capacitors

Series Capacitors cannot exceed 100% of continuous rating.

c. Interchange of VARs

Interchange of VARs between companies at interconnections will be reduced to a minimum and maintained near zero.

d. Distribution of Flow

Schedules on a new project will be compared to simulated power flows to ensure a reasonable level of flowability.

2. Single Contingency Outages

a. Voltage Levels

Maximum voltage deviation on APS' major buses cannot exceed 5%. This deviation level yields a close approximation to the post-transient VAR margin requirements of WECC.

b. Facilities Loading Limits

1) Transmission Lines

Transmission line loading cannot exceed 100% of the lesser of the sag limit or the emergency rating (30-minute rating) which is based upon established conductor temperature limits.

2) Underground Cable

Underground cable loading should not exceed the emergency rating during a single-contingency outage. This rating is based on a cable temperature of 105°C for two hours of emergency operation with no loss of cable life.

3) Transformers

Transformers cannot exceed 120% of top FOA, 65°C rise, nameplate ratings.

4) Series Capacitors

Series Capacitors cannot exceed 100% of emergency rating.

c. Generator Units

Generator units used for controlling remote voltages will be modified to hold their base case terminal voltages.

d. Impact on Interconnected System

Single contingency outages will not cause overloads upon any neighboring transmission system.

## **B. Transient Stability Studies**

Transient stability studies are primarily performed on the 500kV and 345kV systems.

### **1. Fault Simulation**

Three-phase-to-ground faults and single-line-to-ground faults, simulating a stuck circuit breaker in one phase with back-up delayed clearing will be simulated. Fault clearing times of four cycles after fault inception (5 cycles for a 230kV fault) and a back-up clearing time of twelve cycles after fault inception is utilized. System elements are switched out at the appropriate clearing times, as applicable. Fault damping will be applied when applicable at fault inception.

### **2. Series Capacitor Switching**

Series capacitors, at locations determined from short-circuit studies, will be flashed at fault inception and will be reinserted depending on their reinsertion types.

### **3. System Stability**

The system will be considered stable if the following conditions are met:

- a. All machines in the system remain synchronized as demonstrated by the relative rotor angles.
- b. System damping exists as demonstrated by the damping of relative rotor angles and the damping of voltage magnitude swings. Voltages for the first swing after fault clearing should not drop below 75% of pre-fault value with maximum time duration of 20 cycles for voltage dip exceeding 20%.

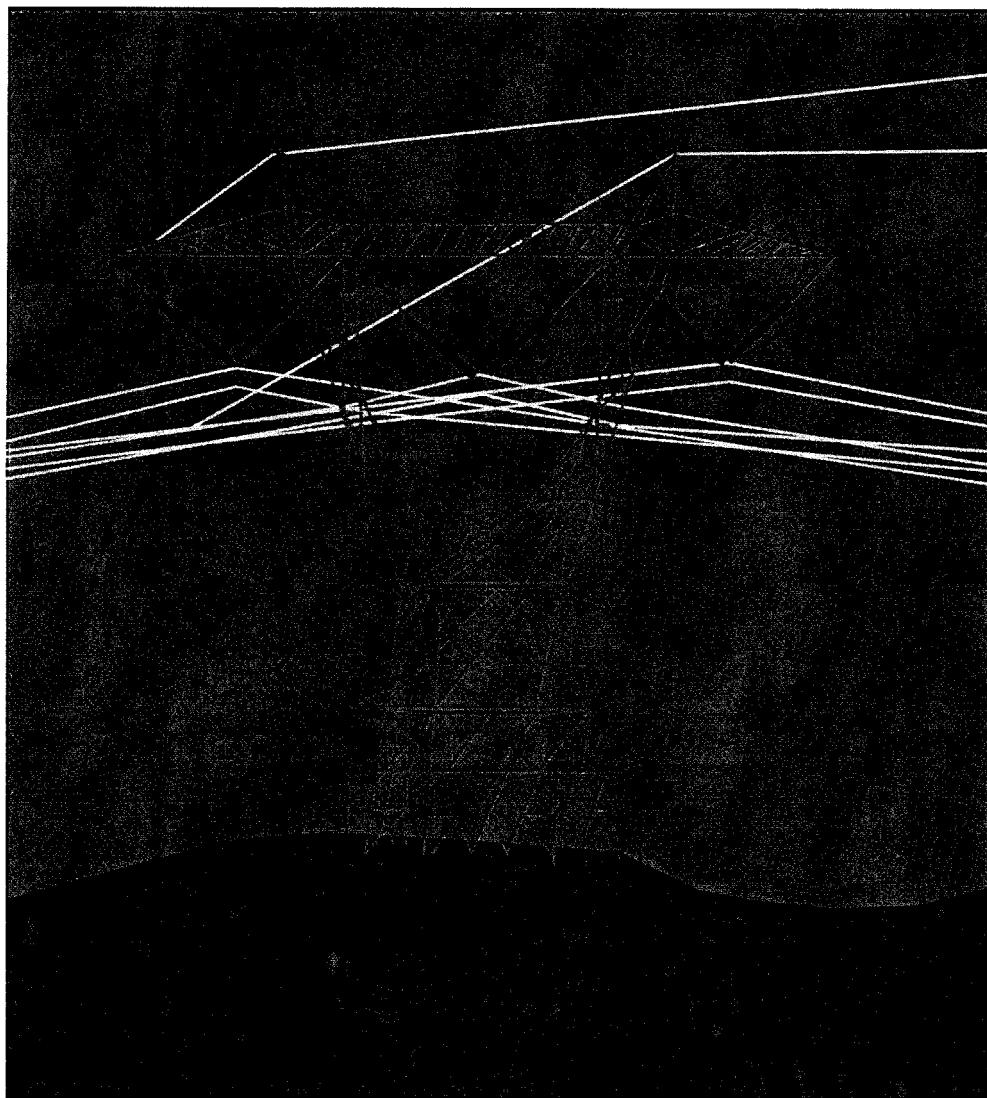
### **4. Re-closing**

Automatic re-closing of circuit breakers controlling EHV facilities is not utilized.

## **C. Short Circuit Studies**

Fault current shall not exceed 100% of the substation fault current interruption capability for three-phase or single-line-to-ground faults.

## **2003 SYSTEM RATING MAPS**



**Prepared By**

**Transmission Operations  
June, 2003**

# **TABLE OF CONTENTS**

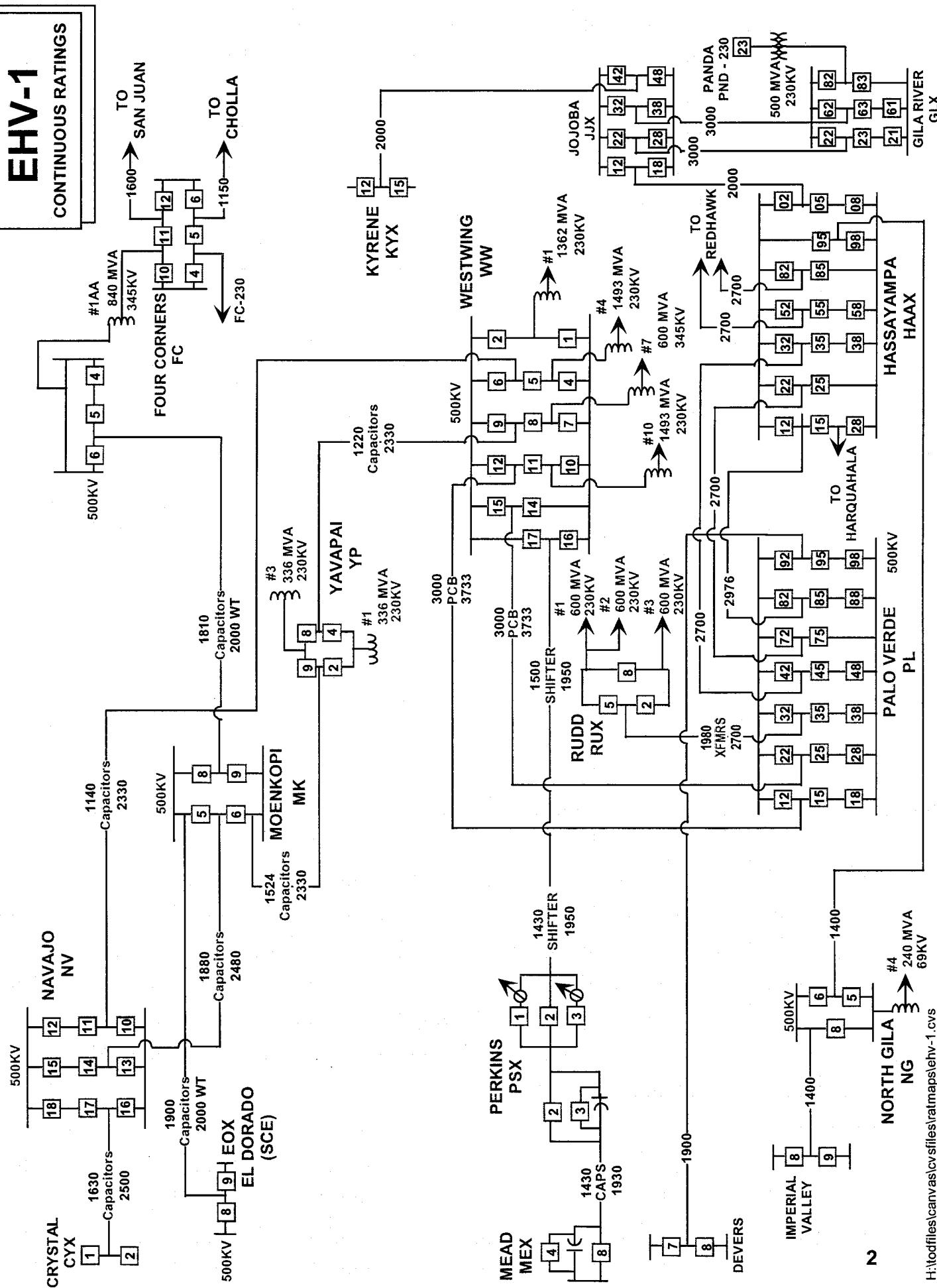
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<b>EHV CONTINUOUS</b>	-----	2
<b>EHV EMERGENCY</b>	-----	4
<b>METRO 230kV CONTINUOUS</b>	-----	6
<b>METRO 230kV EMERGENCY</b>	-----	7
<b>NORTHERN 230kV CONTINUOUS</b>	-----	8
<b>NORTHERN 230kV EMERGENCY</b>	-----	9
<b>SOUTHERN 230kV CONTINUOUS</b>	-----	10
<b>SOUTHERN 230kV EMERGENCY</b>	-----	11

## **LEGEND SYSTEM RATING MAPS**

<u>SYMBOL</u>	<u>DESCRIPTION</u>
— ### —	CURRENT LIMIT IN AMPS LIMITING ELEMENT CONDUCTOR LIMIT IN AMPS
	TRANSFORMER LIMITS ARE IN MVA
—————	OVERHEAD TRANSMISSION LINE
-----	UNDERGROUND CABLE
M	MOTOR OPERATED SWITCH
V	VACCUM SWITCH
H	HYDRAULIC SWITCH
█	BREAKER NUMBER

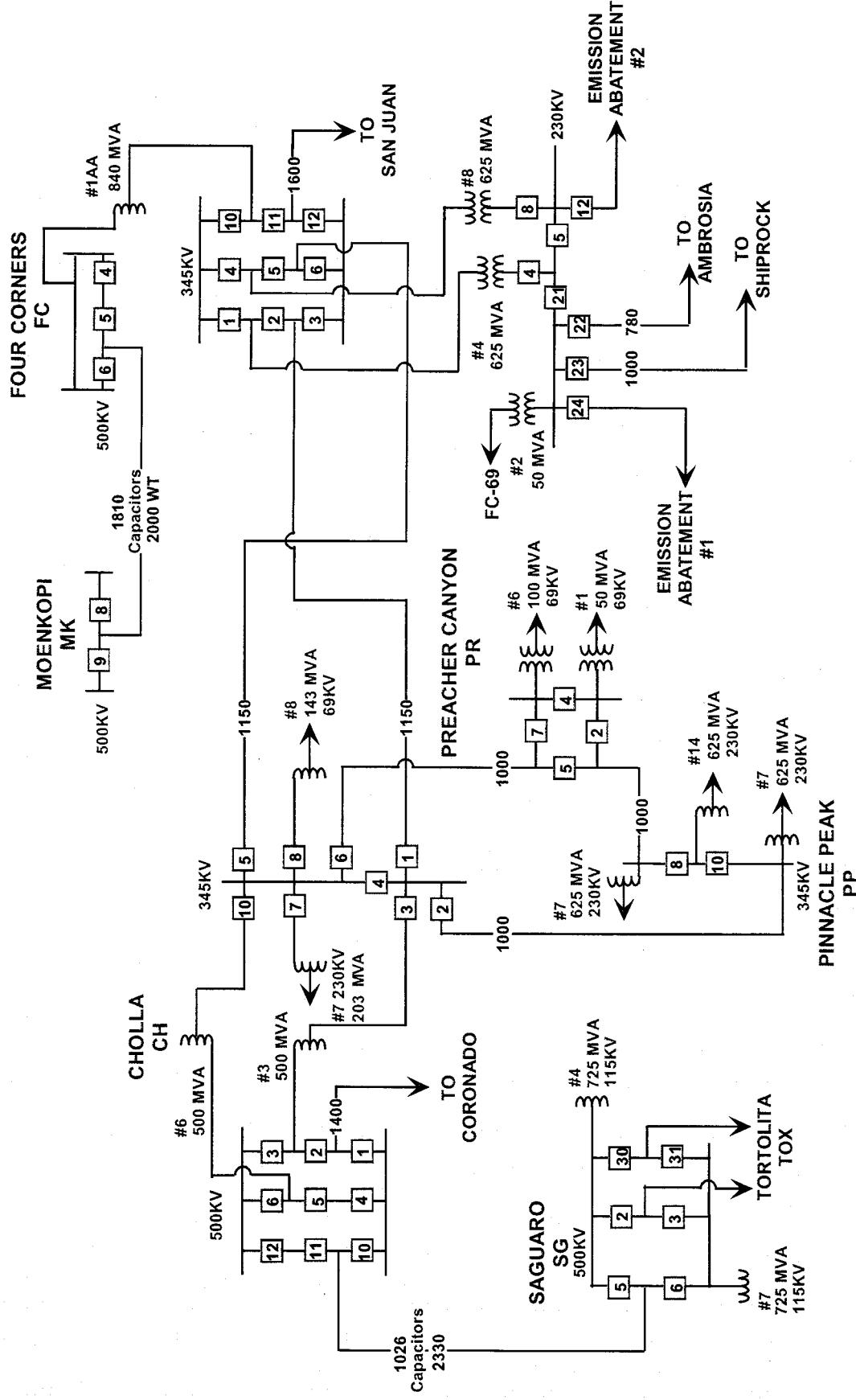
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## CONTINUOUS RATINGS



# EHV-2

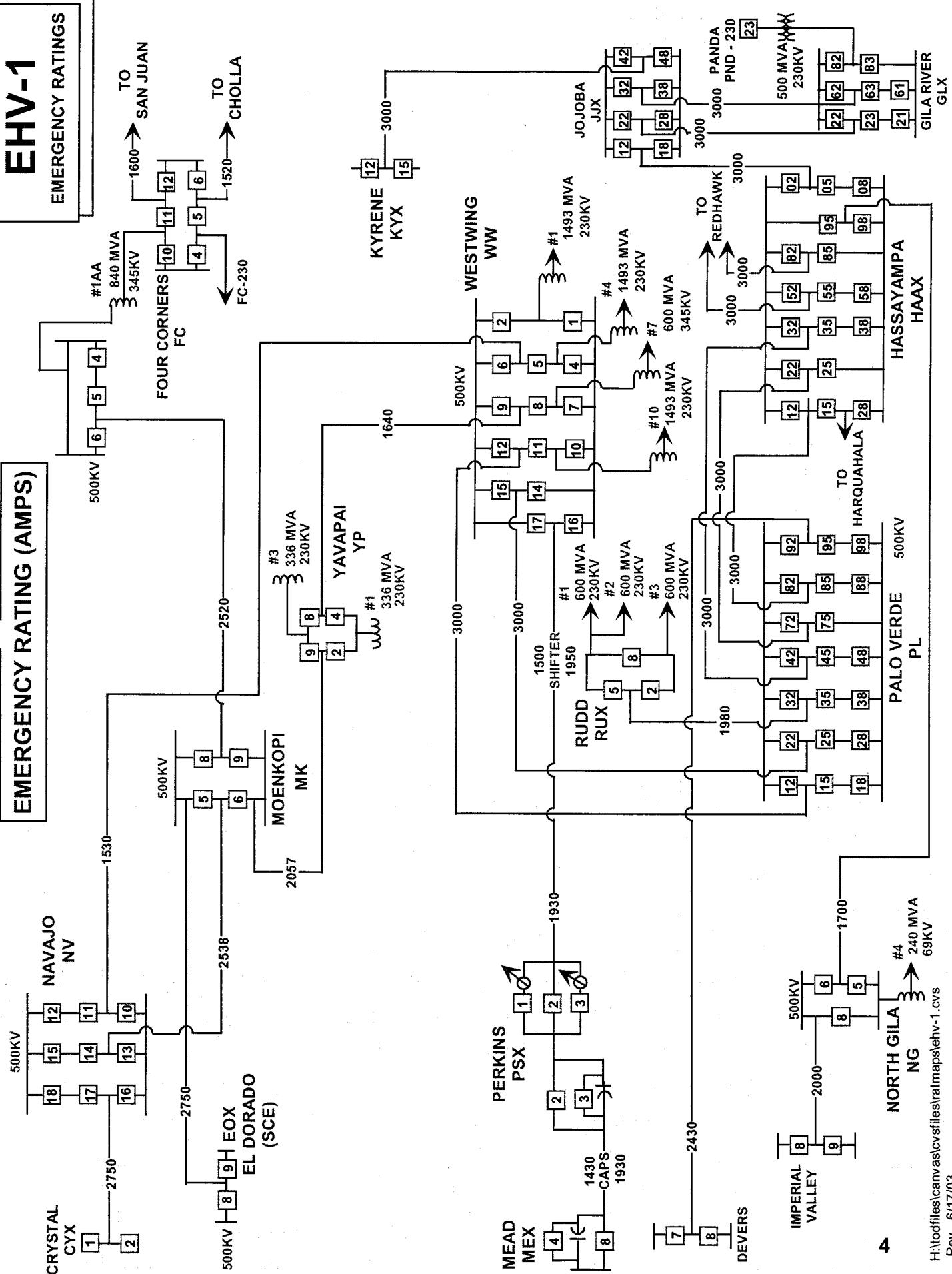
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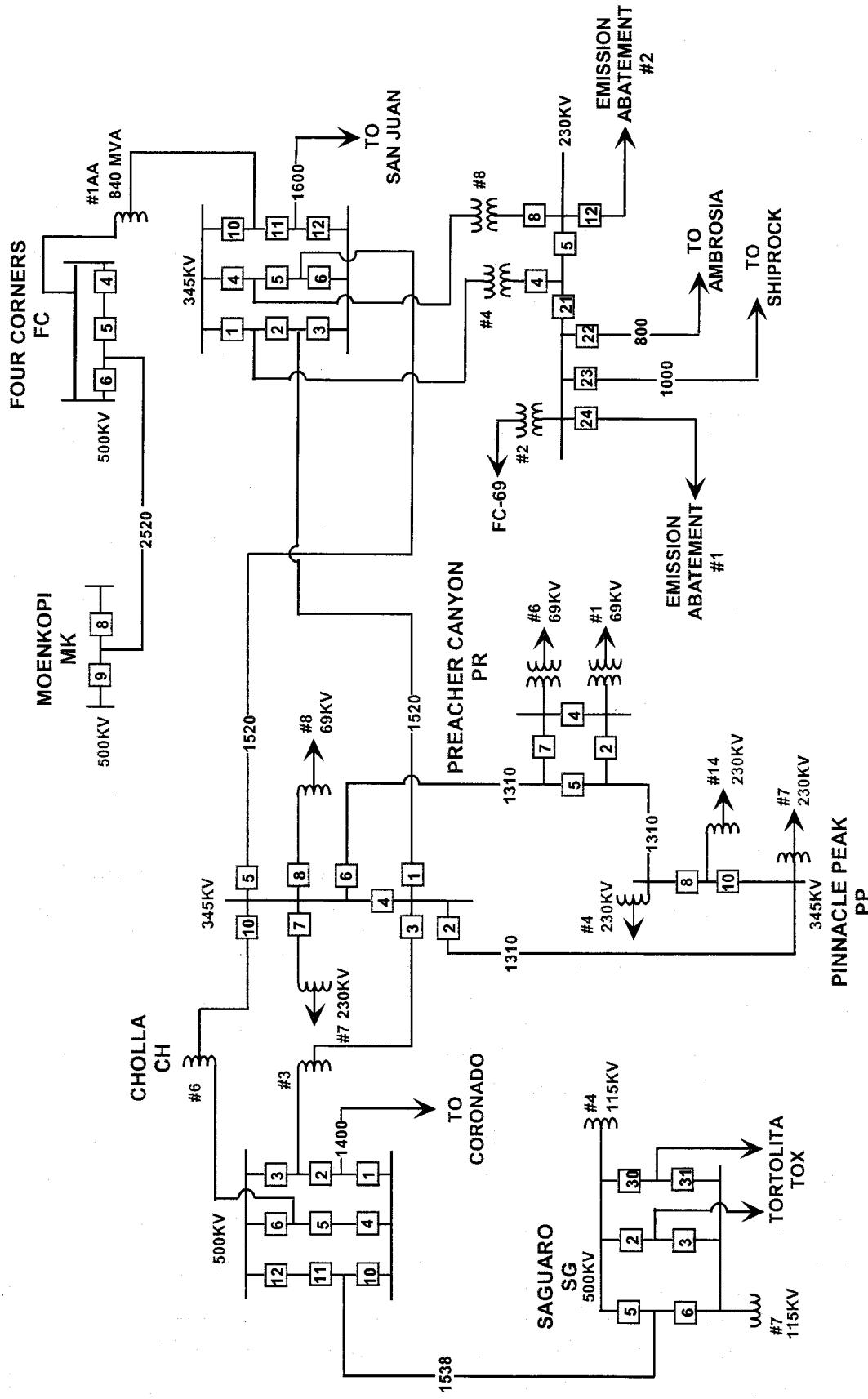
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## EMERGENCY RATINGS

## EMERGENCY RATING (AMPS)



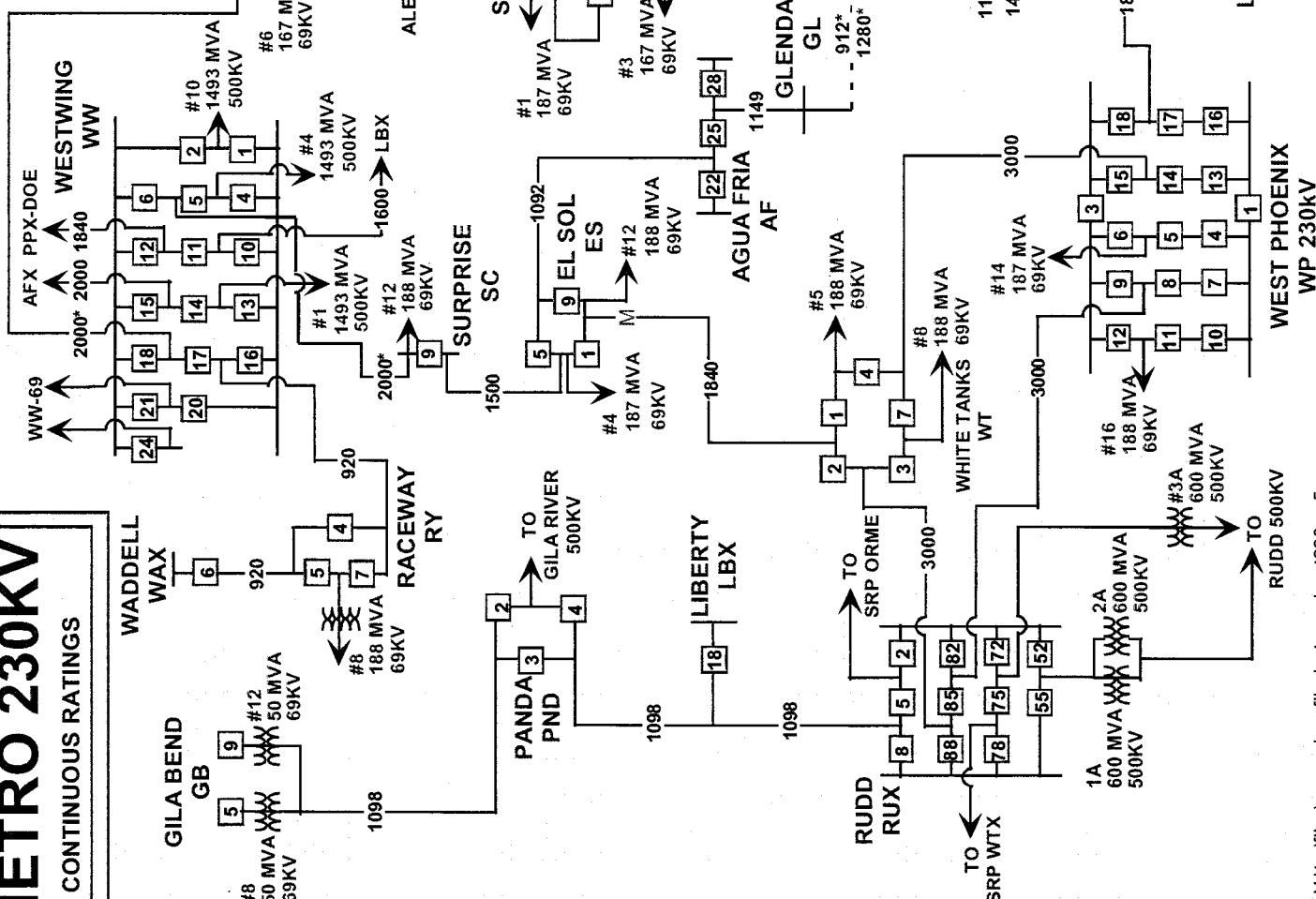
## EMERGENCY RATING (AMPS)



## EHSV-2 EMERGENCY RATINGS

# METRO 230KV

CONTINUOUS RATINGS



PINNACLE PEAK

(SRP) PXX

DEER VALLEY DV

REACH RCH

PINNACLE PEAK PP

ALEXANDER AXR

LONEPEAK LP

SUNNYSLOPE SS

Meadowbrook ME

COUNTRY CLUB CC

PINNACLE PEAK EAST PPE

EL SOL ES

AGUA FRIA AF

WHITE TANKS WT

RUDD RUX

WEST PHOENIX WP

TO KYRENE OCOTILLO OC

TO BRANDON SRP

TO CACTUS CX

TO KYRENE OCOTILLO OC

TO KYRENE OCOTILLO OC

TO KYRENE OCOTILLO OC

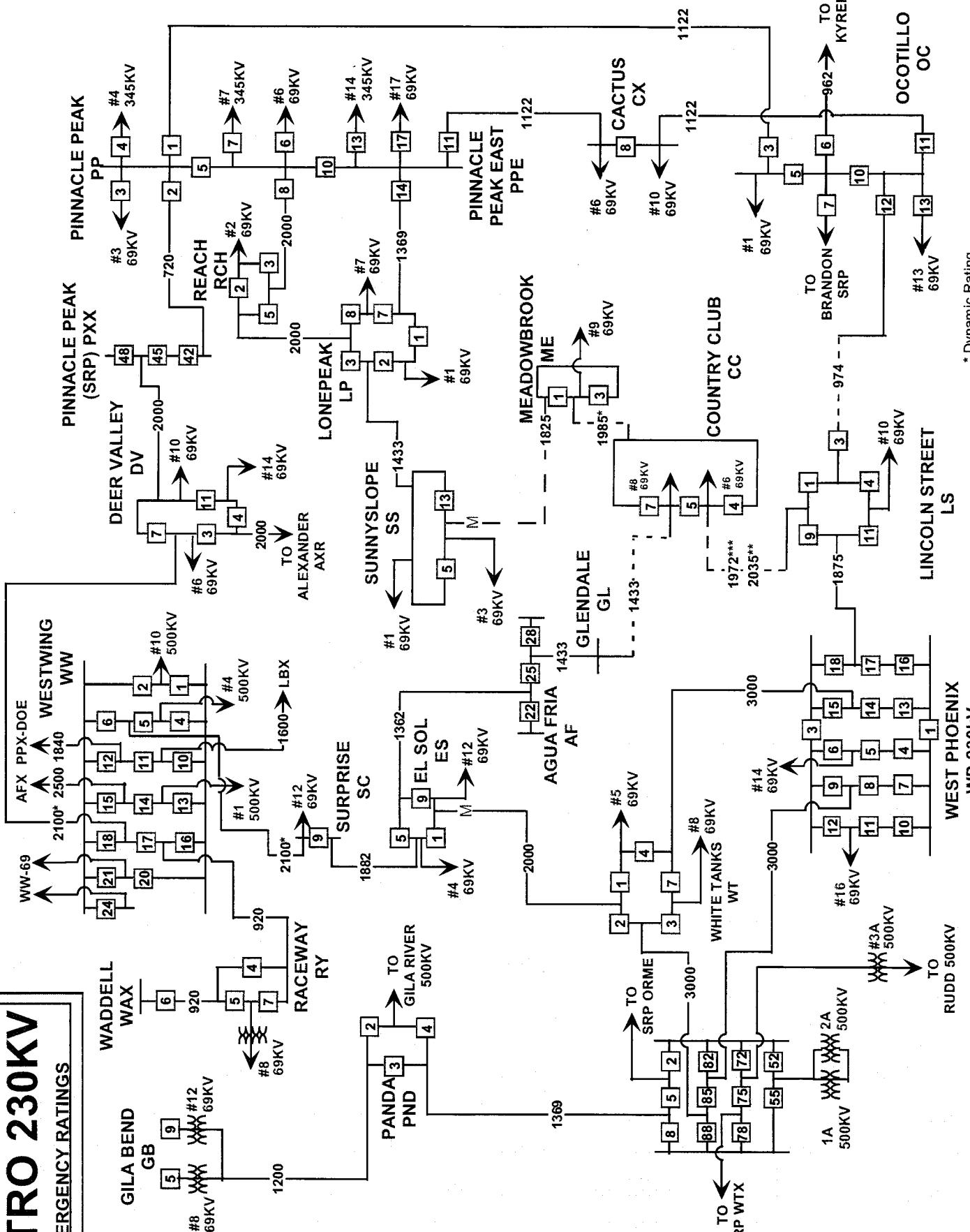
TO KYRENE OCOTILLO OC

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Rev. 06/12/03

\* Dynamic Rating  
\*\* No forced cooling on GT-CC, Cooling both ends LS-CC  
\*\*\* Forced cooling on GT-CC, Cooling one end LS-CC

METRO 230KV

EMERGENCY RATINGS



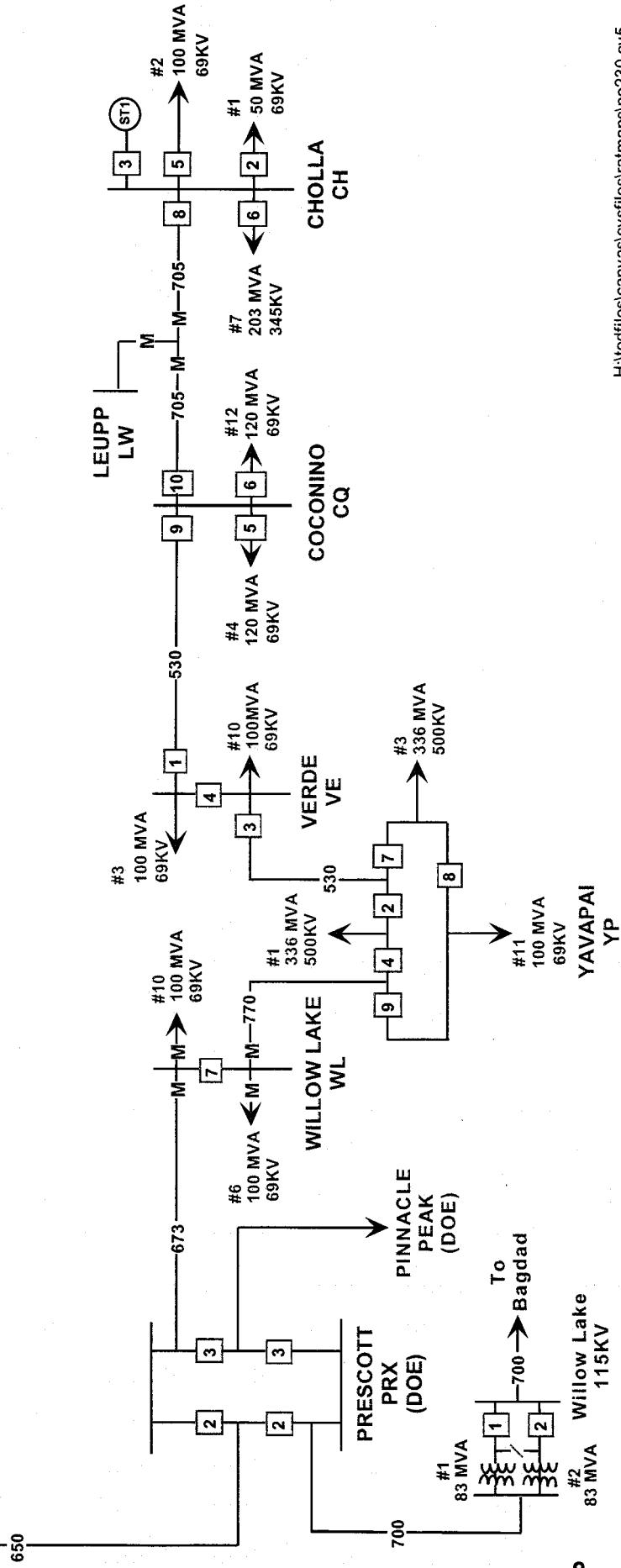
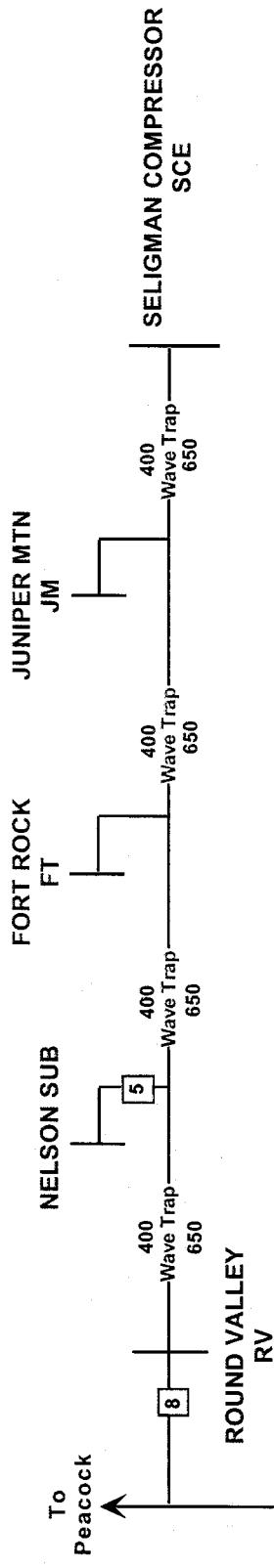
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Rev 06/17/03

8

- \* Dynamic Rating
- \*\* No forced cooling on GT-CC, Cooling both ends LS-CC
- \*\*\* Forced cooling on GT-CC, Cooling one end LS-CC

# NORTHERN 230KV

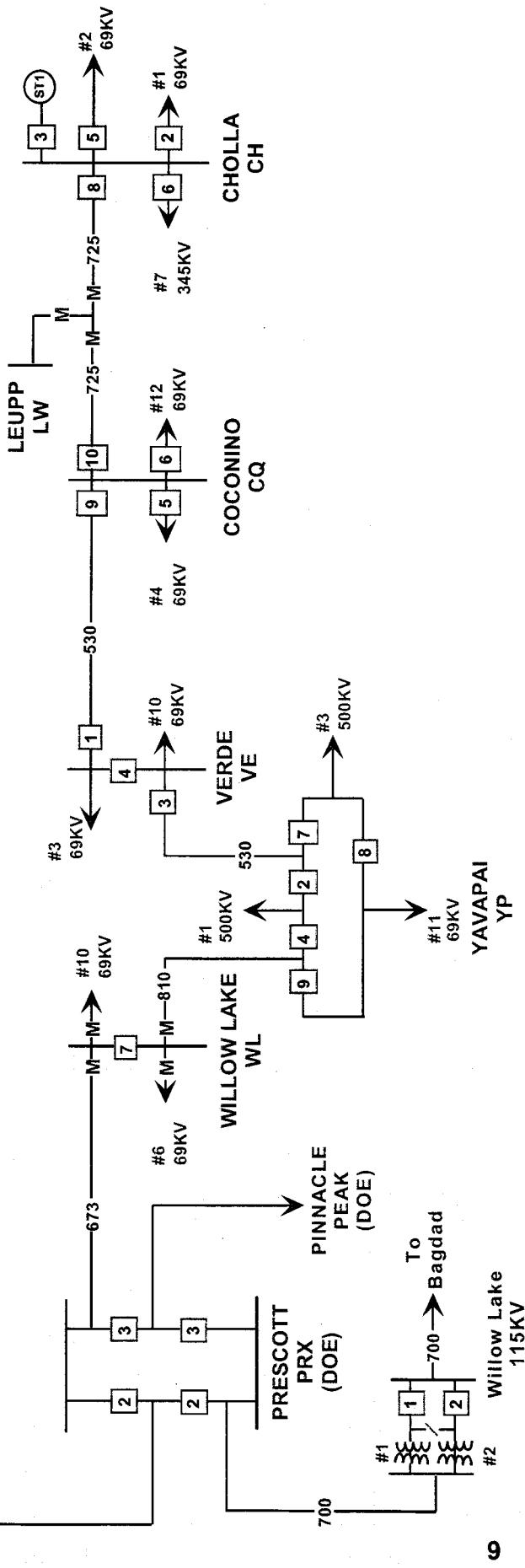
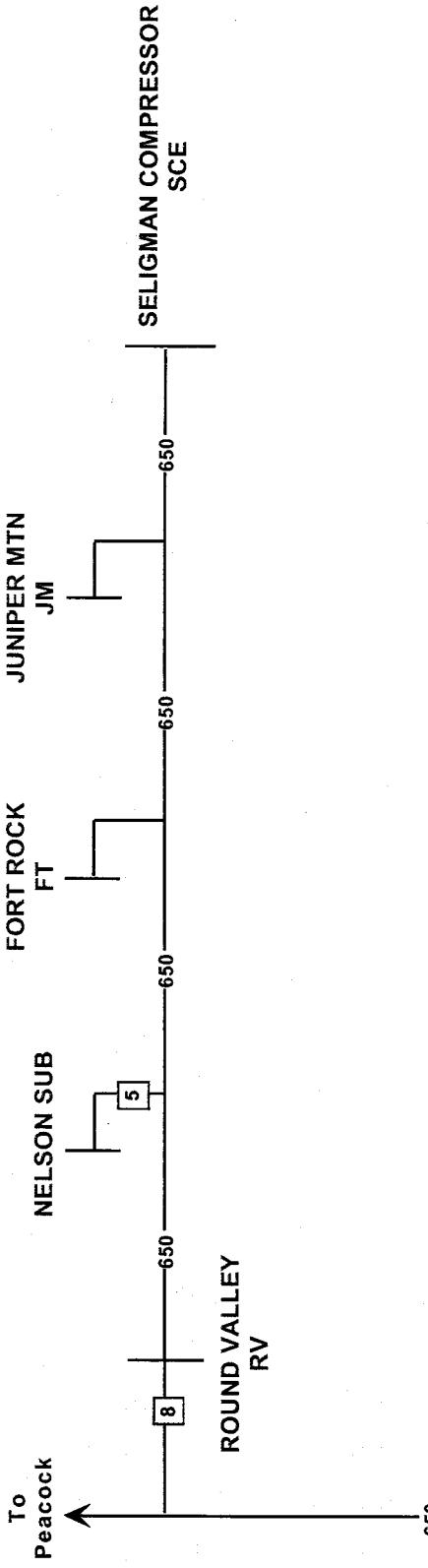
CONTINUOUS RATINGS



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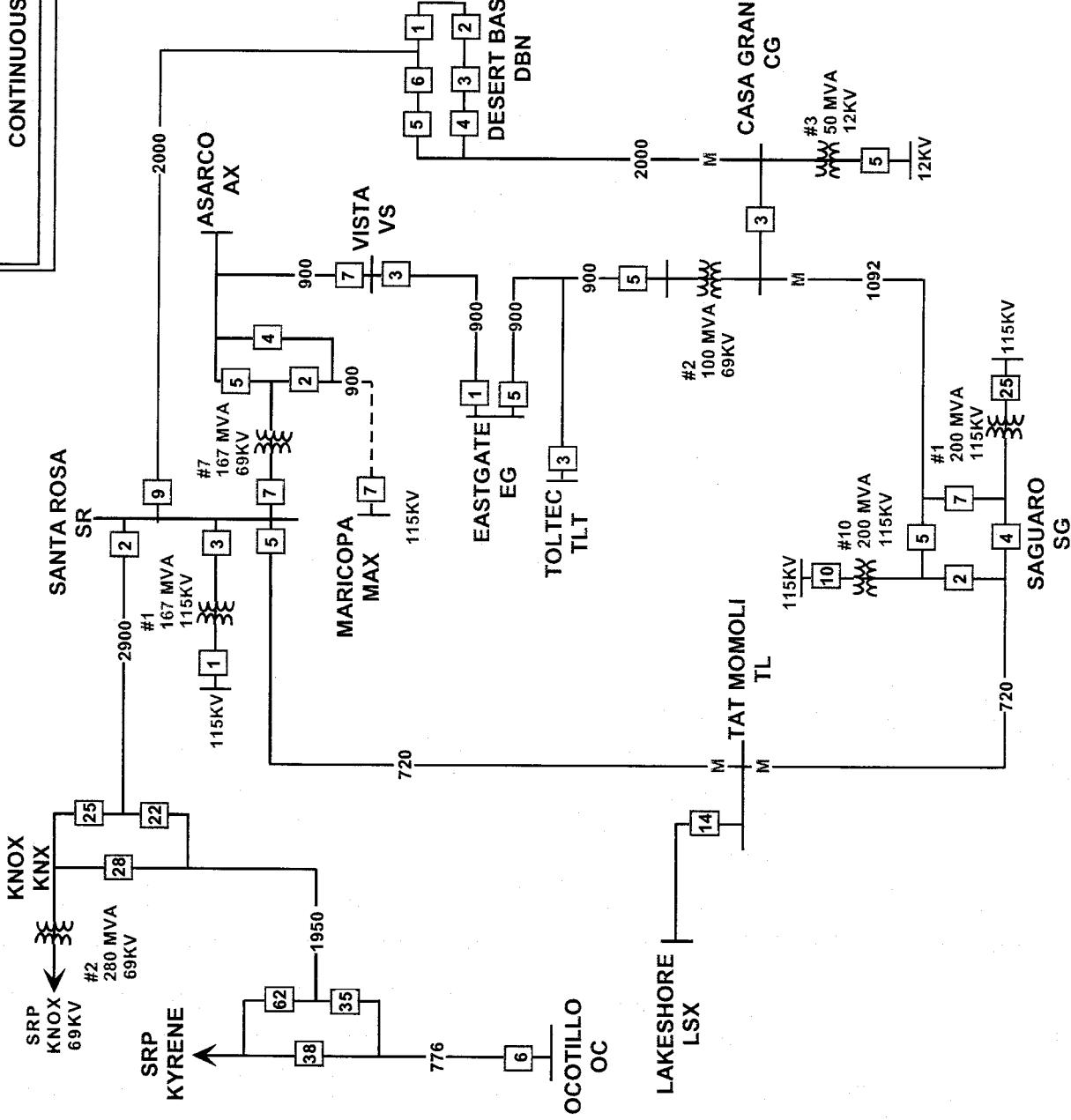
EMERGENCY RATINGS

## EMERGENCY RATING (AMPS)

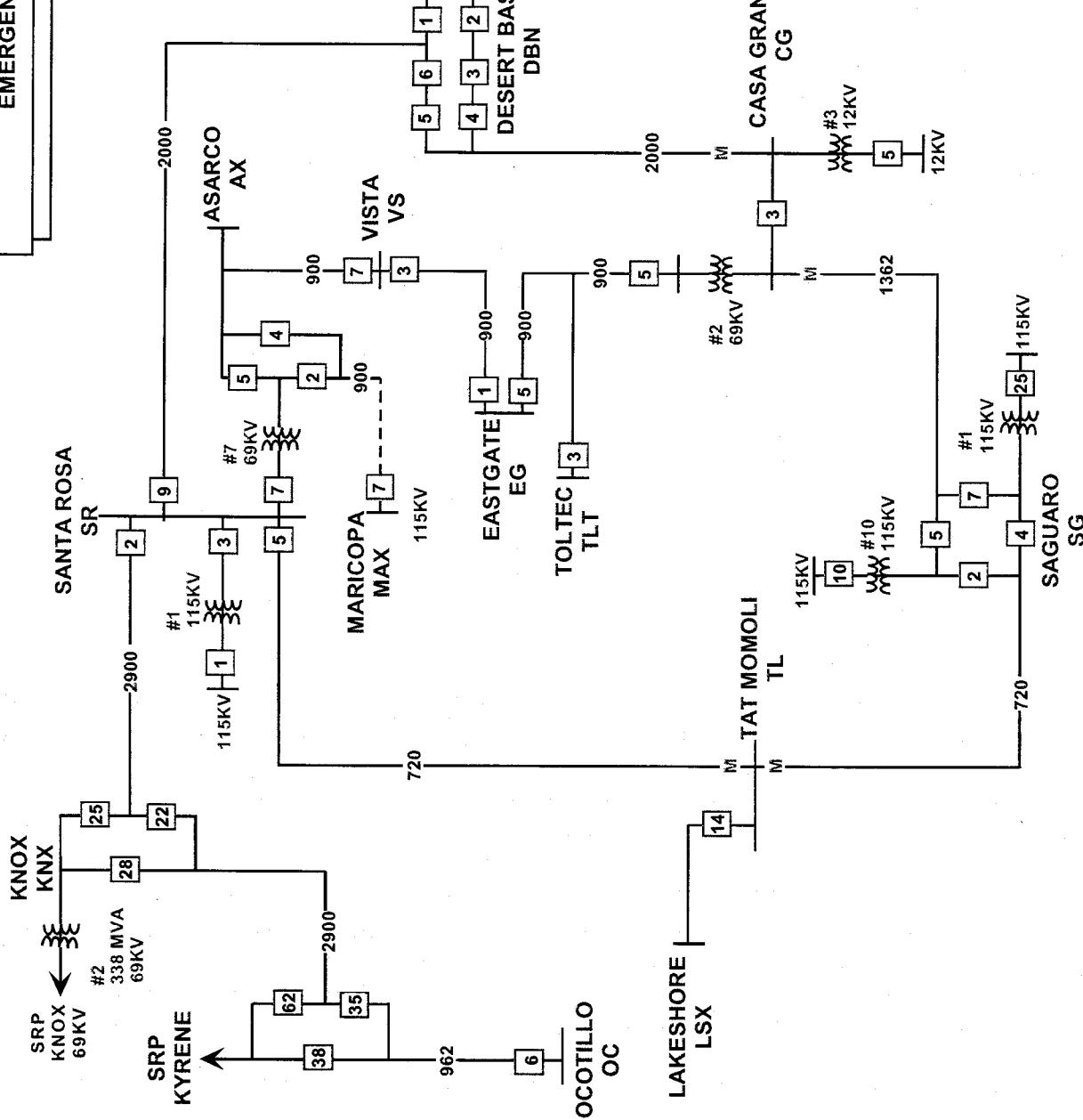


# SOUTHERN 230KV

CONTINUOUS RATINGS



## EMERGENCY RATING (AMPS)



## SOUTHERN 230KV

### EMERGENCY RATINGS

**ARIZONA PUBLIC SERVICE COMPANY**

**TEN-YEAR PLAN**

**2004 – 2013**

**TECHNICAL STUDY REPORT**

**FOR**

**THE ARIZONA CORPORATION COMMISSION**

**JANUARY 2004**

## Table of Contents

	<u>Page</u>
1. Introduction .....	1
2. Power Flow Analyses .....	1
3. Stability Analysis .....	3
 Appendices	
A. Power Flow Maps.....	A1-A40
B. 2006 Stability Plots.....	B1-B30
C. 2012 Stability Plots.....	C1-C31
D. Loop-in of the Jojoba-Kyrene 500-kV line into Rudd.....	D1

**ARIZONA PUBLIC SERVICE COMPANY**  
**2004-2013**  
**TEN-YEAR PLAN**  
**TECHNICAL STUDY REPORT**

**I. Introduction**

This technical study report is filed with the ACC pursuant to A.R.S. § 40-360.02, as amended by House Bill 2040, and Arizona Corporation Commission (“Commission”) Decision No. 63876 (July 25, 2001) regarding the Biennial Transmission Assessment prepared by Commission Utilities Division Staff.

Two aspects of technical studies were performed and reported here. They are power flow analyses and stability analyses. Power flow analysis was performed for two scenarios. The first is for all transmission system elements being in service. All system elements must be within its continuous rating. The second scenario is for outage of a single element. All remaining system elements must remain within its emergency ratings. Voltage deviations for these scenarios must also be within established guidelines. These voltage deviation guidelines closely approximate post-transient var margin requirements of the Western Electricity Coordinating Council. More detail is provided in APS’ Transmission Planning Process and Guidelines, which is also included in this filing.

The stability analyses were performed to simulate electrical disturbances on the transmission system and evaluate the system response. The desired result is that all generators will remain on line, no additional lines will open, and the system oscillations will damp out.

Results of the power flow and stability analyses aid in determining when and where new electrical facilities are needed because of reliability or security reasons. Additionally, some facilities are planned to address adequacy concerns. These include the interconnection of generation to the transmission system or efforts to increase import capability to load-constrained or other areas.

**II. Power Flow Analyses**

Power flow cases were created for each year of the 2004-2013 study time frame. These cases represent the latest transmission and sub-transmission plans, load projections, and resource plans of utilities and independent power producers. Base case and single contingency conditions are evaluated to determine system needs and timing. Various iterations of possible solutions lead to the final plans for transmission additions.

The single contingency analysis involves simulations for every non-radial 115kV or above line that APS owns, partially owns, or operates. Transformer outages are also evaluated. Results of the power flow studies are tabulated in a Security Needs Table and an Adequacy Needs Table, below. These tables identify sixteen transmission

lines/projects that are included in this Ten-Year Plan filing. Some of the projects were classified as Adequacy Needs because of the uncertainty of generation location, size, and availability in the later years. As projects near the five-year planning time frame, they may be redefined as Security Needs projects. Selected maps of the power flow simulations are contained in the appendix.

### Security Needs Table

<b>Transmission Project</b>	<b>In Service Year</b>	<b>Critical Outage</b>	<b>Limiting Element</b>
Loop-in of Pinnacle Peak-Prescott 230kV line to Gavilan Peak 230kV substation	2005	Jomax-Dove Valley 69kV line	Voltage deviation @ Dove Valley 69kV & load loss @ Gavilan Peak 69kV and Dove Valley 69kV.
Rudd-TS3 230kV line & TS4-TS3 230kV line.	2006	White Tanks 230/69kV transformer or local 69kV lines	White Tanks 230/69kV xfmr #2 & voltage deviation @ White Tanks & 69kV system busses
TS1-TS2-TS3 230kV lines	2008	Loss of Surprise 230/69kV transformer or loss of Westwing 230/69kV transformer, and local 69kV lines	Surprise 230/69kV transformer, Westwing 230/69kV transformer, and local 69kV lines
Raceway-Avery 230kV line	2008	Raceway transformer & local 69kV lines	Voltage deviation @ Avery & 69kV system lines
Loop-in of Coronado-Silver King 500kV line to Second Knoll	2009	Cholla-Zeniff 69kV line or Cholla-Showlow 69kV line	Voltage deviations on the sub-transmission system in the area.
Pinnacle Peak-TS6-Avery 230kV line	2009	Raceway-Avery 230kV line	230/69kV transformers @ Deer Valley, Gavilan Peak, and Pinnacle Peak and voltage deviation @ Avery
Gila Bend-Yuma 230kV line	2010	Palo Verde-N. Gila 500kV line	Voltage deviation @ Yuma & scheduling capacity

### Adequacy Needs Table

<b>Transmission Project</b>	<b>In Service Year</b>	<b>System Benefits</b>
Hassayampa-Jojoba-Pinal West 500kV line. Pinal West-Santa Rosa-S.E. Valley 500kV line.	2006-2007	Increases import capability for the Phoenix metropolitan area, increases the export capability from the PV area. Increases transmission system reliability and ability to deliver power.
Loop-in of Cholla-Saguaro 500kV line into Silver King 500kV substation.	2007	Increase transmission system reliability and ability to deliver power. Increases import capability for the Phoenix metropolitan area.
Palo Verde-TS5 500kV. TS5-TS1 230kV.	2007	Increases import capability for the Phoenix metropolitan area, increases the export capability from the PV area. Increase system capacity and reliability to deliver power to the western part of the Phoenix Metropolitan area.
Loop-in of Navajo-Westwing 500kV to Raceway 500kV substation. TS5-Raceway 500kV line.	2010	Increases import capability for the Phoenix metropolitan area, increases the export capability from the PV area. Increase system reliability and ability to deliver power.
Westwing-Raceway 230kV line #2	2010	Increase reliability to Raceway and provide a backup for outage of Westwing 500/230kV transformers.
Gila Bend-TS8 230kV line	2012	Increases import capability for the Yuma area. Increases transmission system reliability and ability to deliver power.
Westwing-El Sol 230kV line	2013	Increase transmission system reliability and ability to deliver power.
Loop-in of Cholla-Pinnacle Peak 345kV to Mazatzal 345kV substation	TBD	Increase transmission system reliability and ability to deliver power.
Palo Verde-Pinal West-Saguaro	TBD	Increase transmission system reliability and ability to deliver power.

### III. Stability Analysis

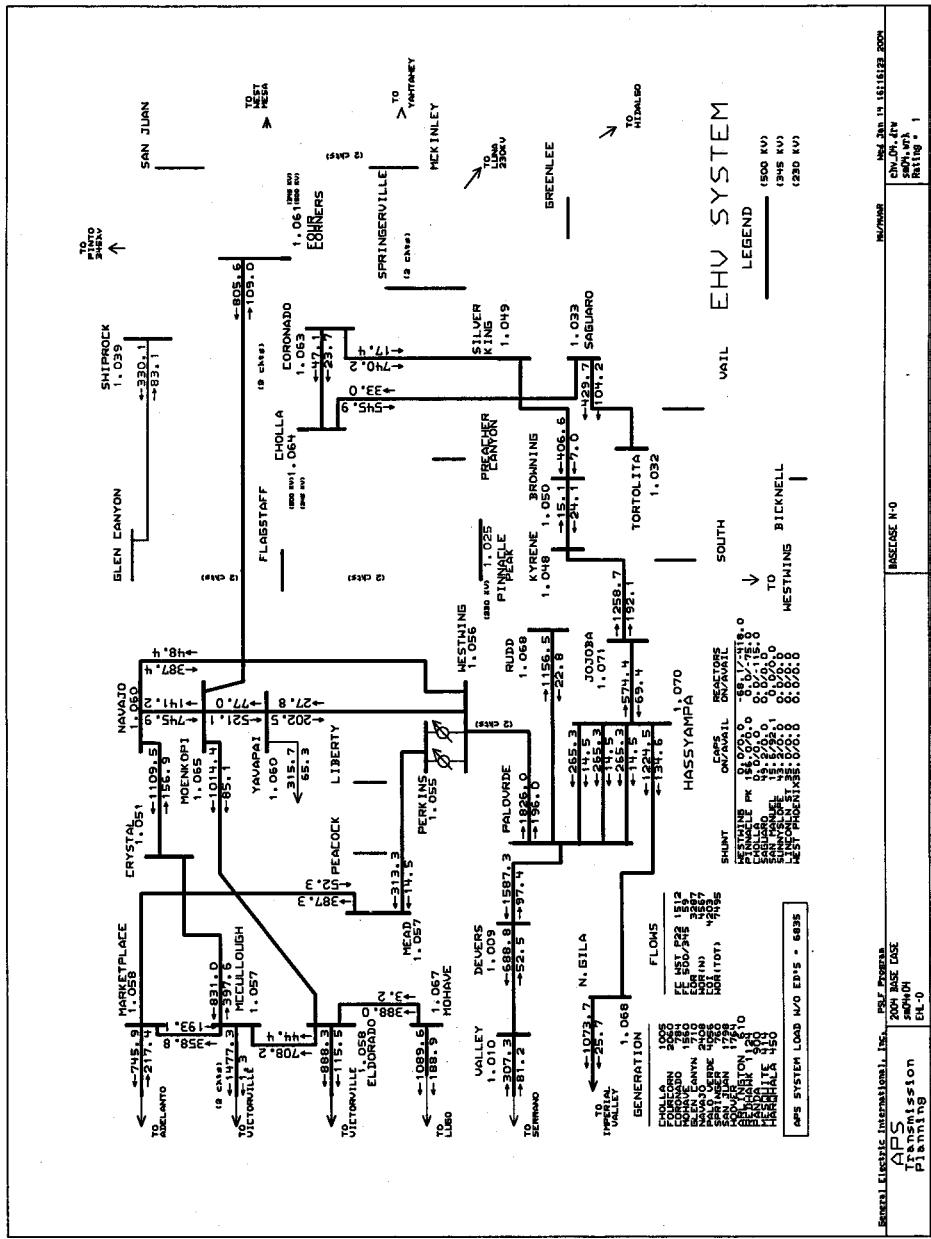
A stability simulation for simulated three-phase faults was performed for 2005 and 2012 for every 345kV or 500kV line that APS owns (totally or partially) or operates. It has been APS' experience that stability concerns do not manifest on the 230kV system, which is primarily designed to deliver power to load. Therefore, no 230kV simulations were performed. Additionally, every new proposed generation plant will be required to

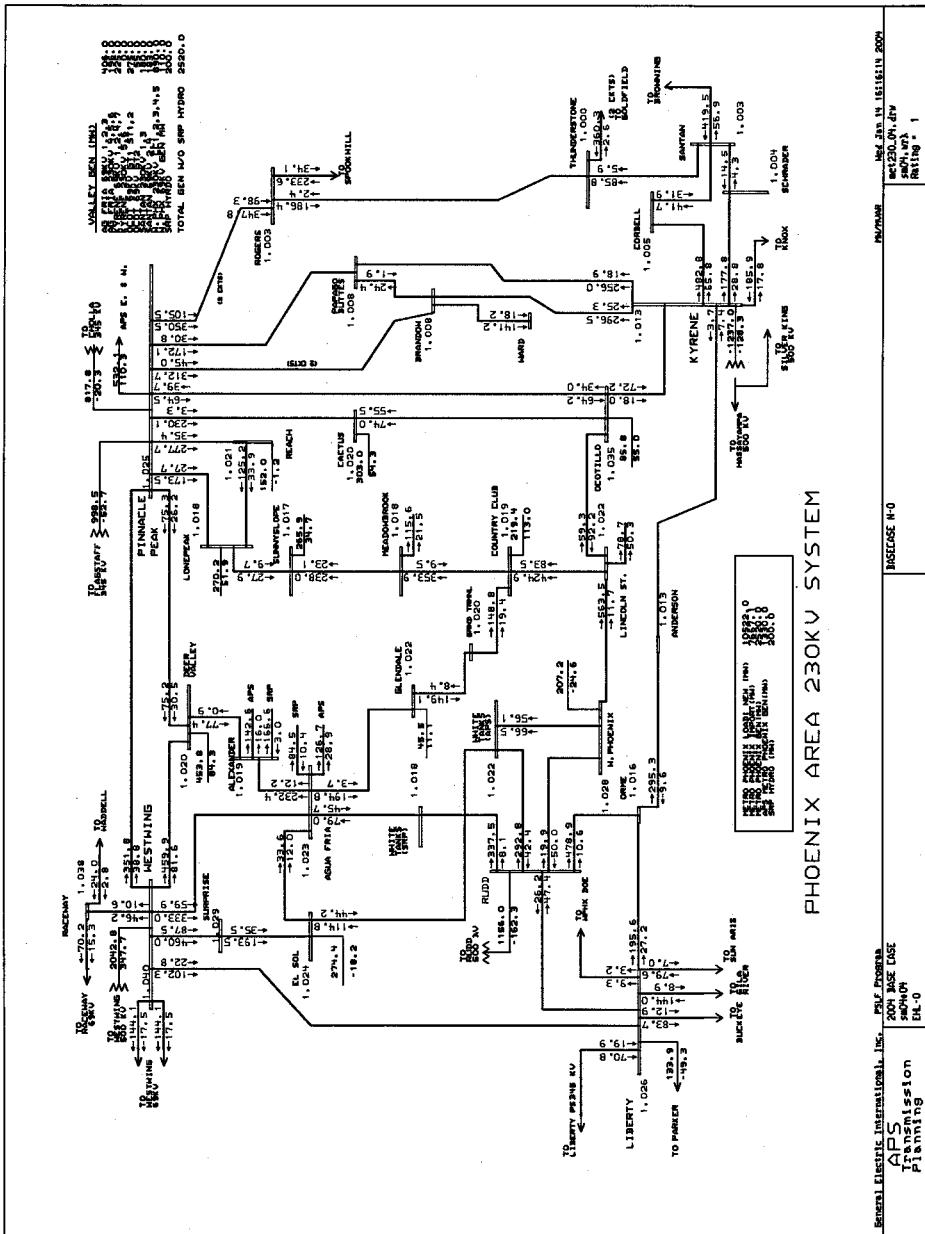
perform stability evaluations prior to receiving permission to interconnect to the transmission system.

Each simulation modeled a 3-phase bus fault, appropriate series capacitor flashing and reinsertion, and fault removal and transmission line removal. System performance was evaluated by monitoring representative generator rotor angles, bus voltages and system frequency. Plots of these system parameters are included in Appendix B. The stability simulations performed to date indicate that no stability problems limit the transmission system.

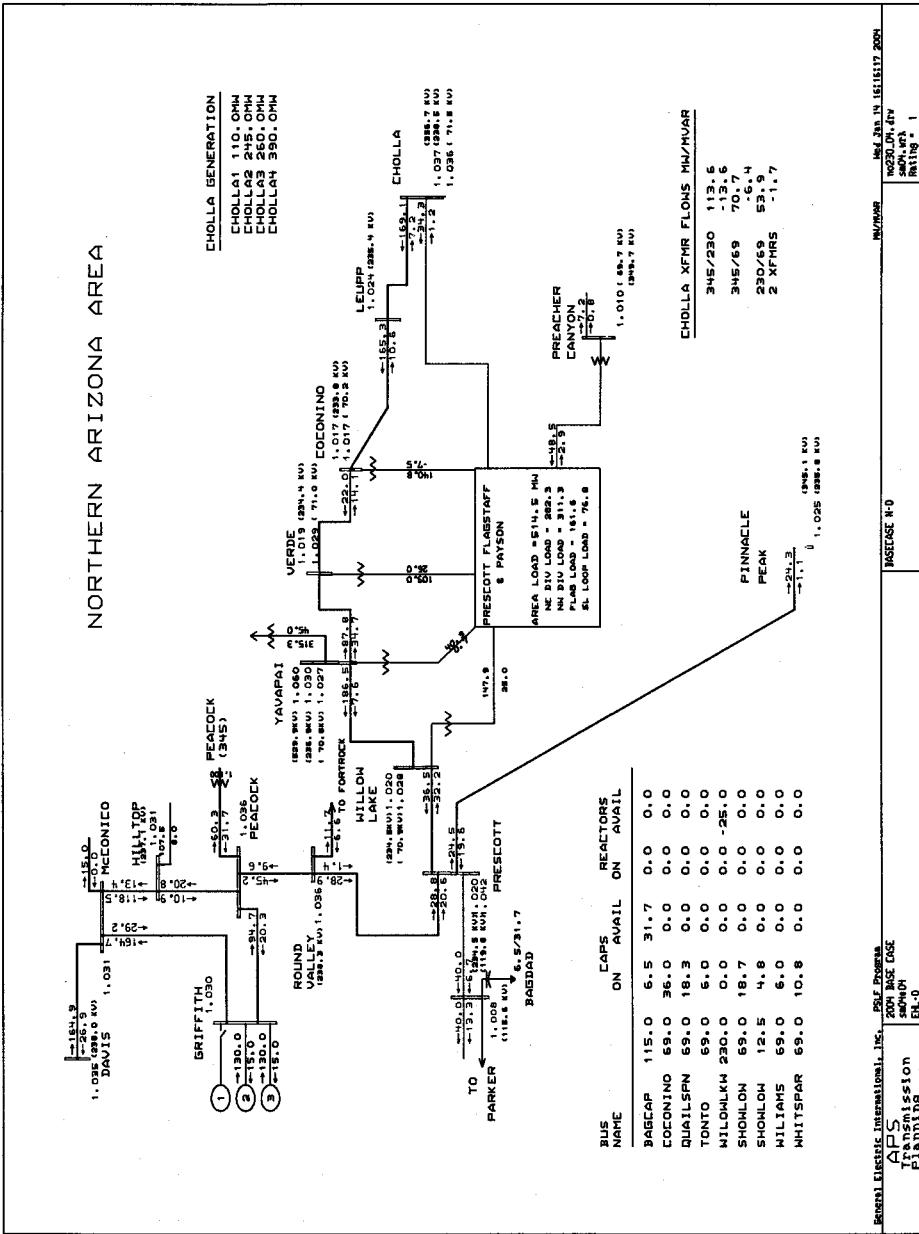
## **APPENDIX A**

### **Power Flow Maps**

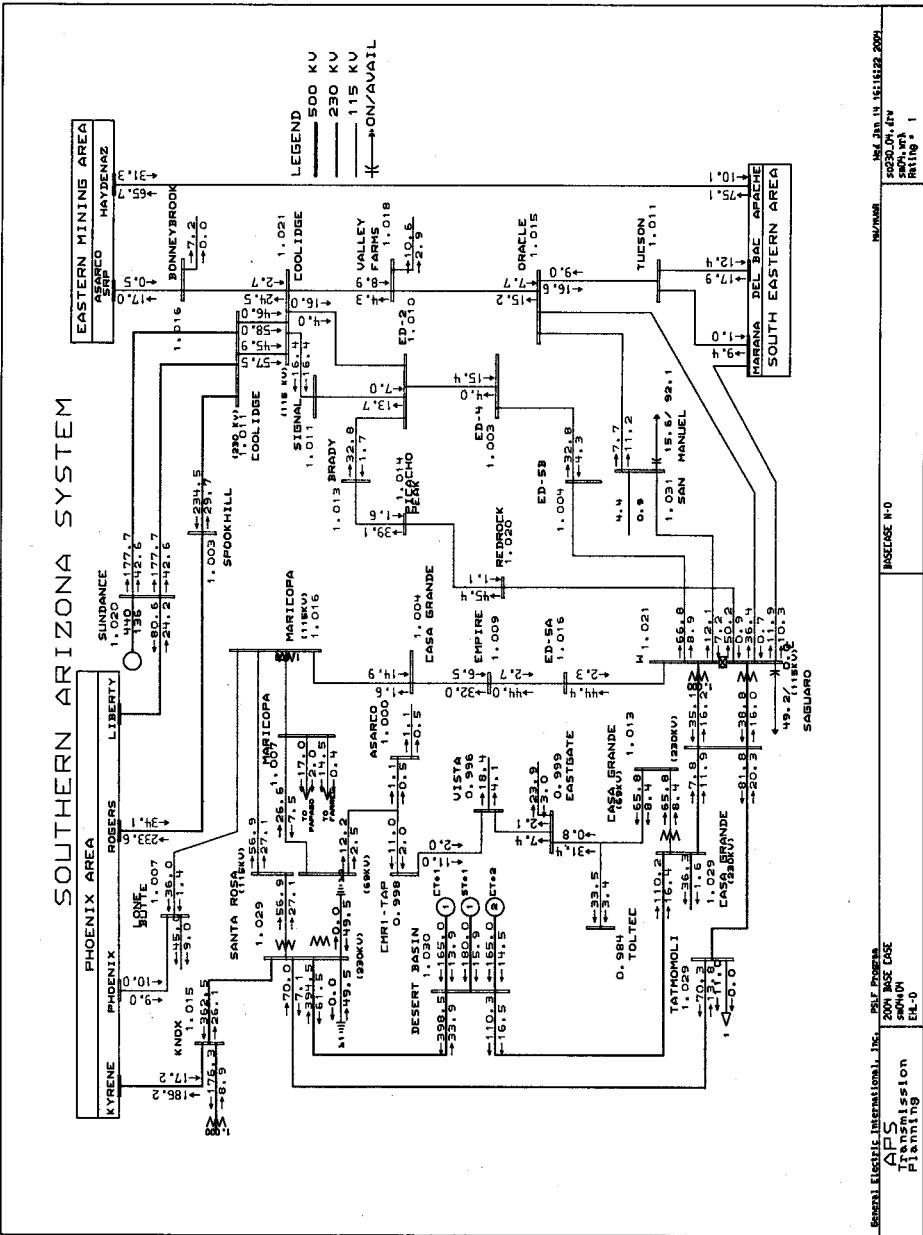


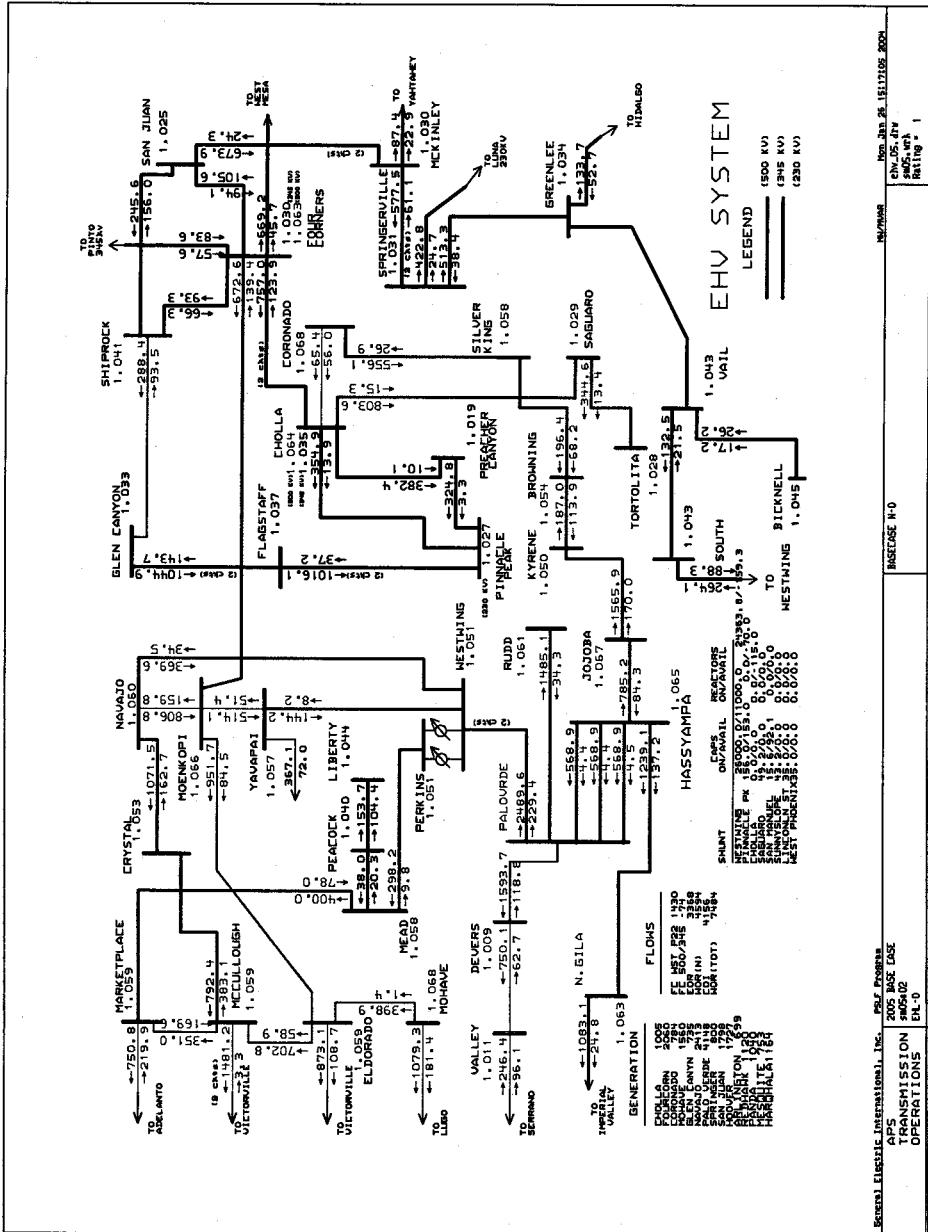


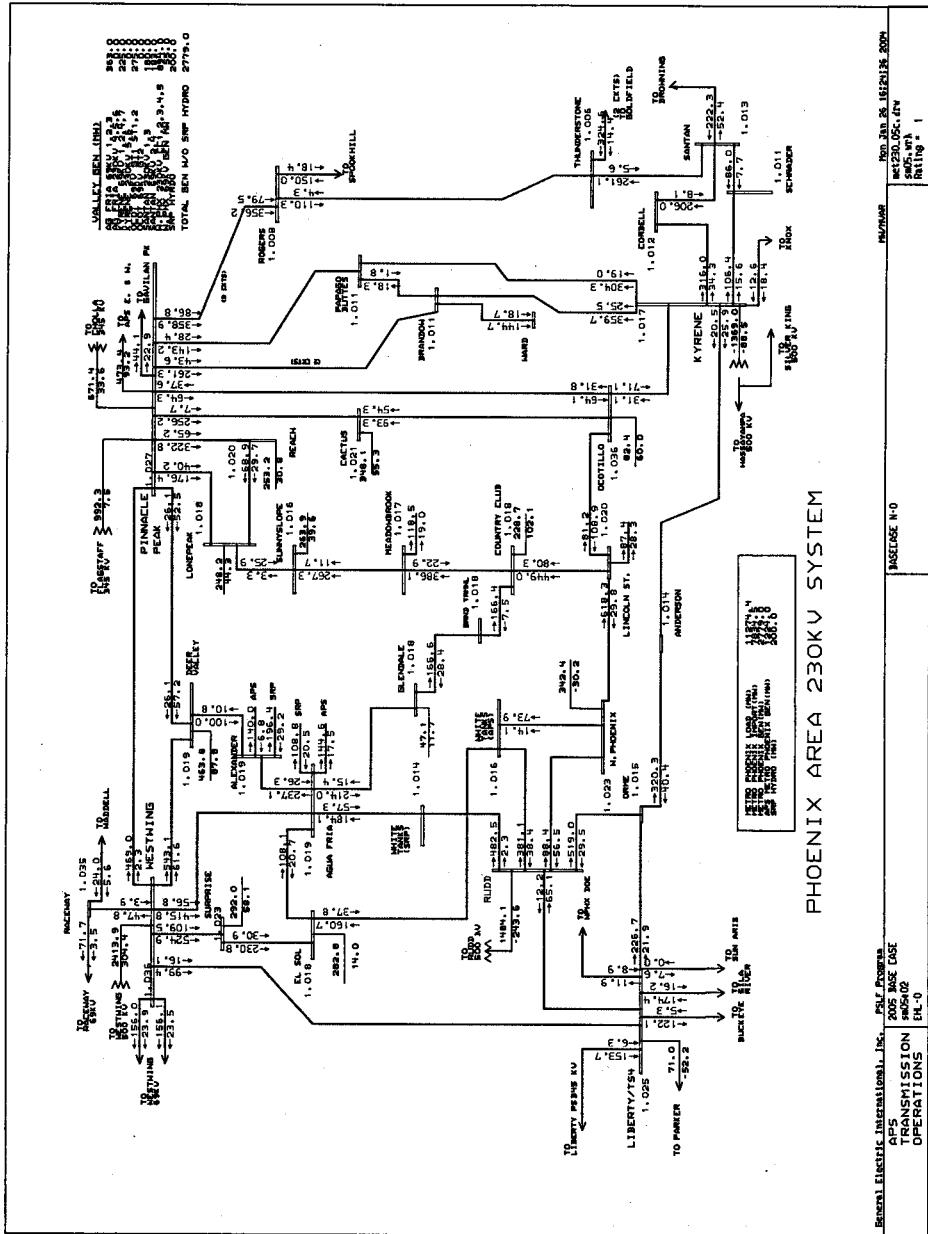
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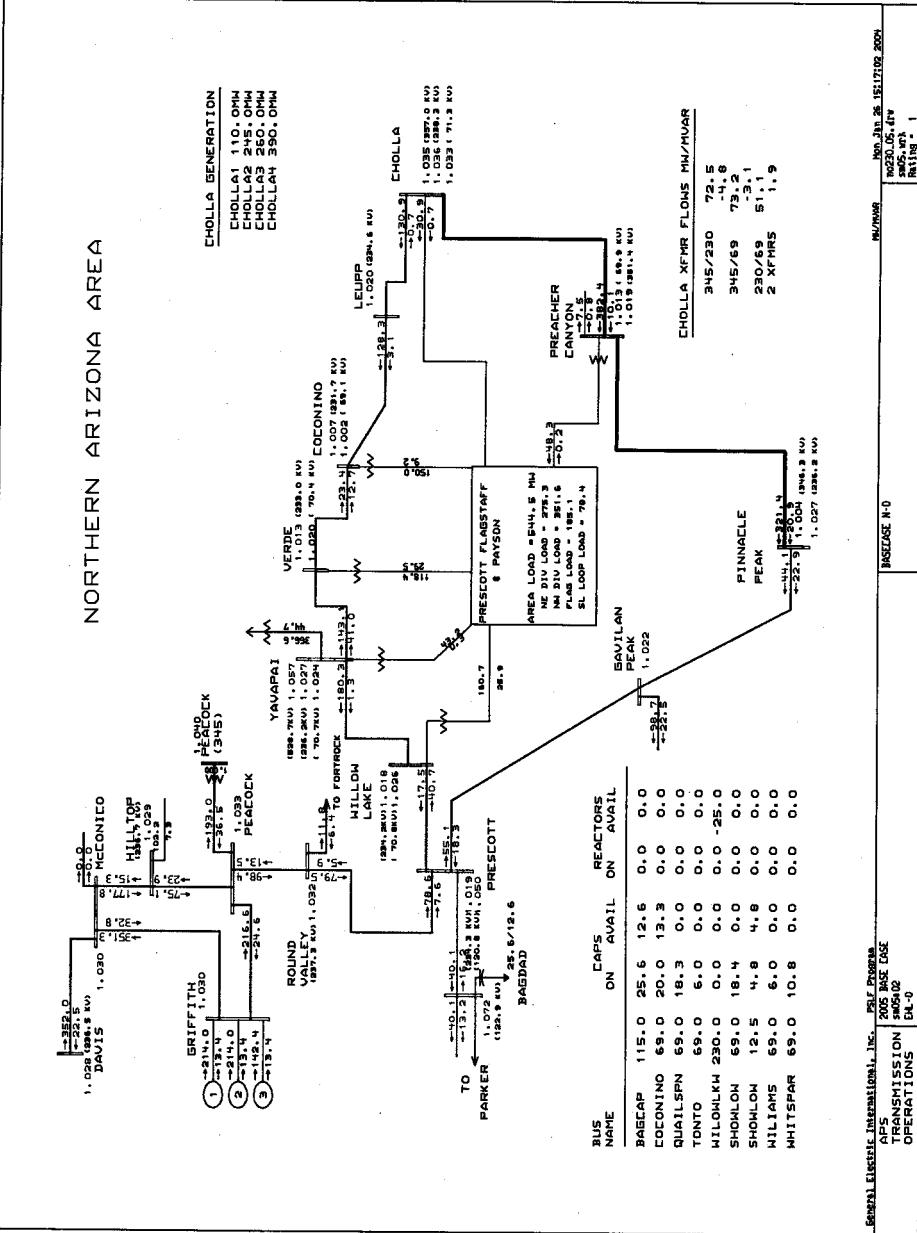
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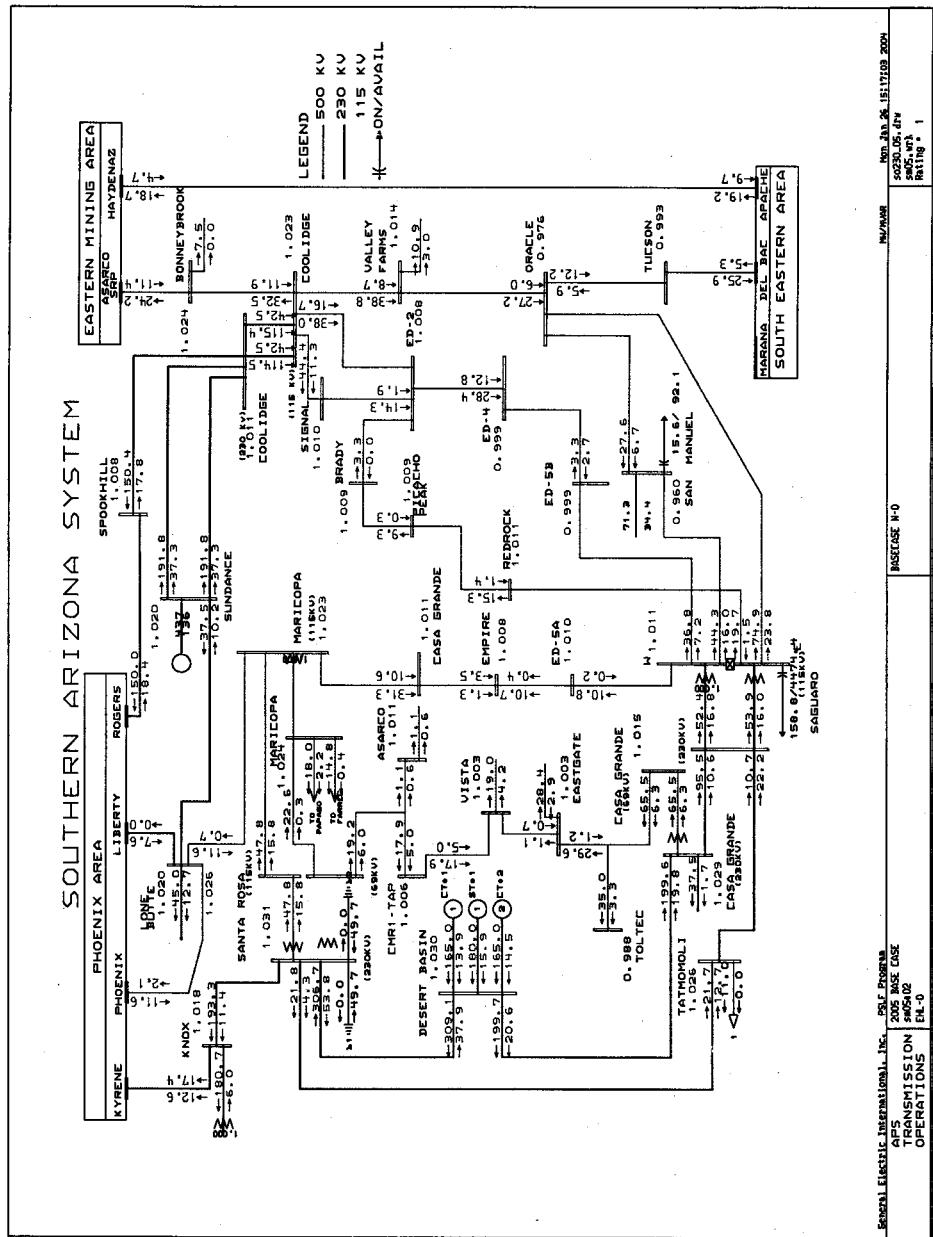


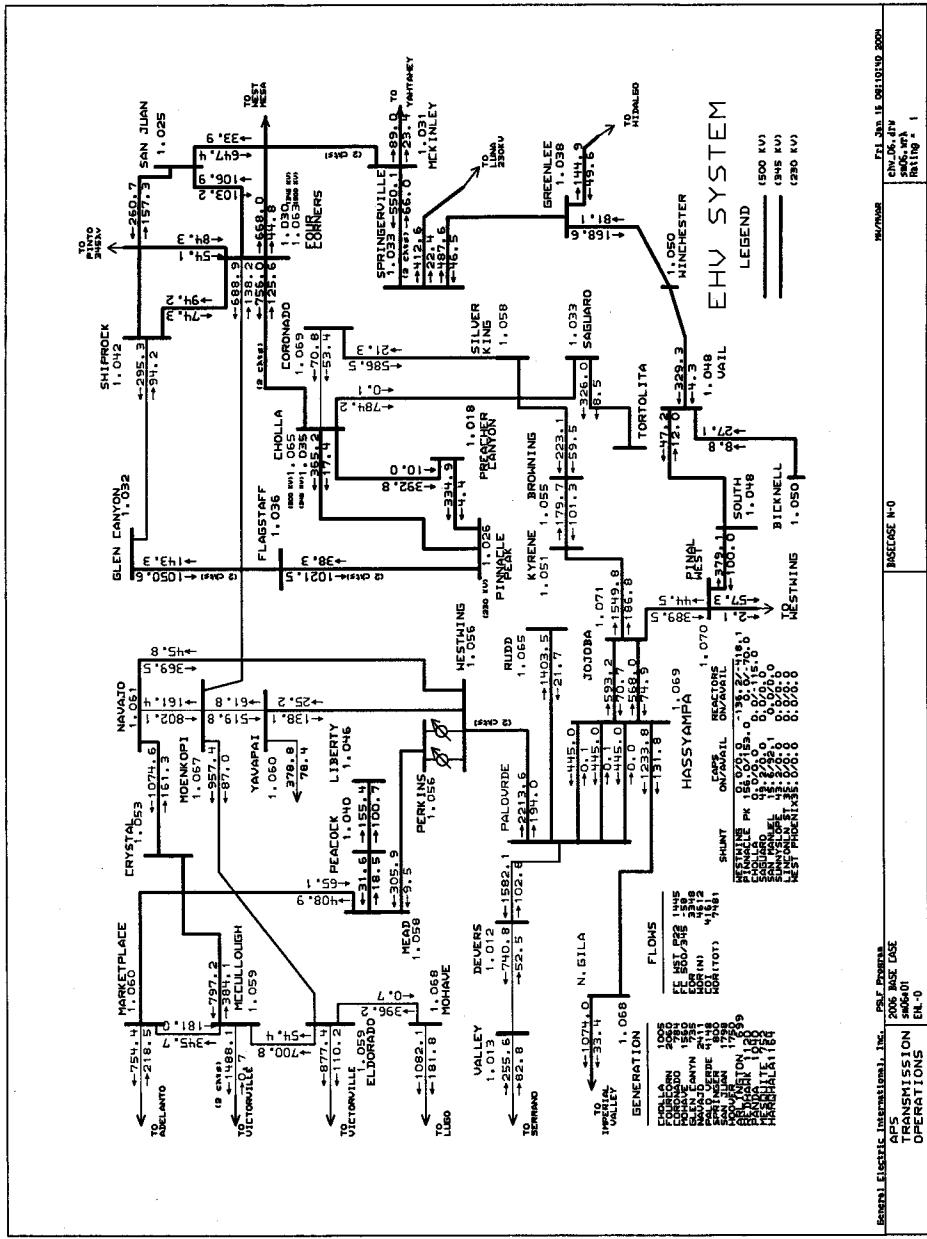


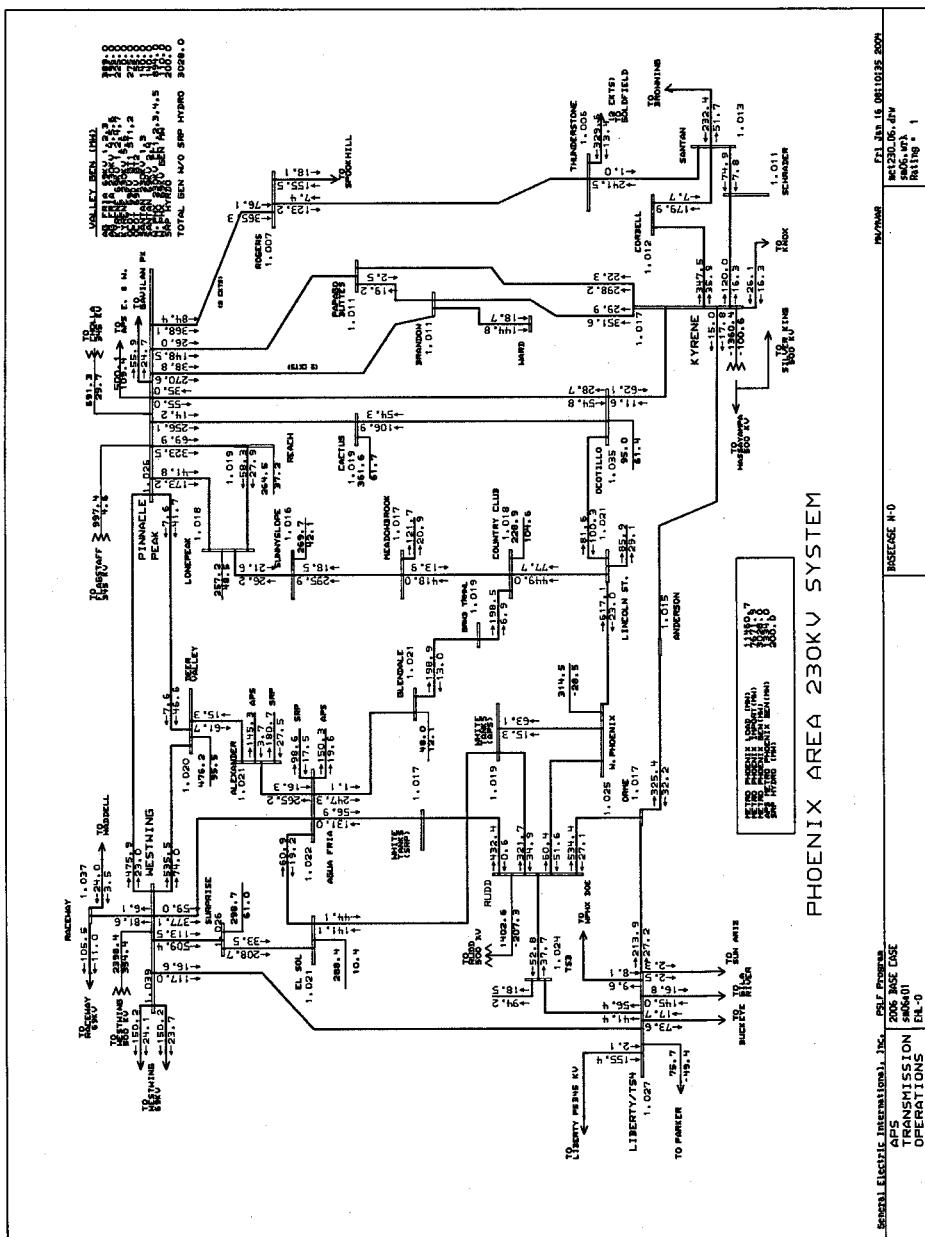


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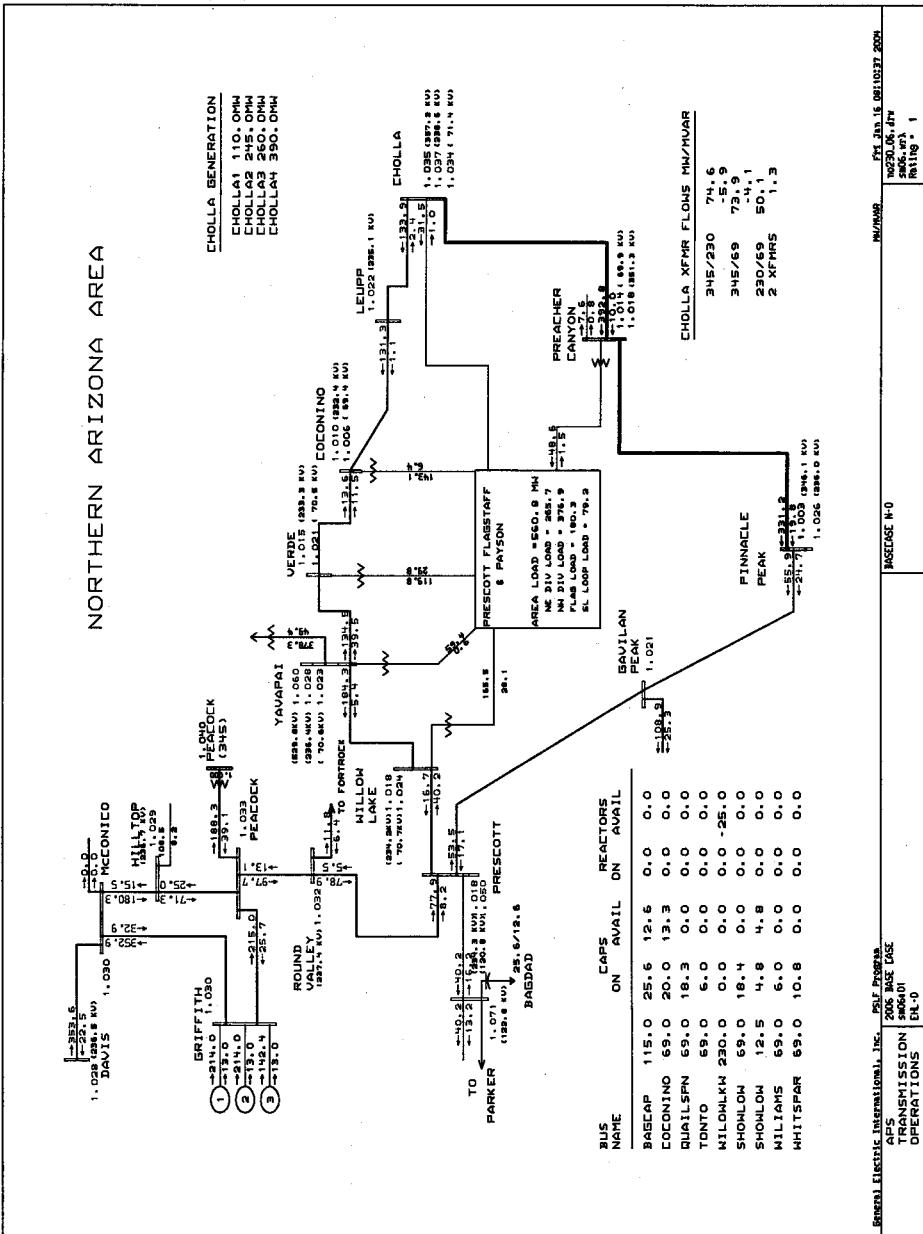






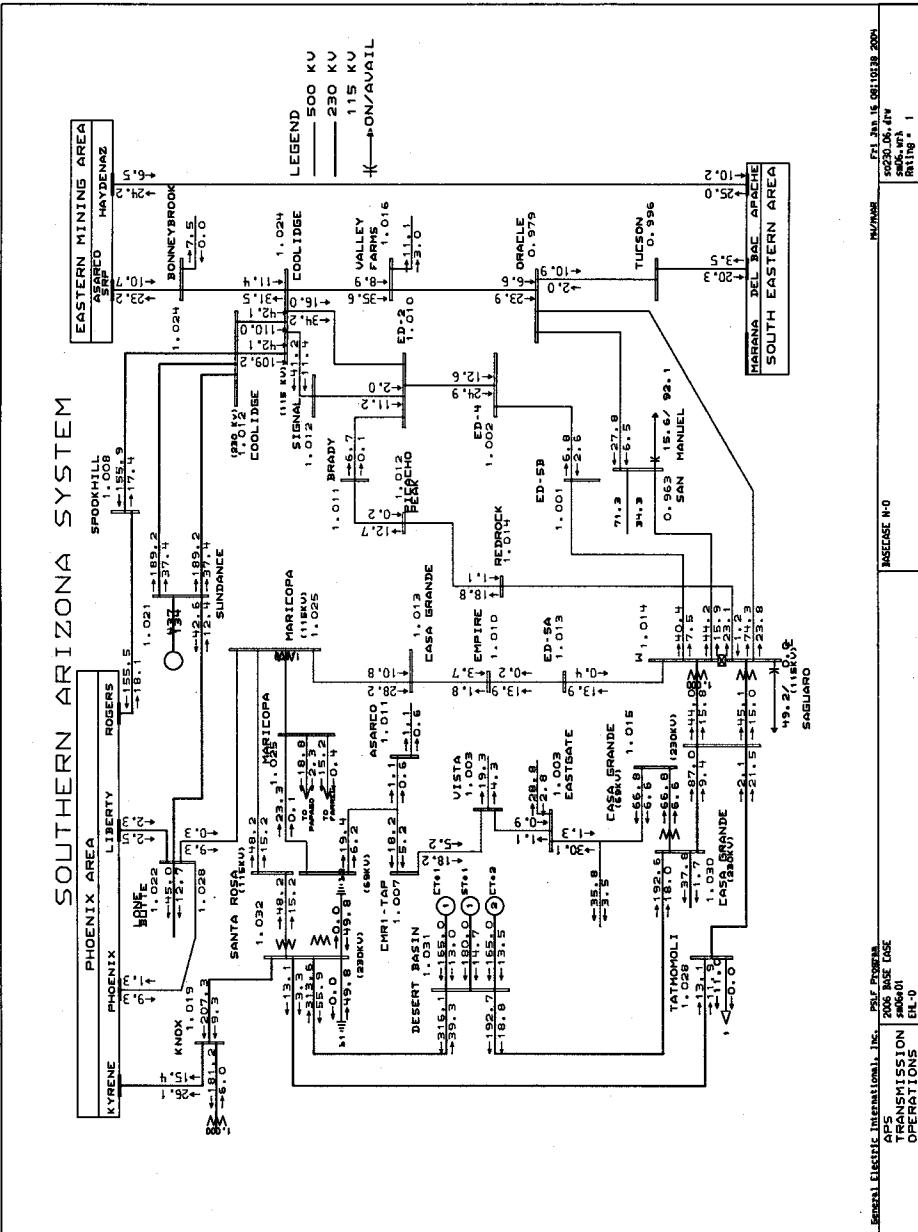


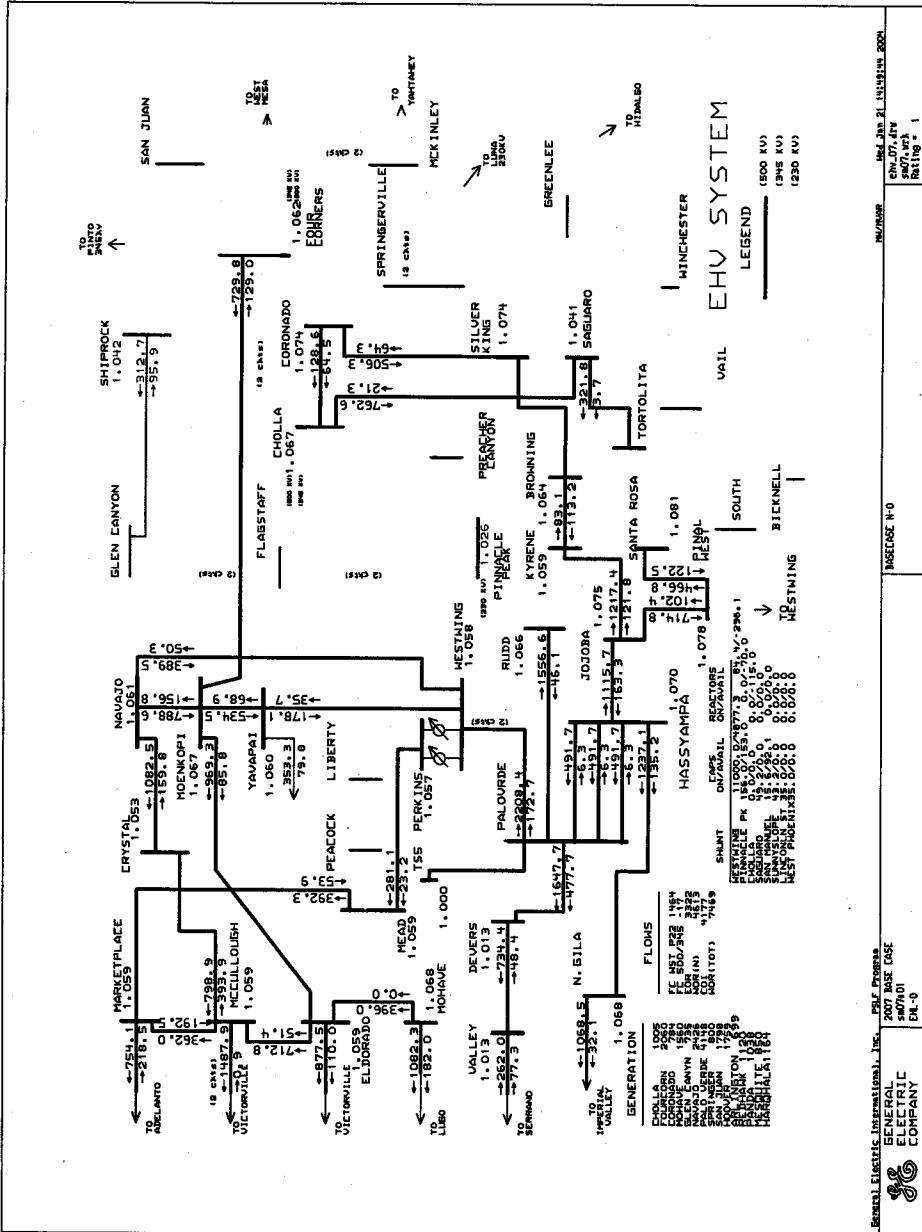
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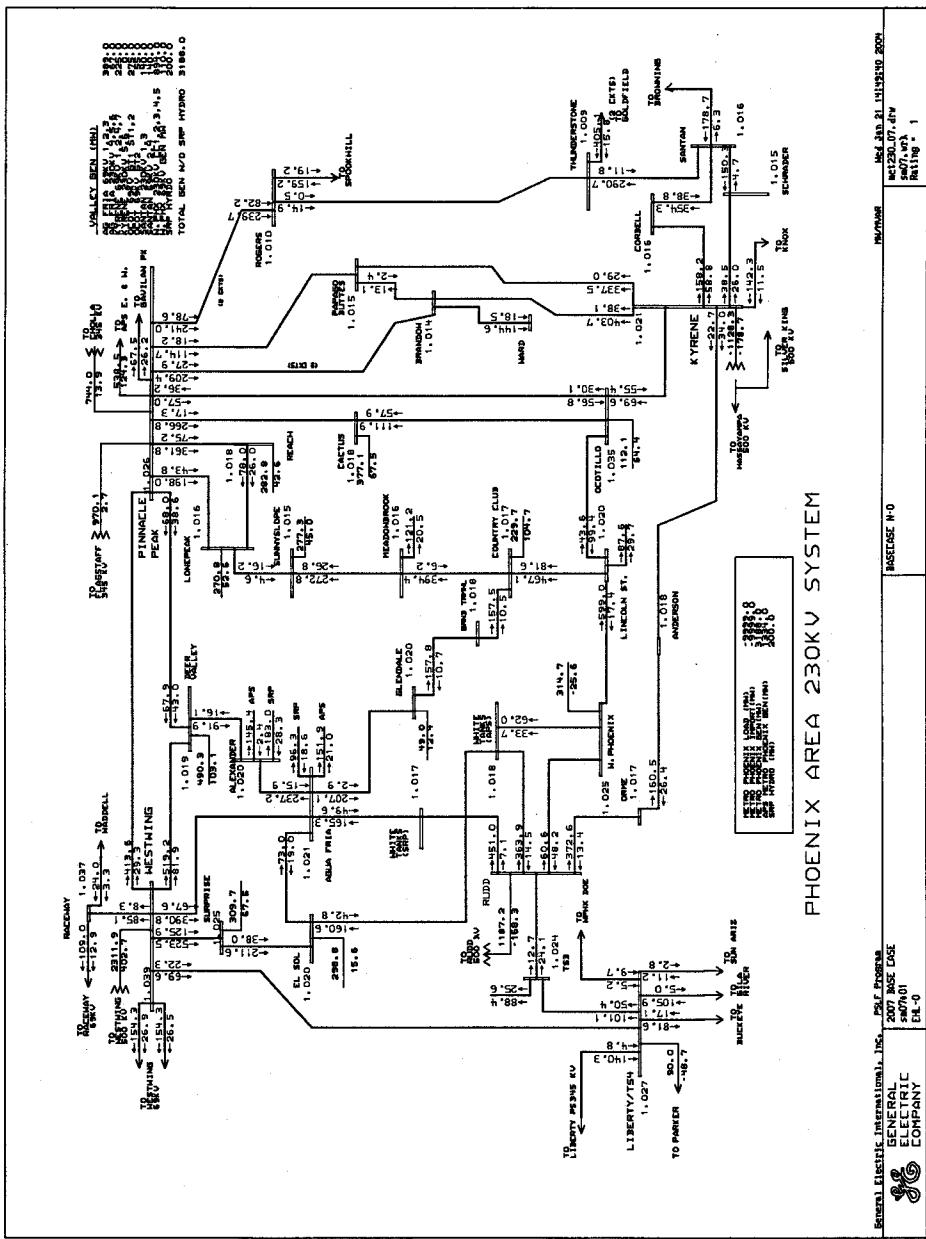


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GEF Phoenix  
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TRANSMISSION SYSTEM  
OPERATIONS  
ER-0

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2006, 16, 47v  
Solve #1  
Rating = 1



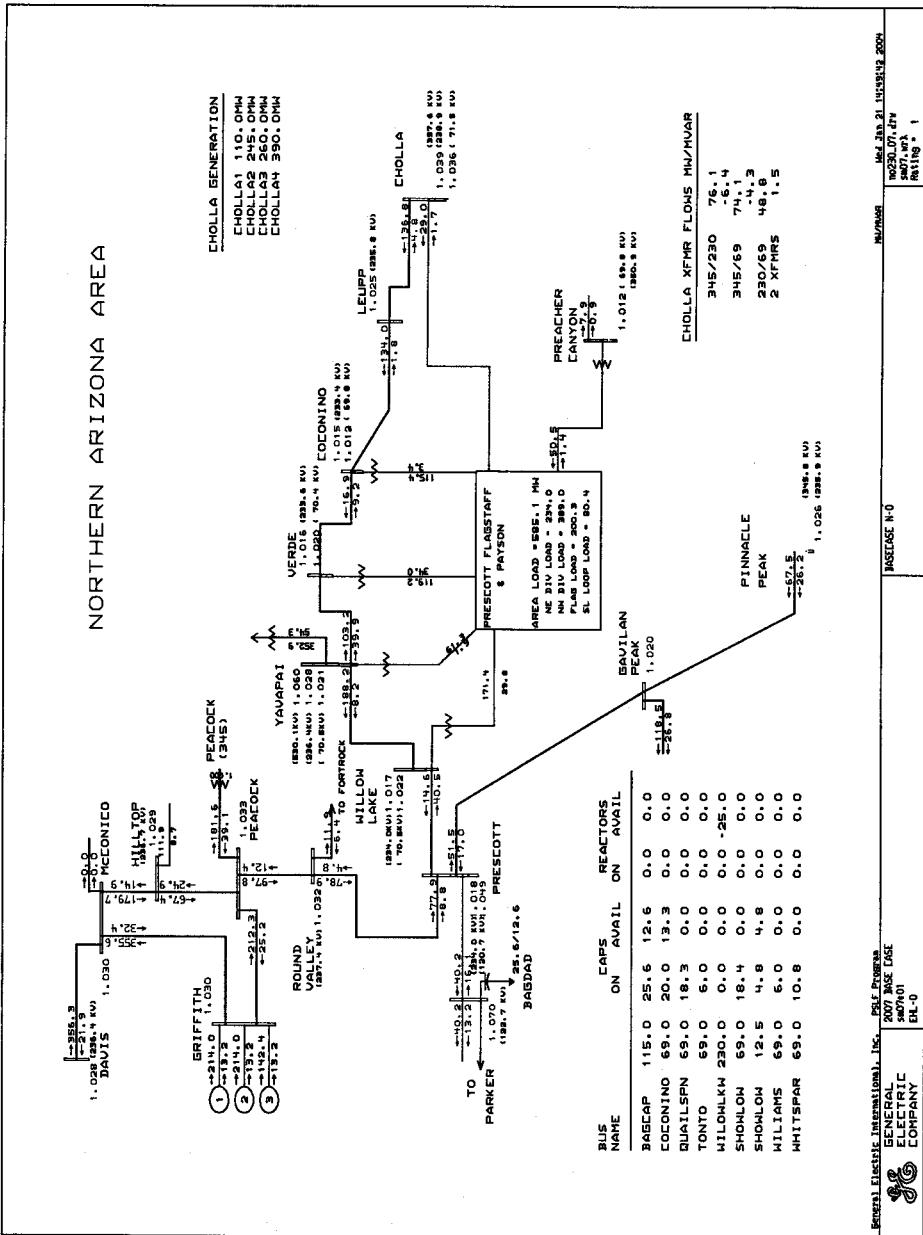




PHOENIX AREA 230KV SYSTEM

**General Electric International, Inc., P.G.E. Programs**

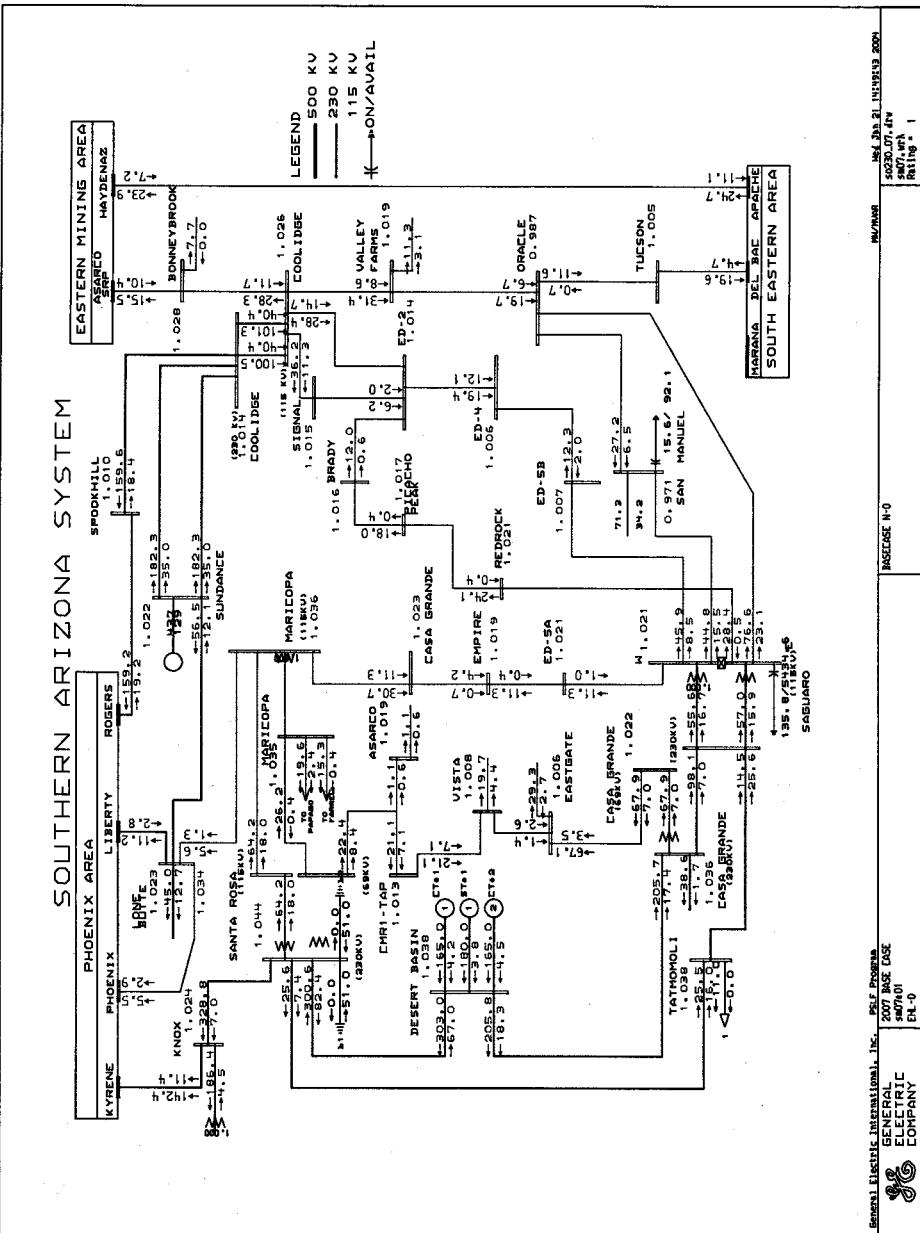
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	SM0701
	EN-0



General Electric International, Inc.  
GE Power Generation  
GENERAL ELECTRIC COMPANY  
2007 BASE CASE  
SAFETY  
EL-0

RELEASE N-0

INTERFAZ  
Rev. Jan. 21, 1995/96/97/98/2000  
No. 200, 07/07/98  
Rating = 1



General Electric International, Inc. GE Power  
GENERAL ELECTRIC COMPANY  
© 2007 GE Power  
E&I  
E&I  
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Rev. D, 21-Nov-2004

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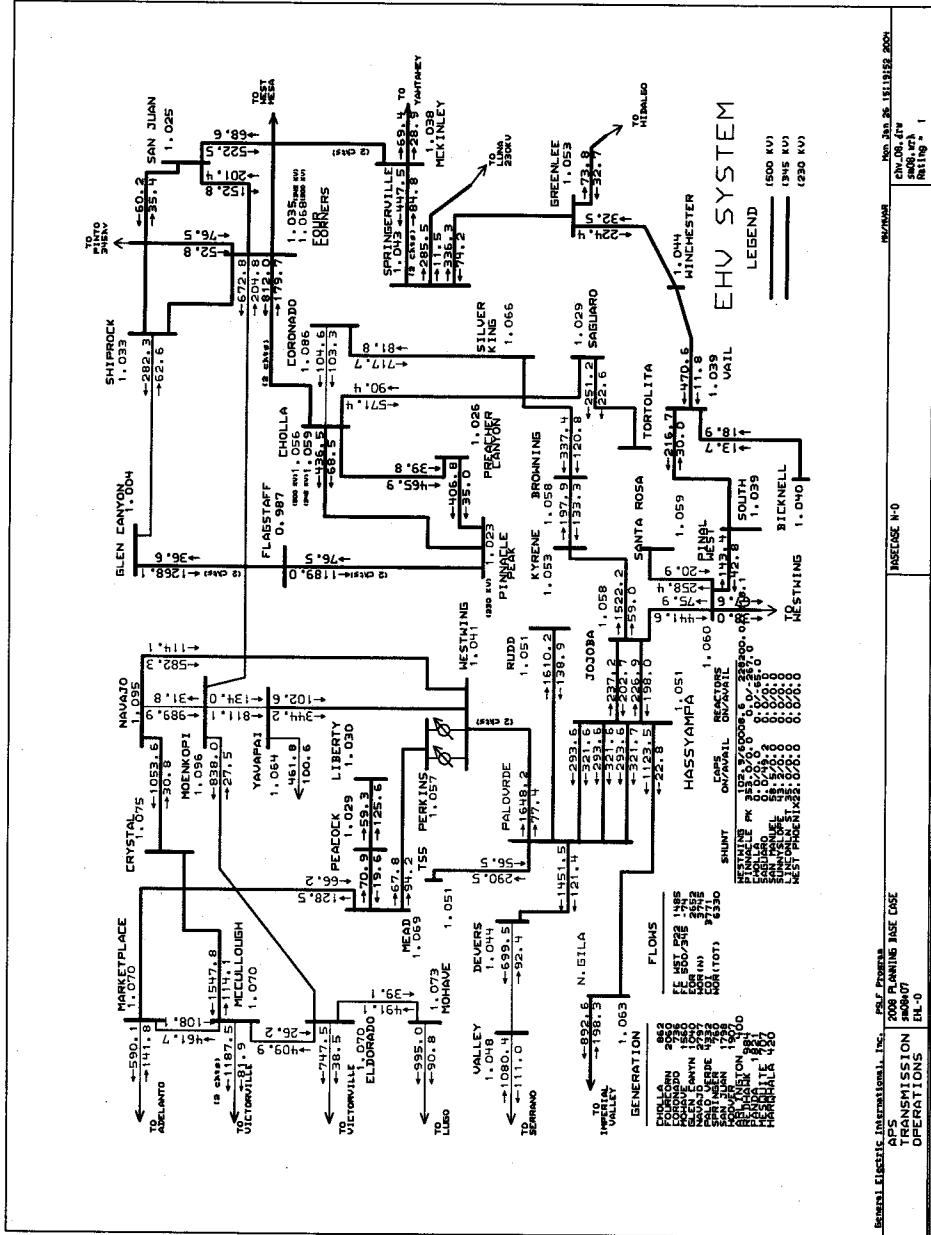
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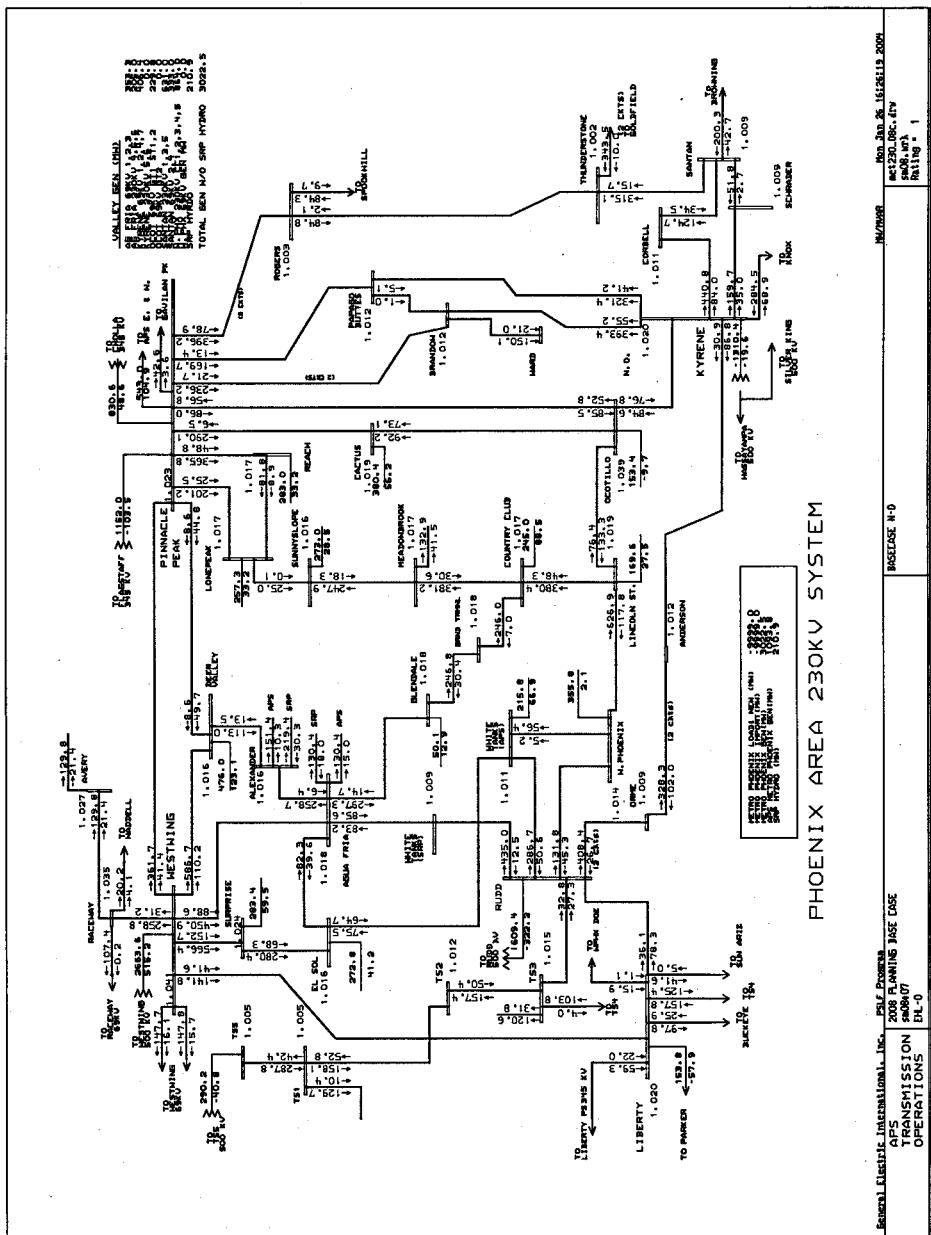
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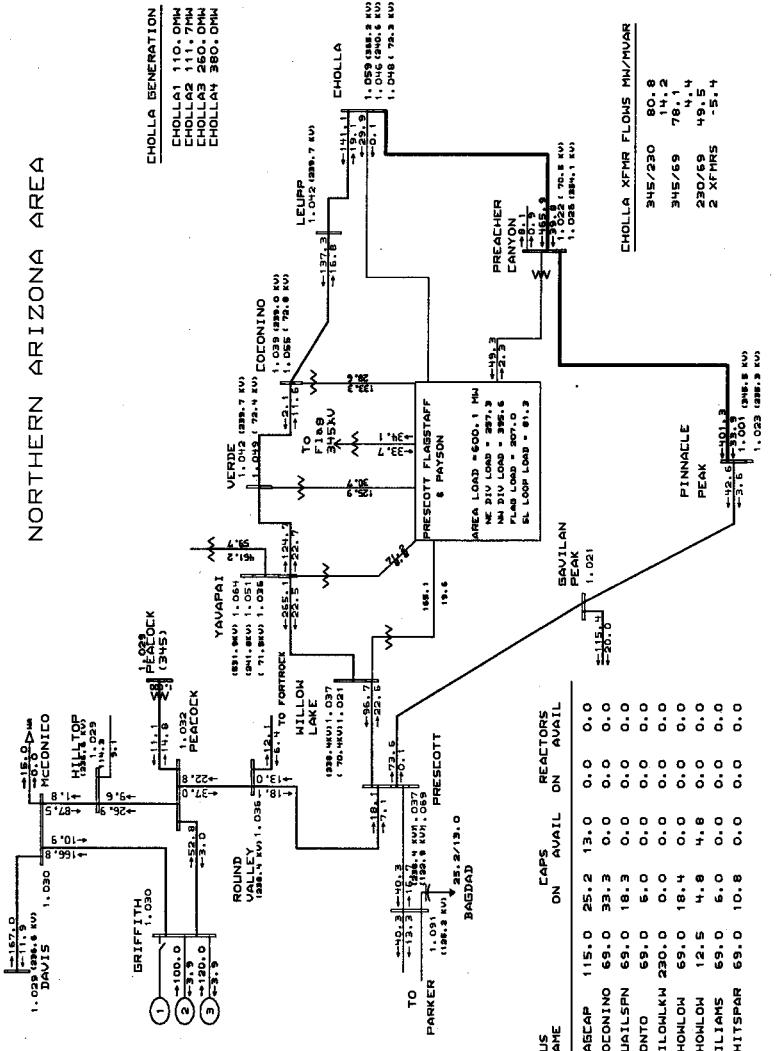
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NORTHERN ARIZONA AREA



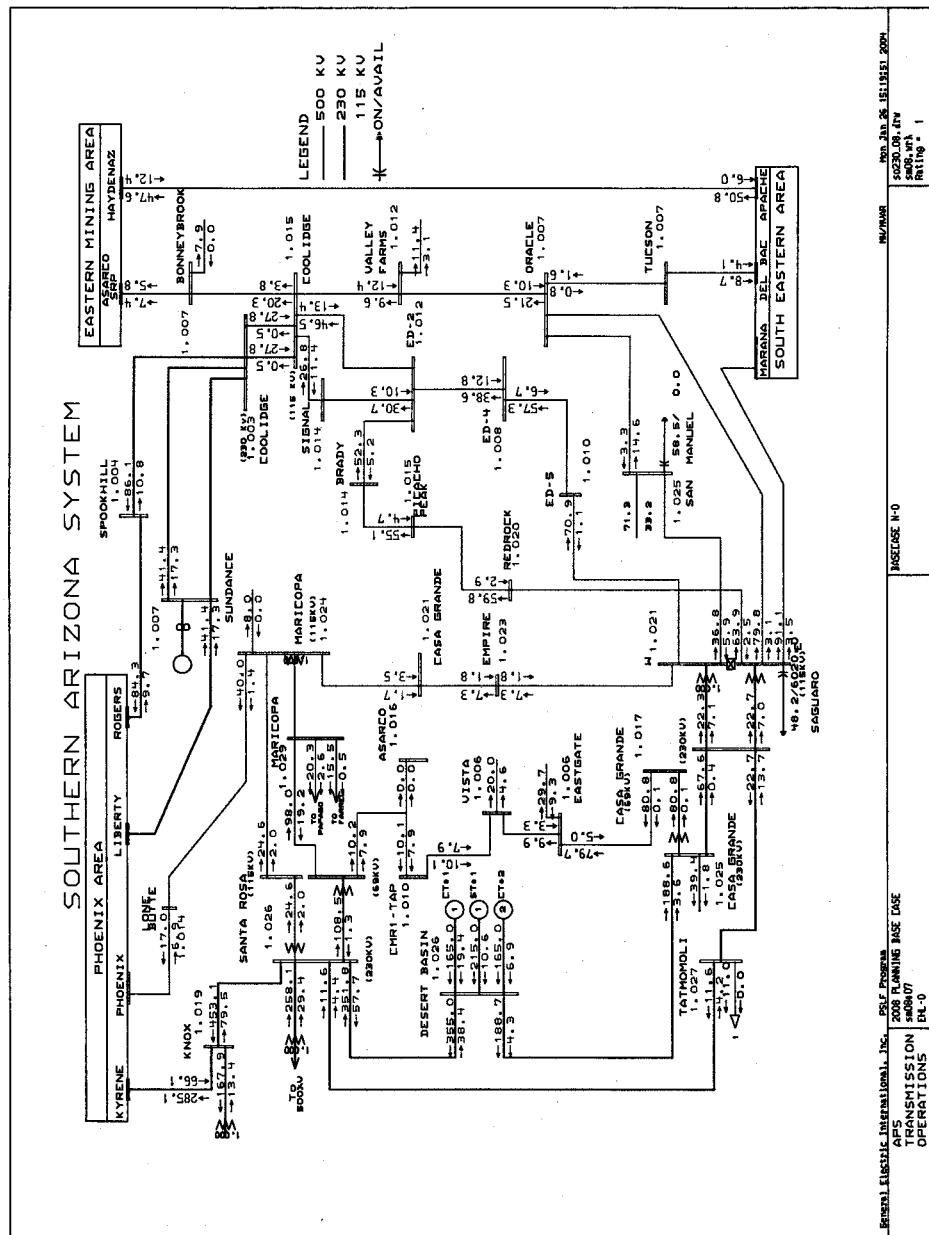
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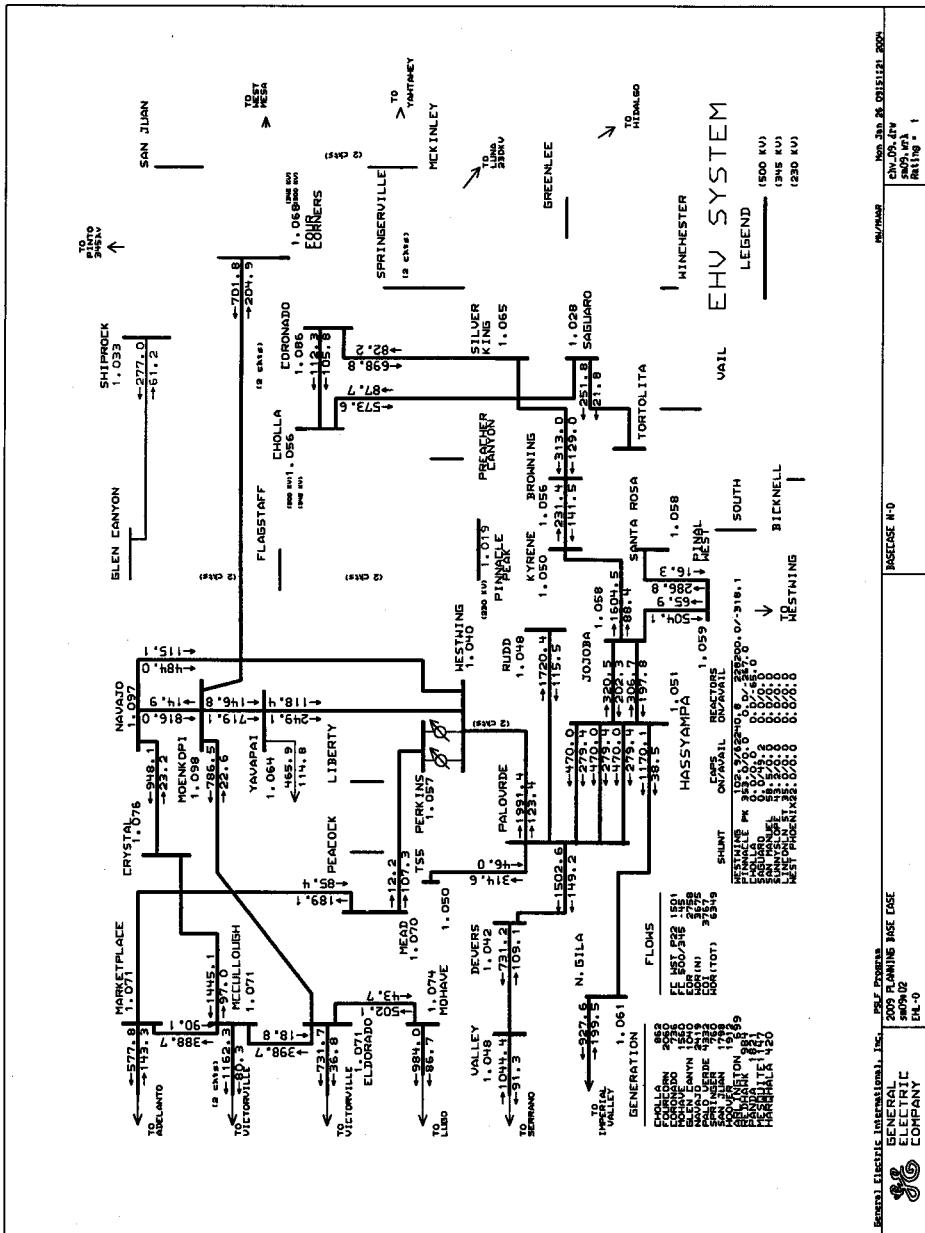
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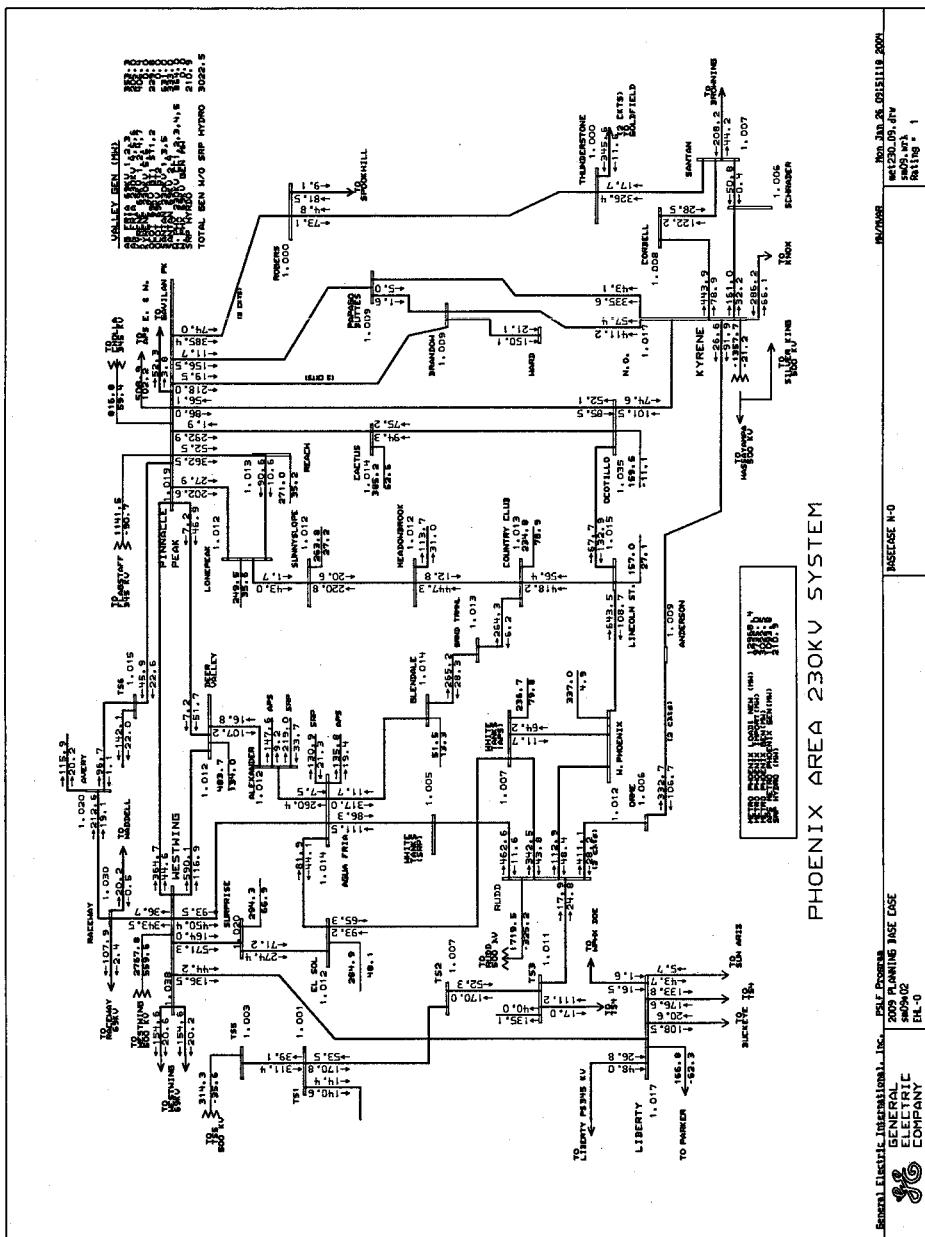
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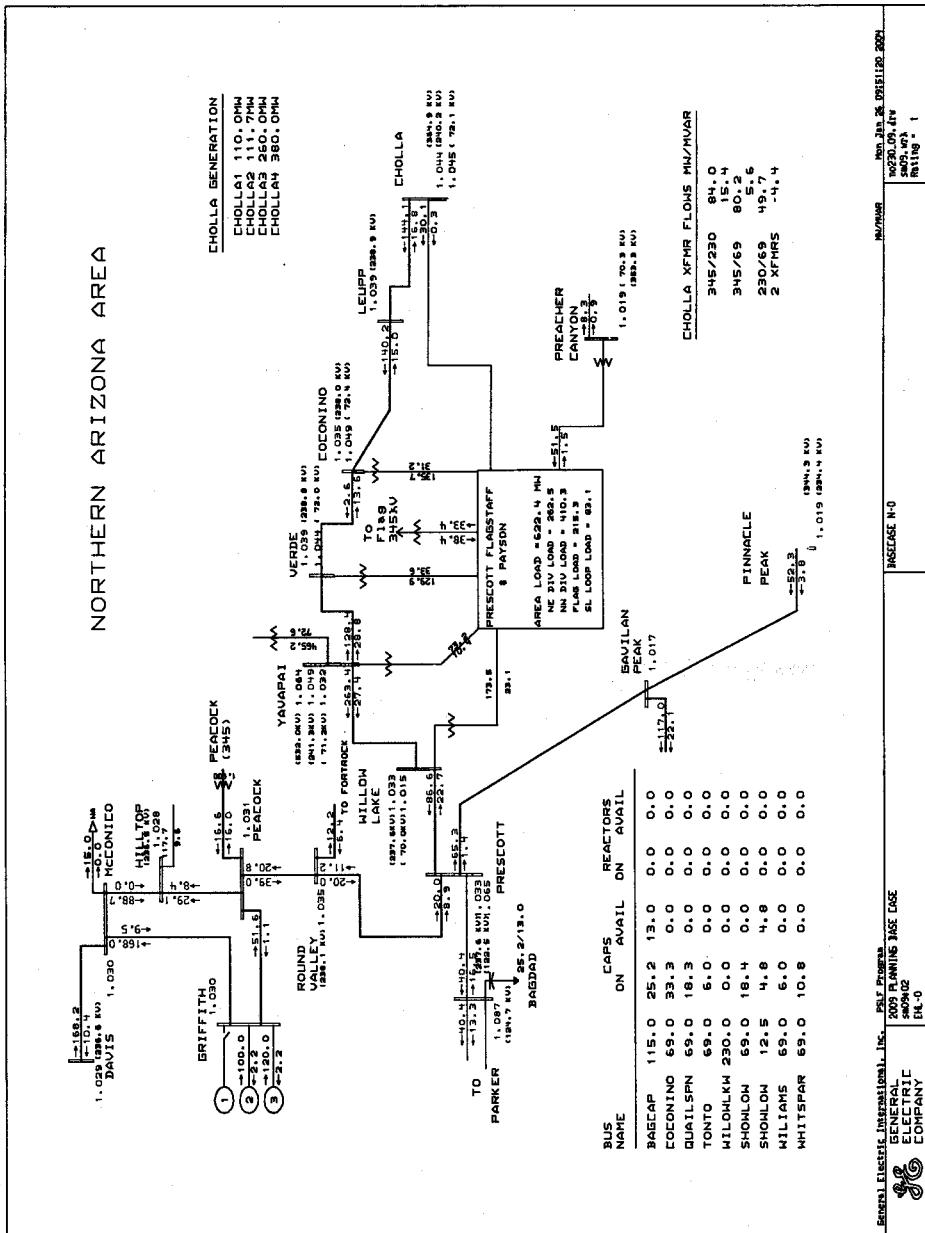
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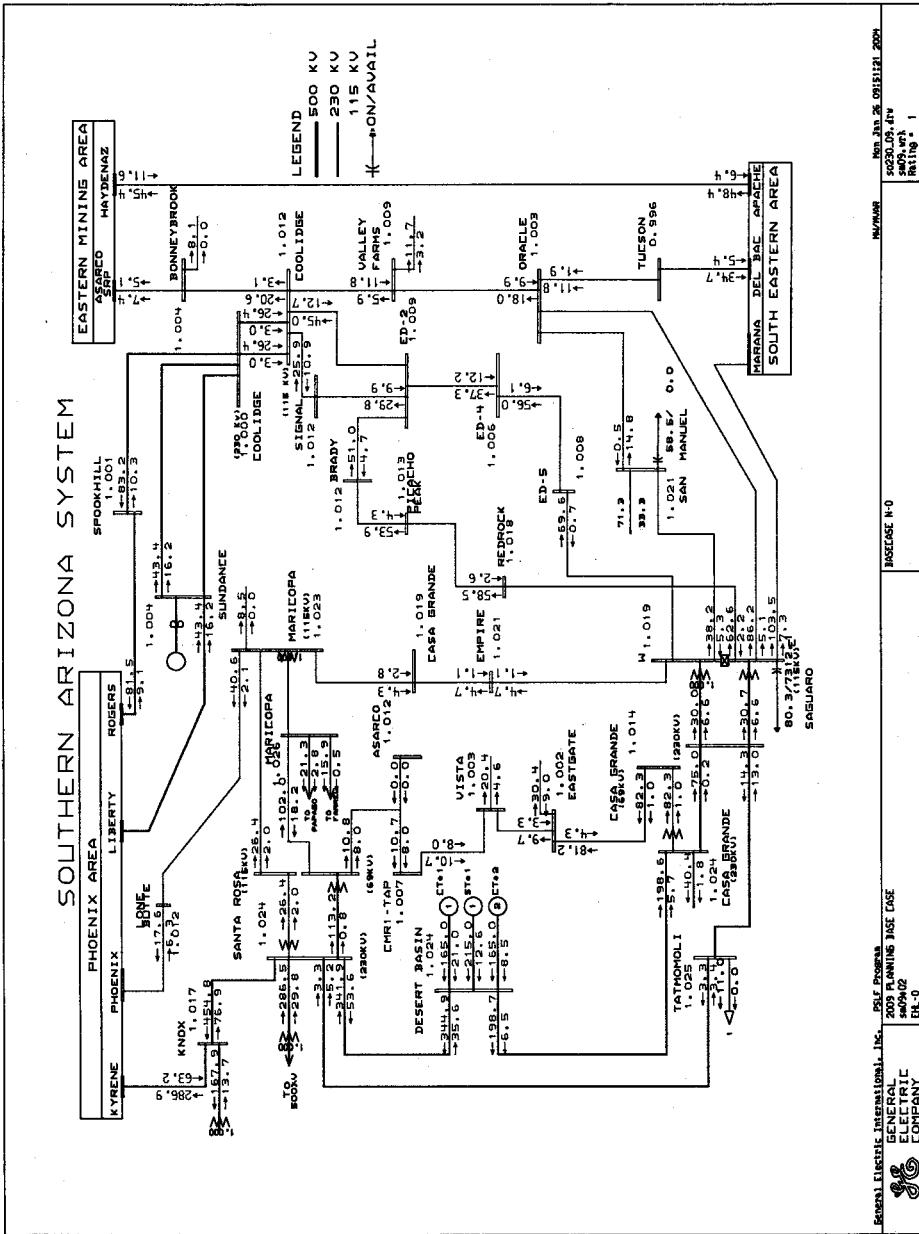






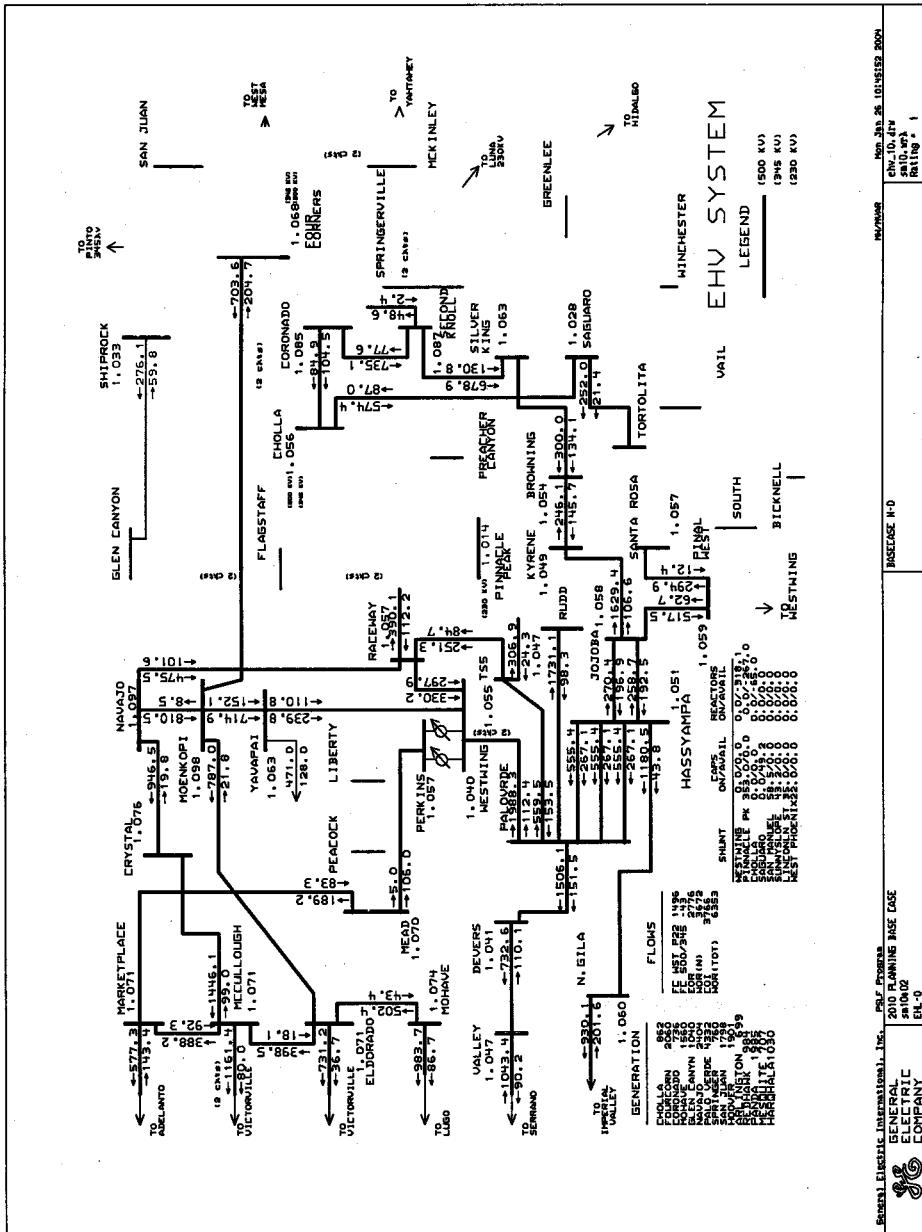


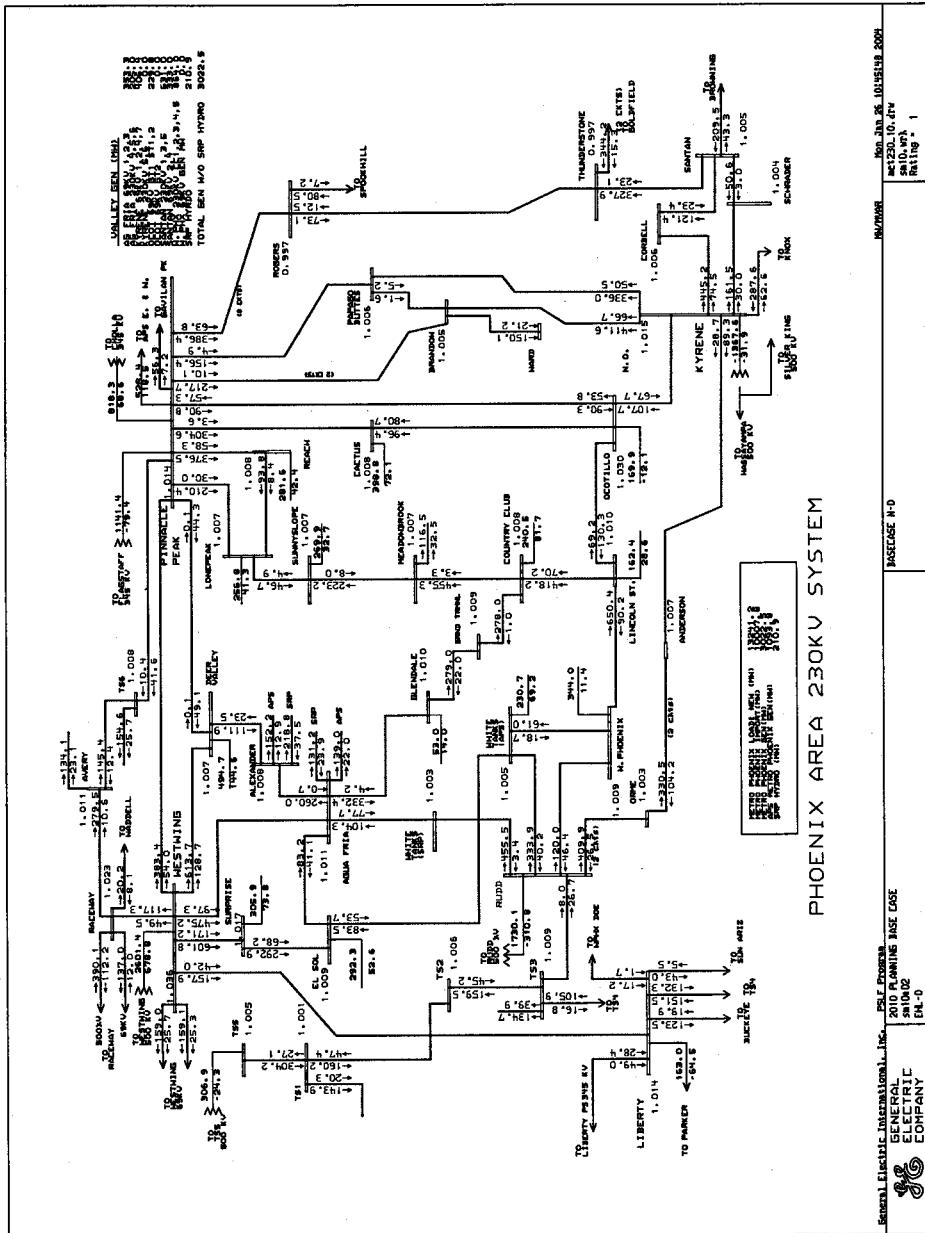
SOUTHERN ARIZONA SYSTEM



**General Electric International, Inc.** PSLF Program  
**GENERAL** 2009 PLANNING  
**ELECTRIC** 2009-02  
**COMPANY** EH-0  


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External Electric International, Inc.  
P.O. Box 26101518-2004  
2010 PLANNING BASE CASE  
SOL02  
EL-0

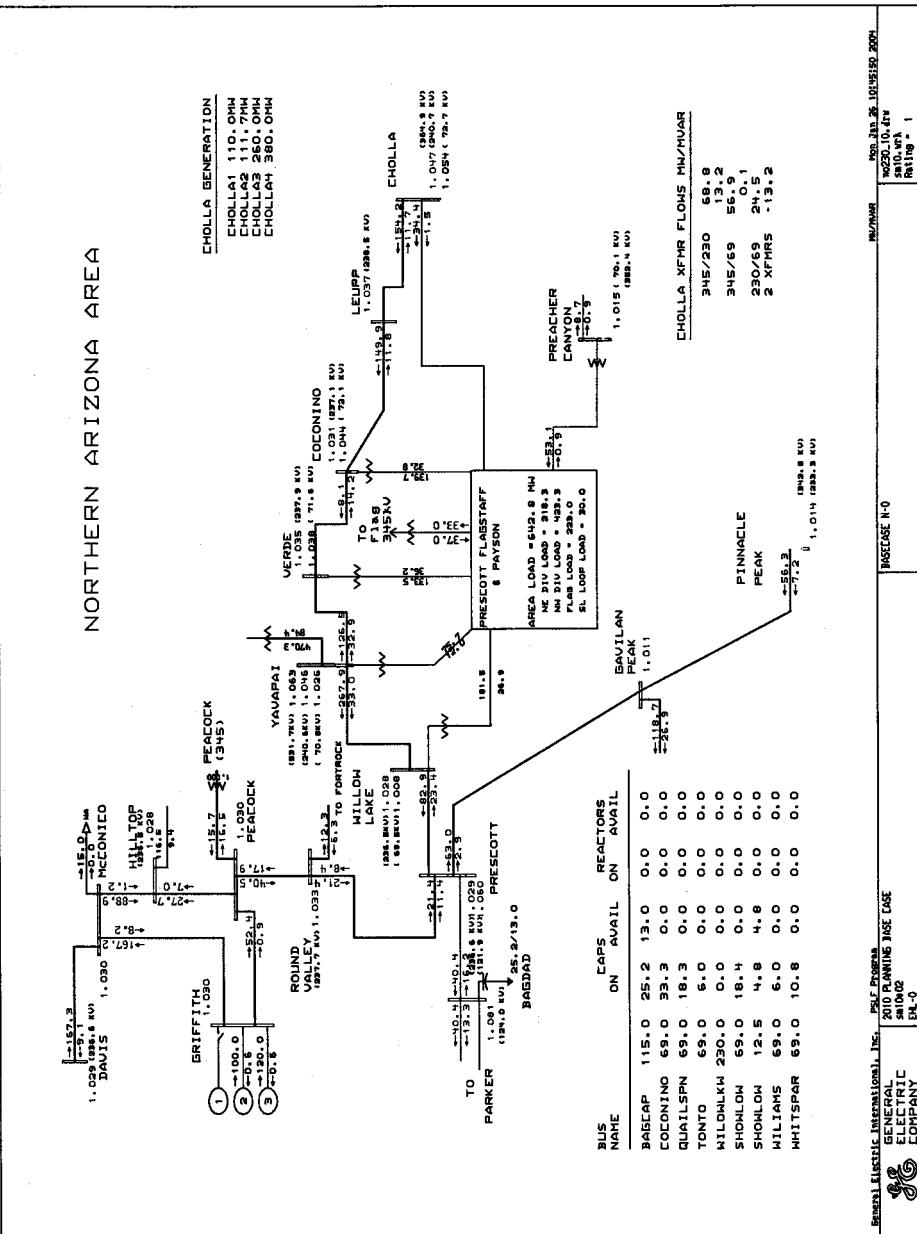
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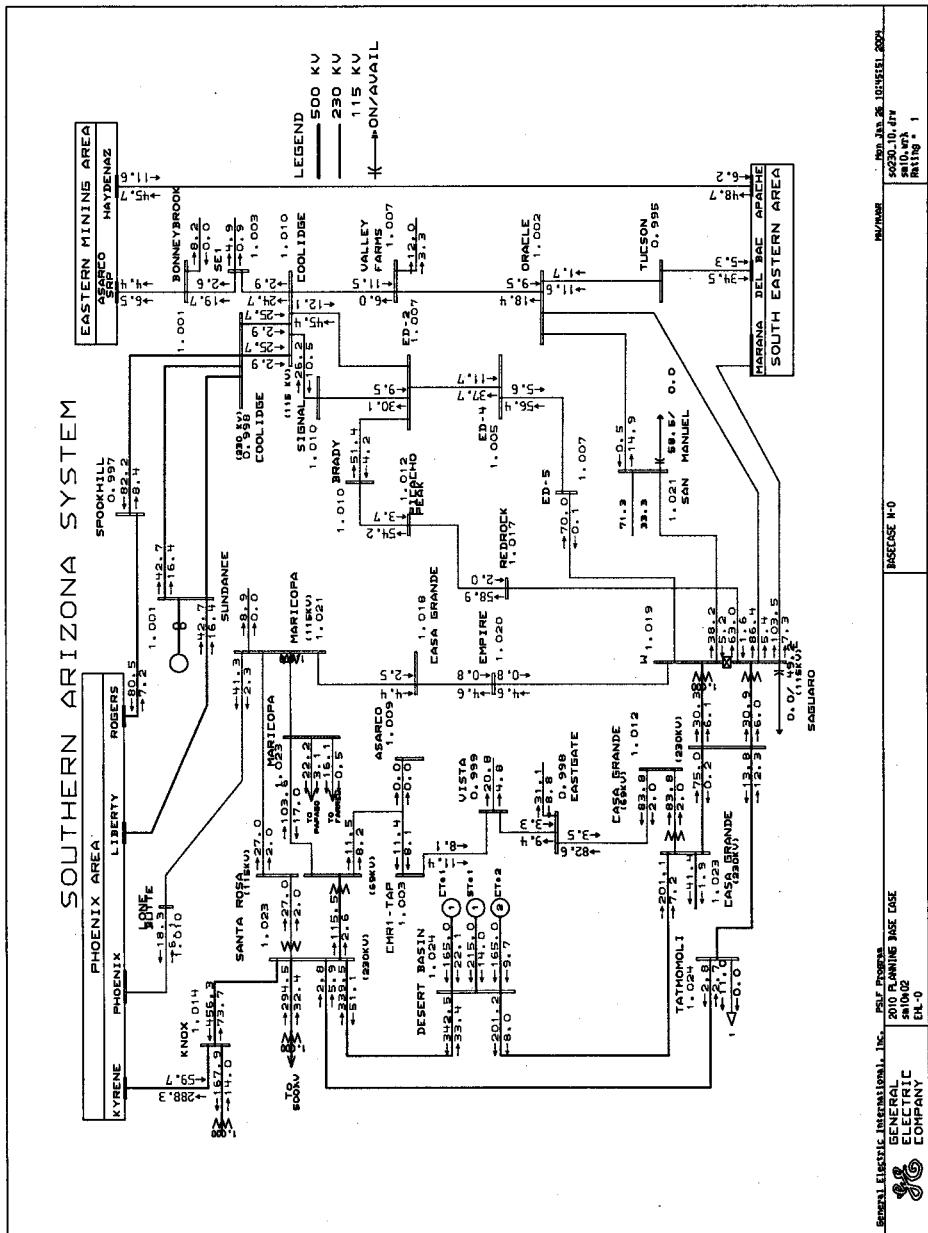
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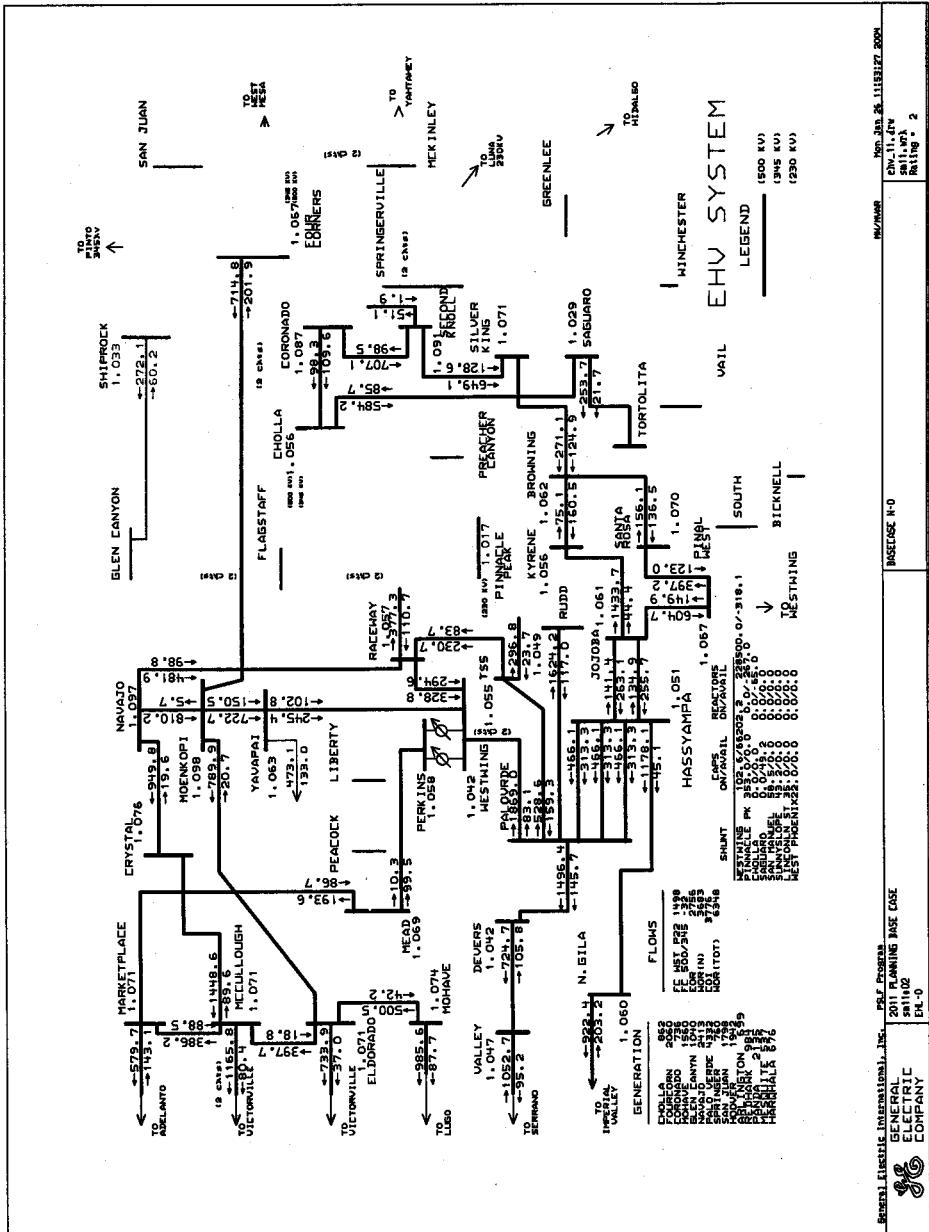
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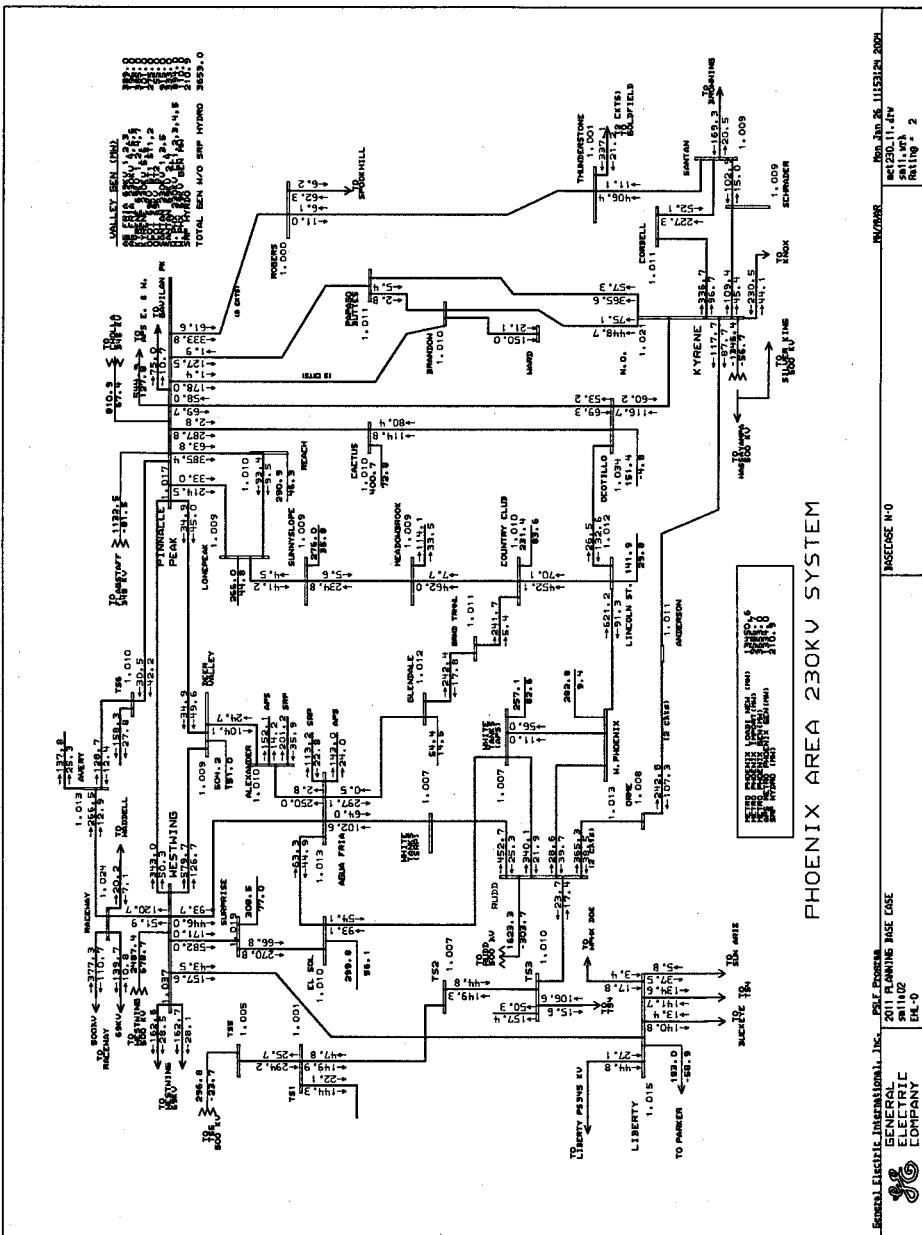
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PC-230.10.kv  
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Rating = 1

NORTHERN ARIZONA AREA

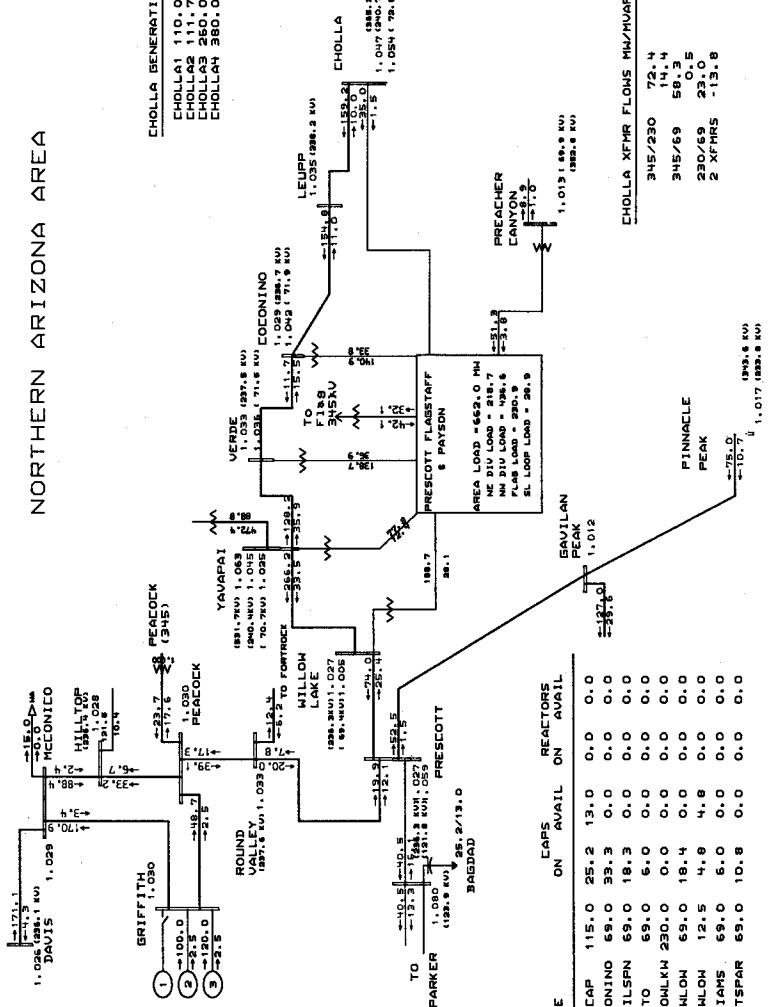




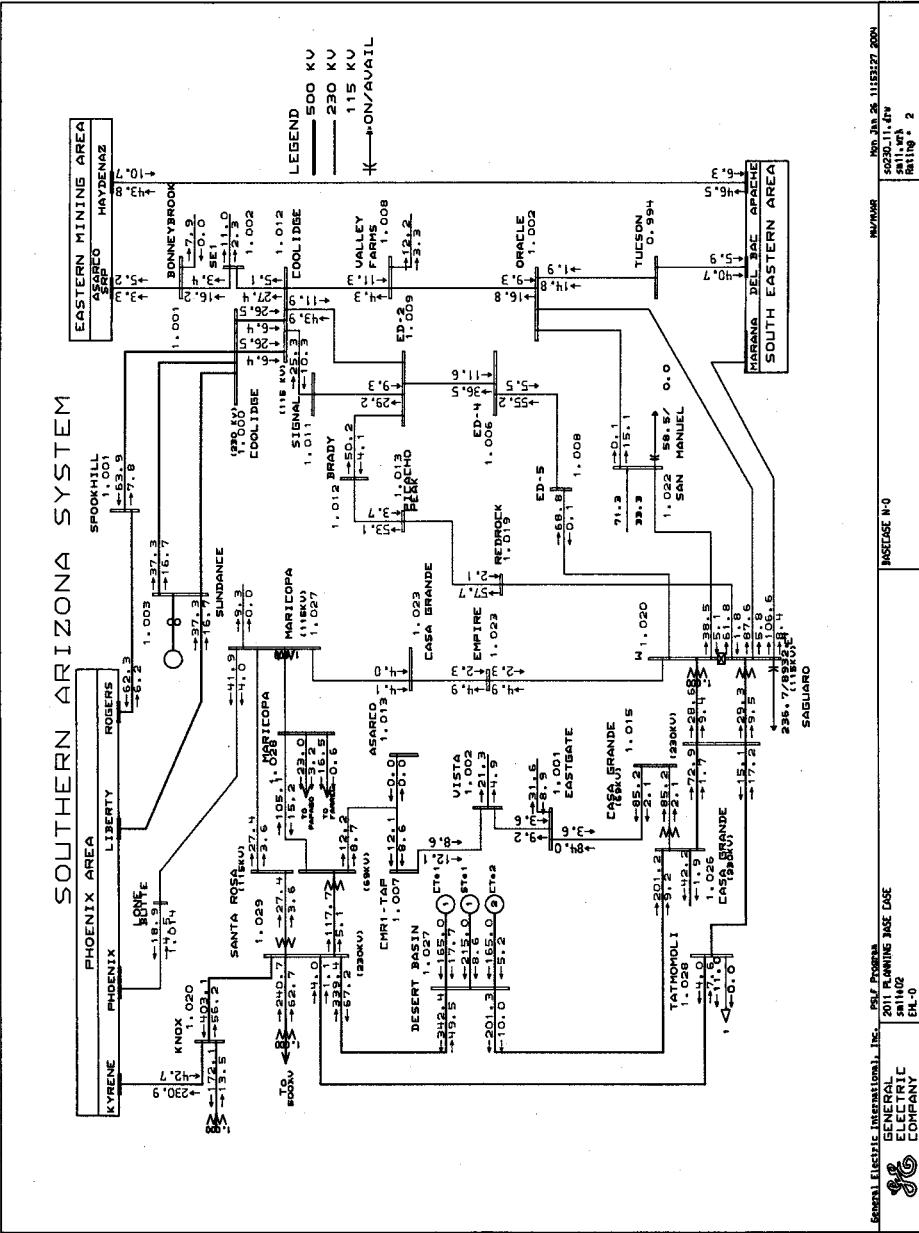


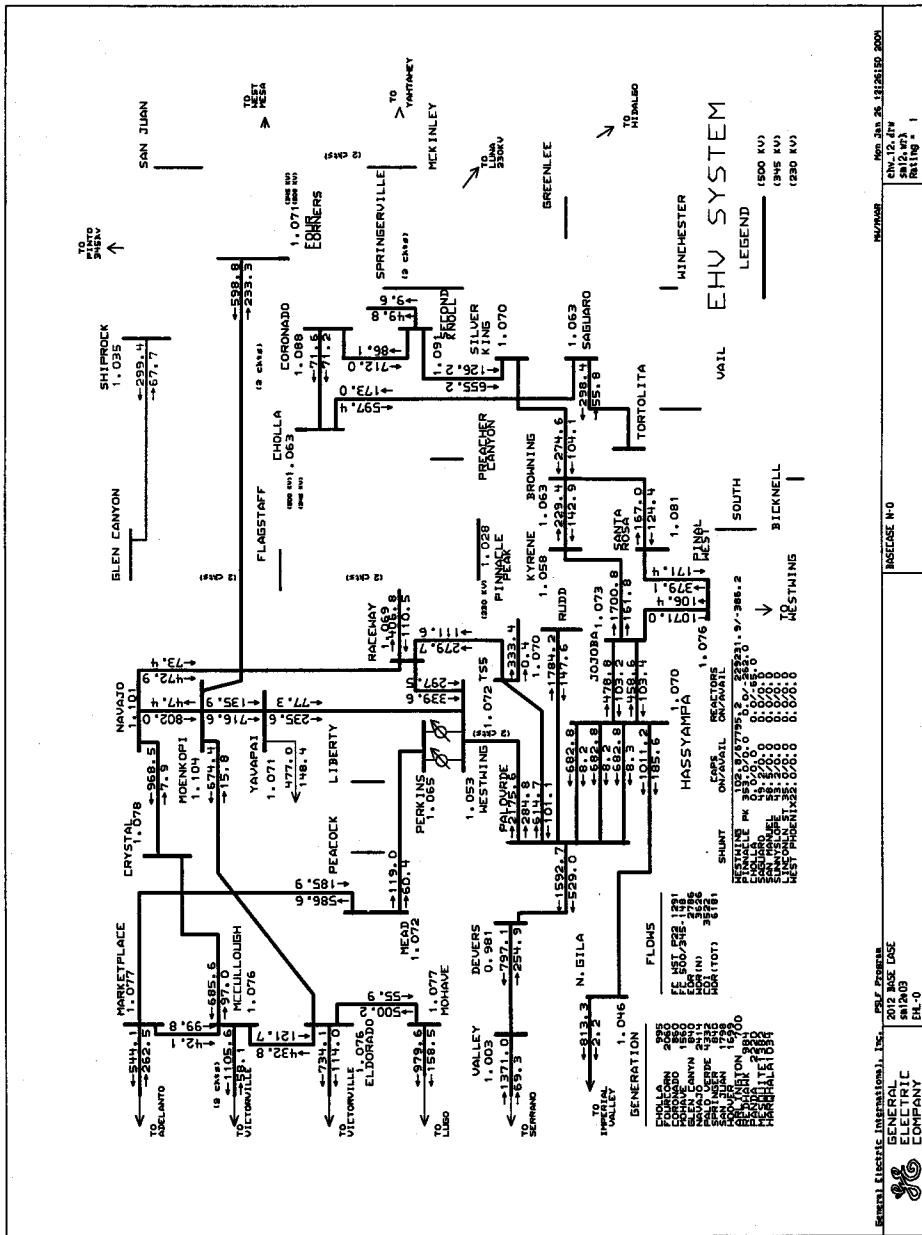


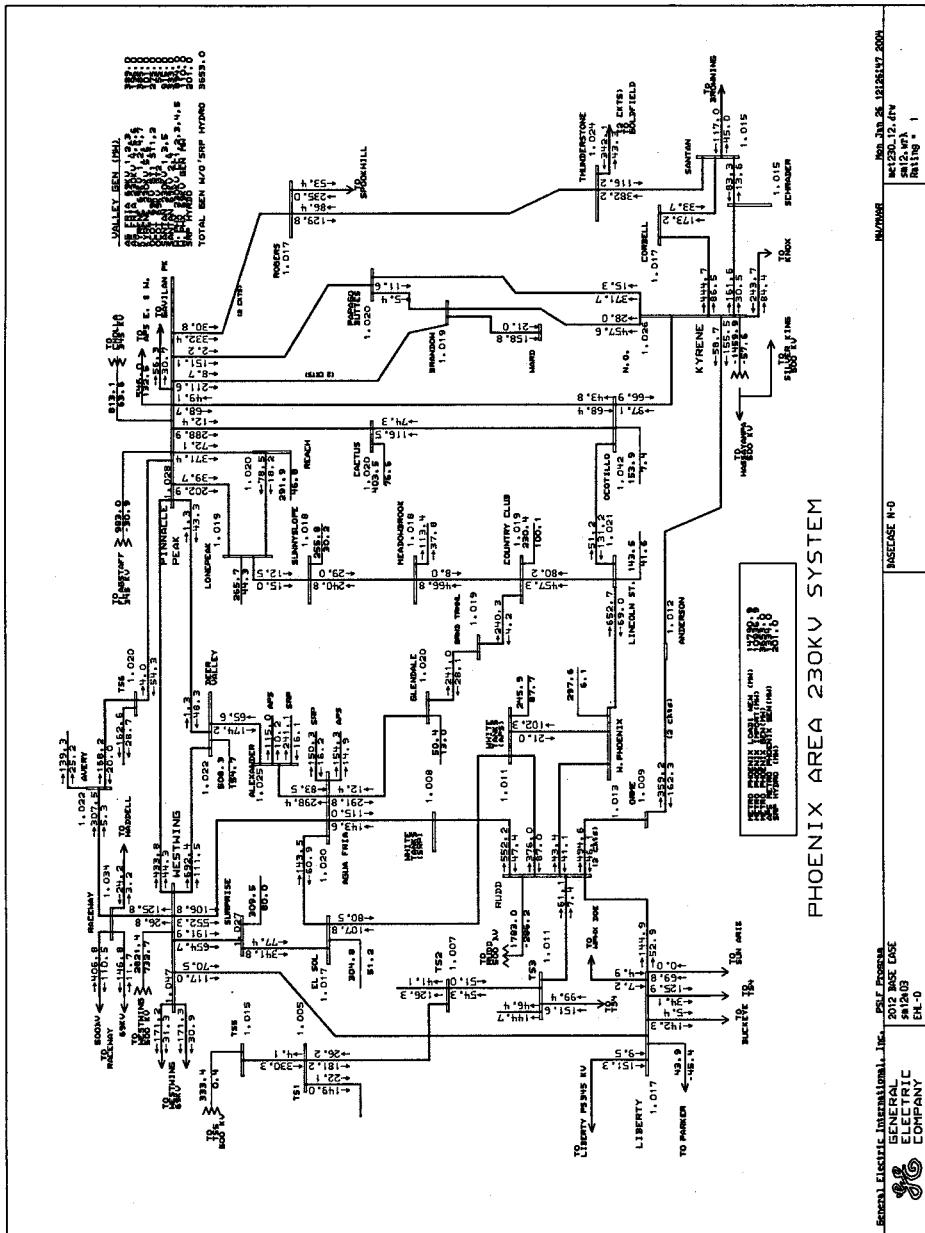
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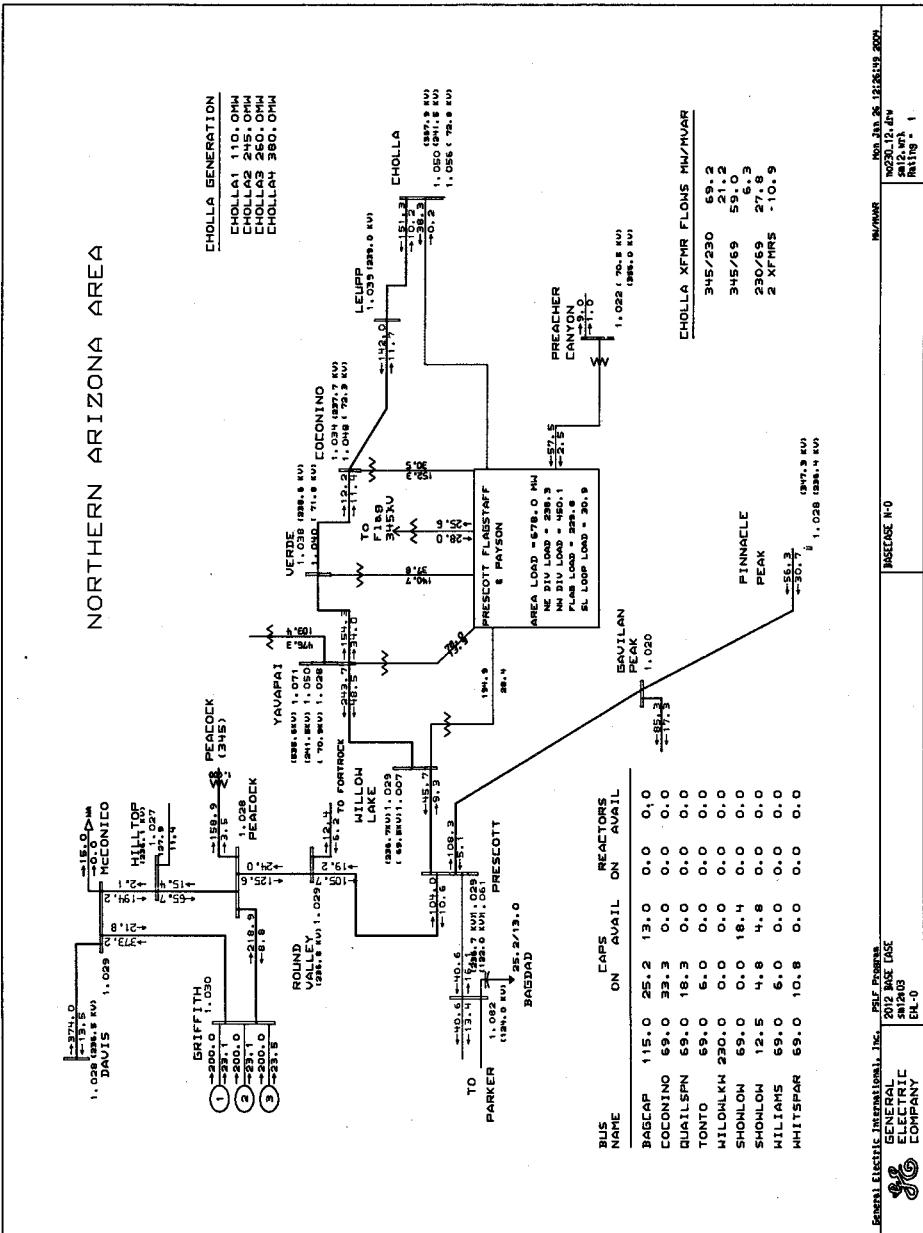
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GENERAL ELECTRIC ELECTRIC COMPANY	2010 BOUNDARY LINE DATE SINCE 1992 GE	1,026,100	NUCLEAR 1,026,100 SINCE 1992 GE

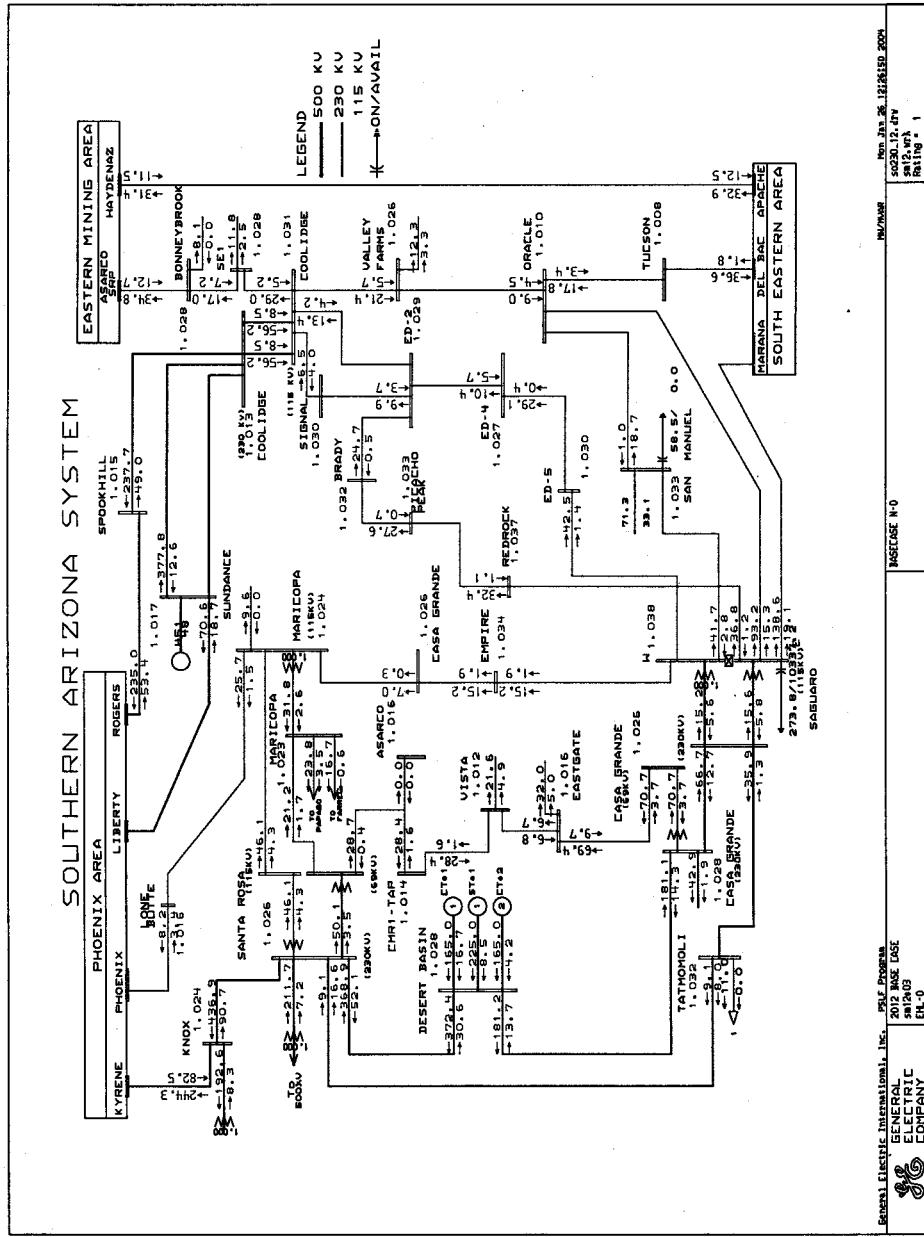


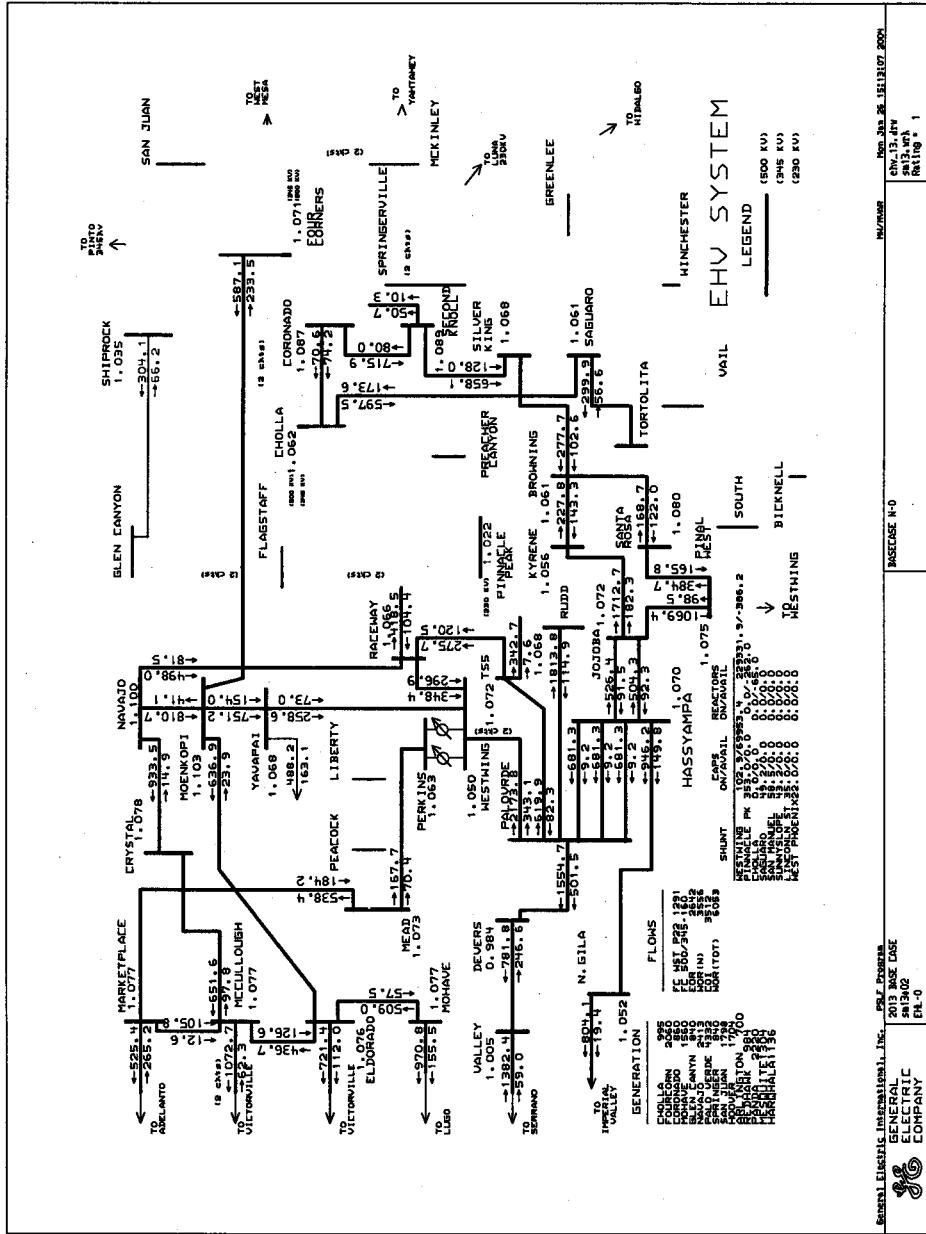


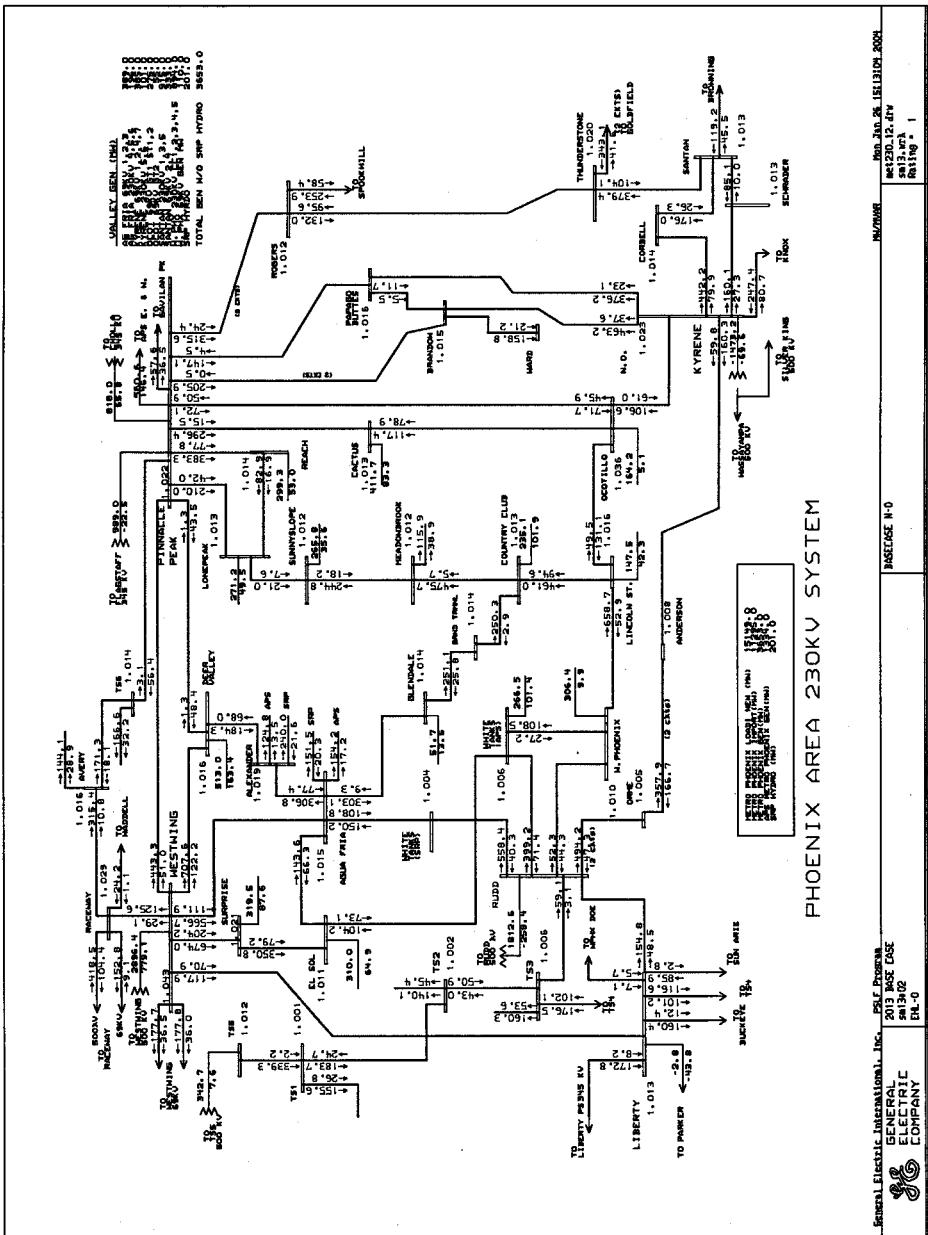


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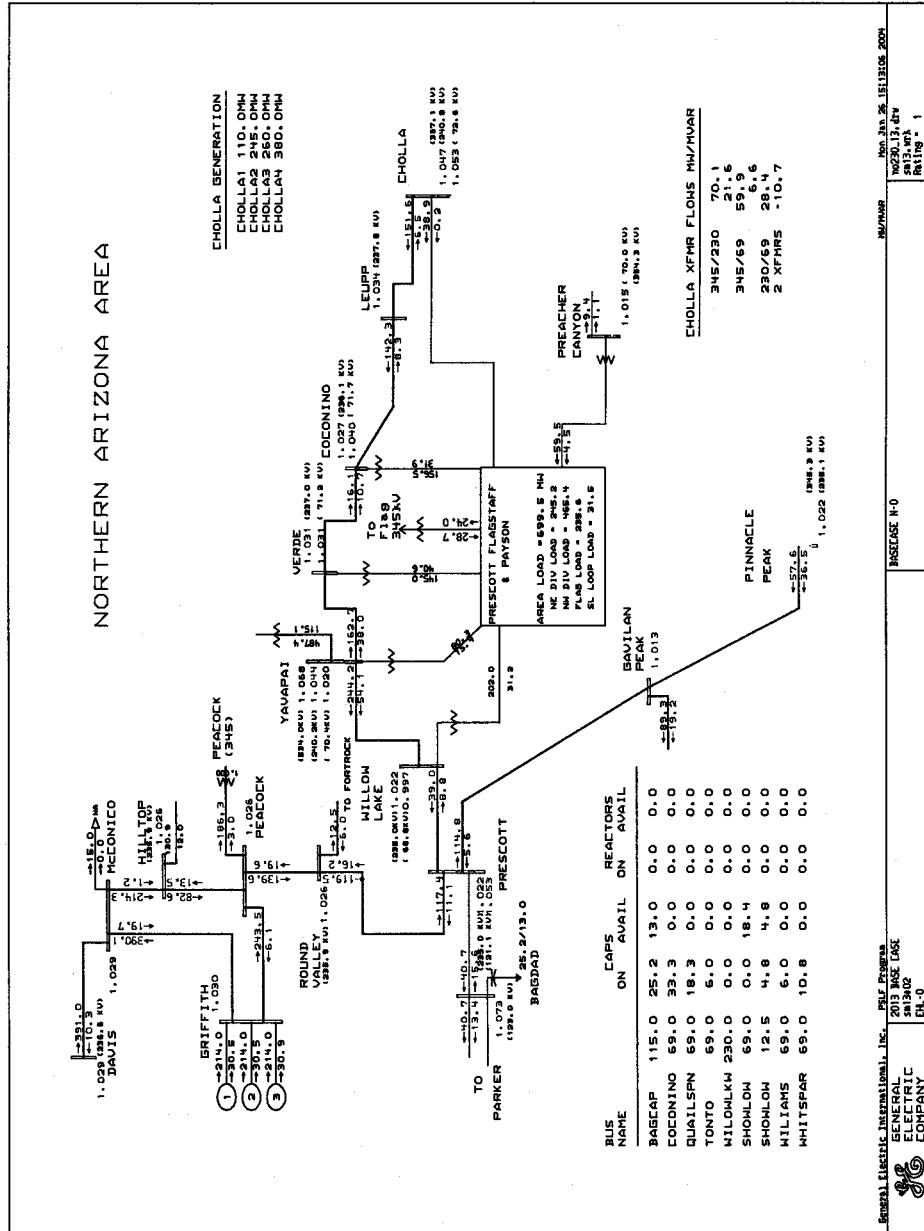


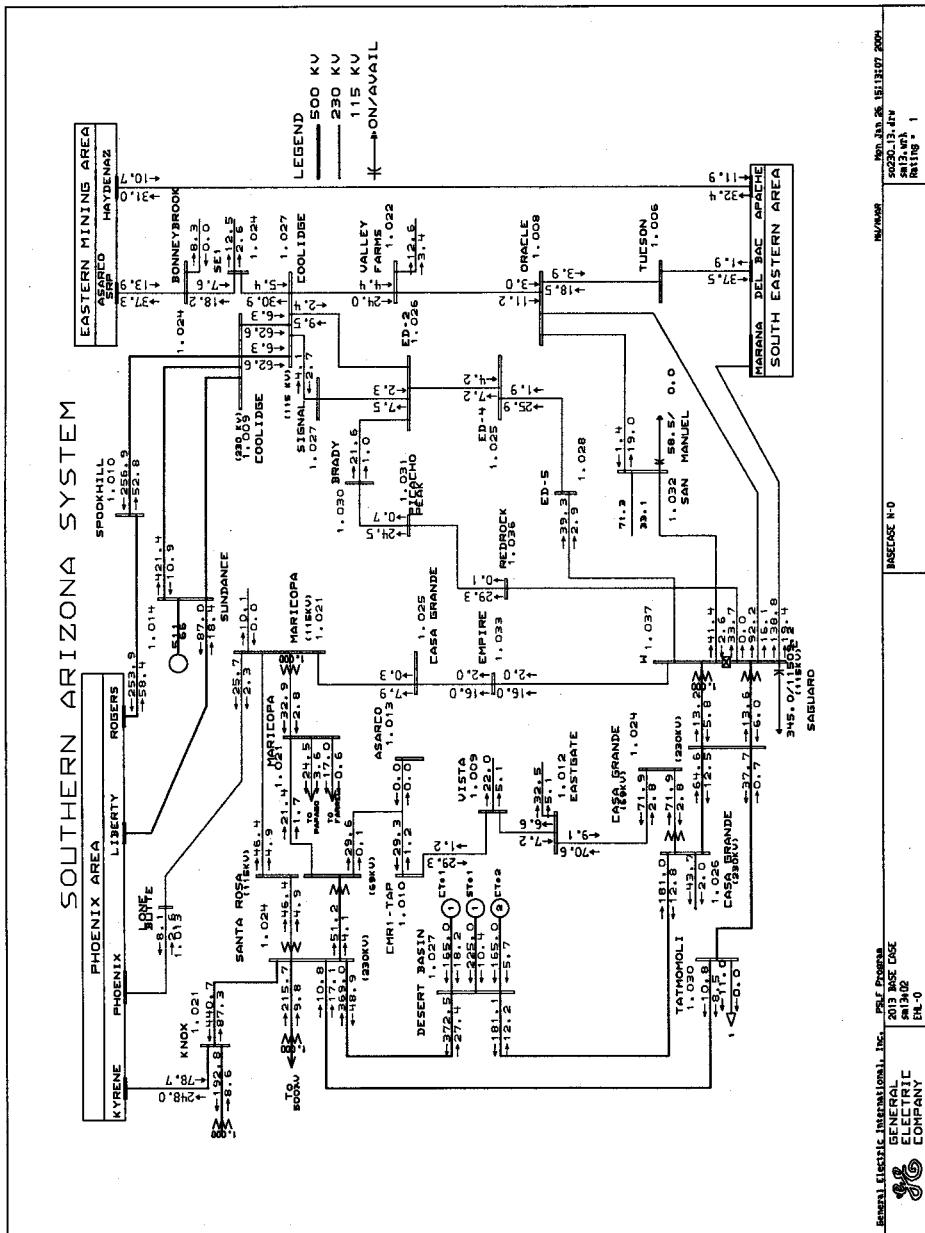






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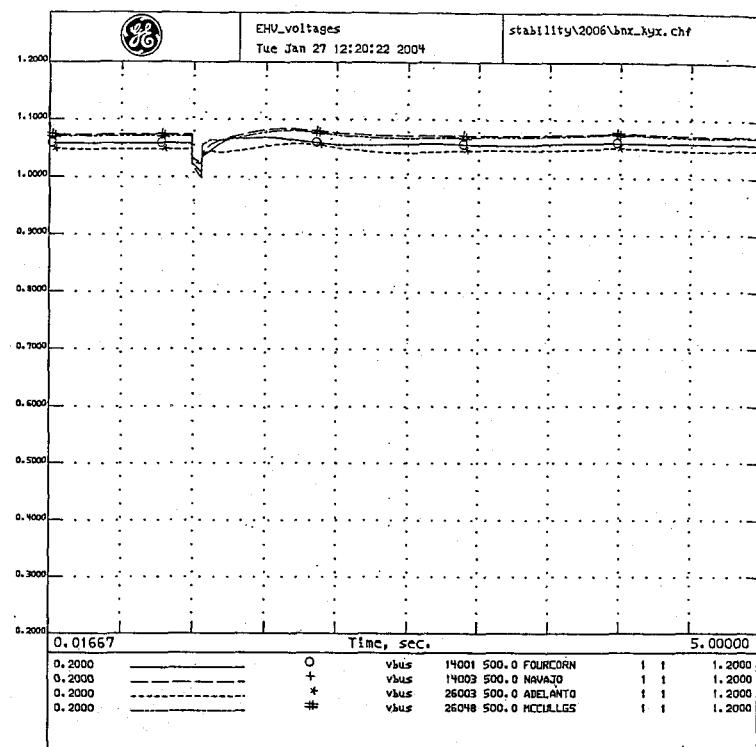
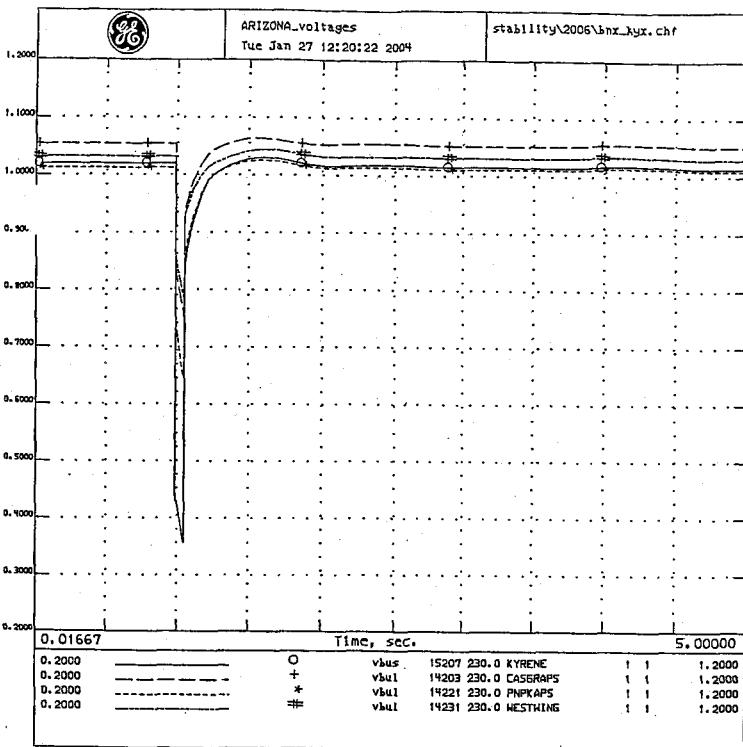


## **APPENDIX B**

### **2006 Stability Plots**

## Table of Contents

<u>Simulation</u>	<u>Page</u>
<b>Browning 500kv</b>	
Browning-Kyrene outage .....	B1
<b>Cholla 500 &amp; 345kv</b>	
Cholla-Coronado outage .....	B2
Cholla-Four Corners outage .....	B3
Cholla-Pinnacle Peak outage .....	B4
Cholla-Saguaro outage .....	B5
<b>Four Corners 500kv</b>	
Four Corners-Moenkopi outage .....	B6
<b>Jojoba 500kv</b>	
Jojoba-Hassayampa outage .....	B7
Jojoba-Kyrene outage .....	B8
<b>Kyrene 500kv</b>	
Kyrene-Jojoba outage .....	B9
<b>Moenkopi 500kv</b>	
Moenkopi-Eldorado outage .....	B10
Moenkopi-Yavapai outage .....	B11
<b>North Gila 500kv</b>	
North Gila-Hassayampa outage .....	B12
North Gila-Imperial Valley outage .....	B13
<b>Navajo 500kv</b>	
Navajo-Crystal outage .....	B14
Navajo-Moenkopi outage .....	B15
Navajo-Westwing outage .....	B16
<b>Perkins 500kv</b>	
Perkins-Mead outage .....	B17
<b>Palo Verde 500kv</b>	
Palo Verde-Devers outage .....	B18
Palo Verde-Jojoba outage .....	B19
Palo Verde-North Gila outage .....	B20
Palo Verde-Rudd outage .....	B21
Palo Verde-Westwing outage .....	B22
<b>Pinnacle Peak 345kv</b>	
Pinnacle Peak-Cholla outage .....	B23
<b>Rudd 500kv</b>	
Rudd-Palo Verde outage .....	B24
<b>Saguaro 500kv</b>	
Saguaro-Cholla outage .....	B25
<b>Westwing 500kv</b>	
Westwing-Navajo outage .....	B26
Westwing-Palo Verde outage .....	B27
Westwing-Yavapai outage .....	B28
<b>Yavapai 500kv</b>	
Yavapai-Moenkopi outage .....	B29
Yavapai-Westwing outage .....	B30

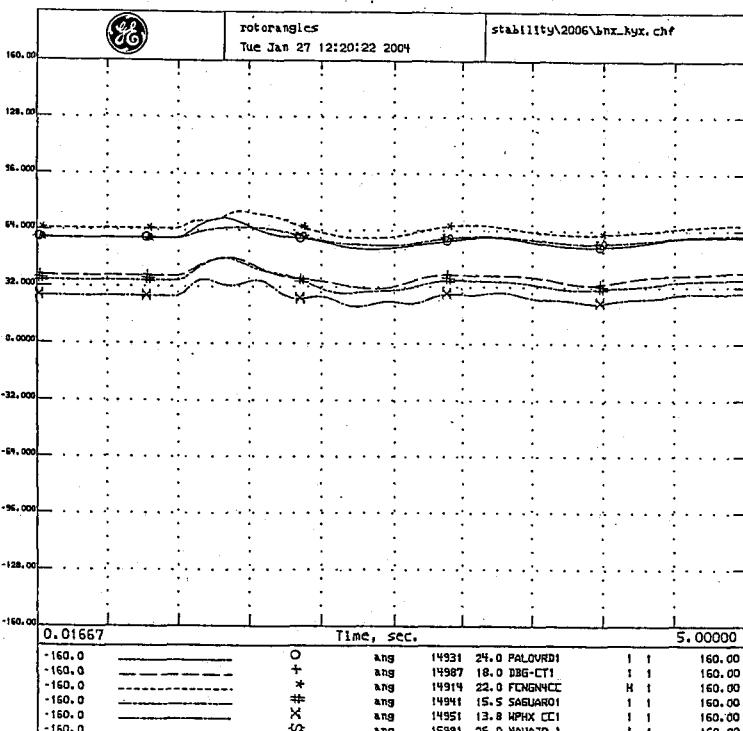


KYRENE FLT KYR-BRWN LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
BRWN-KYR STAB +/- 01/03; T=0 3P FLT KYR500;  
4C CLR FLT W/BRWN-KYR; 2006.4y4|NSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

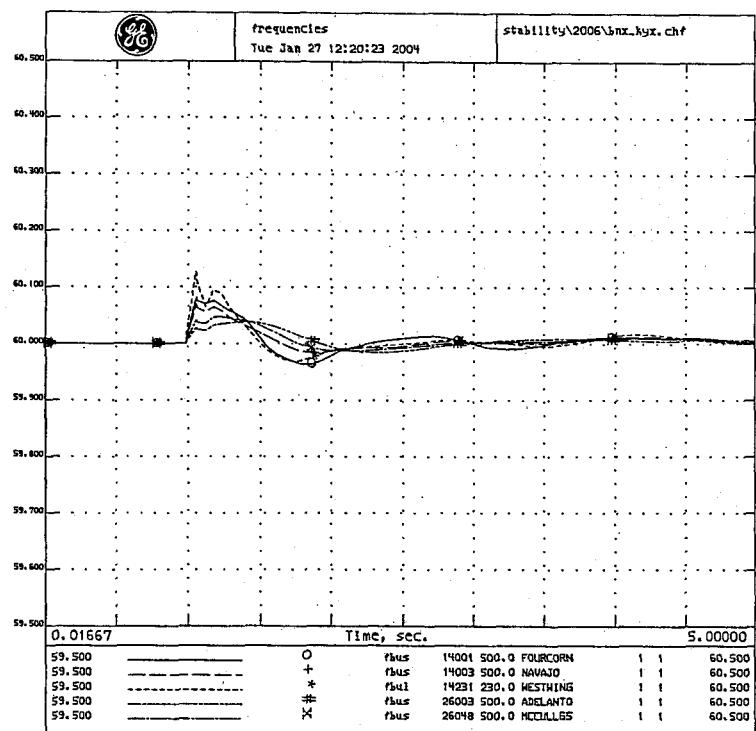
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OCTOBER 28, 2003  
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4C CLR FLT W/BRWN-KYR; 2006.4y4|NSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



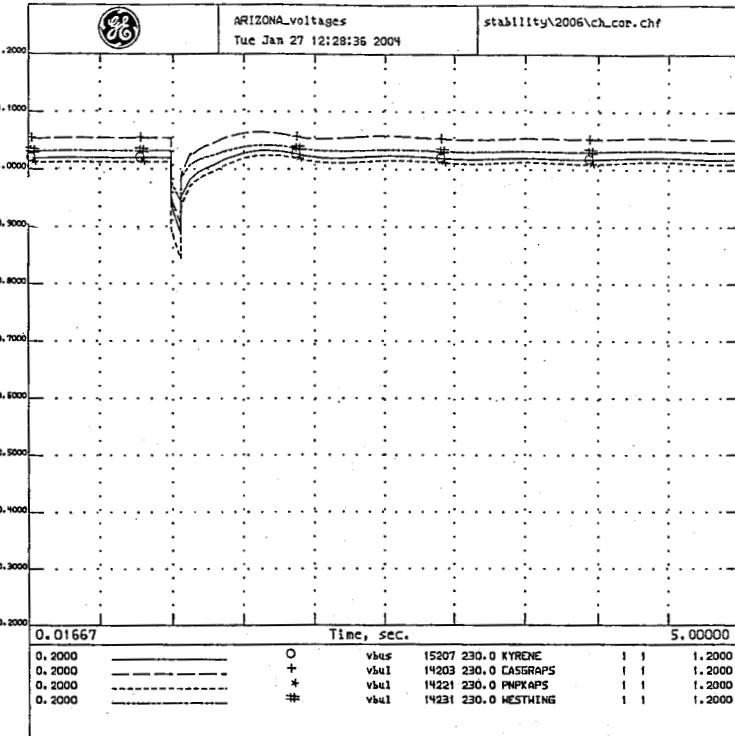
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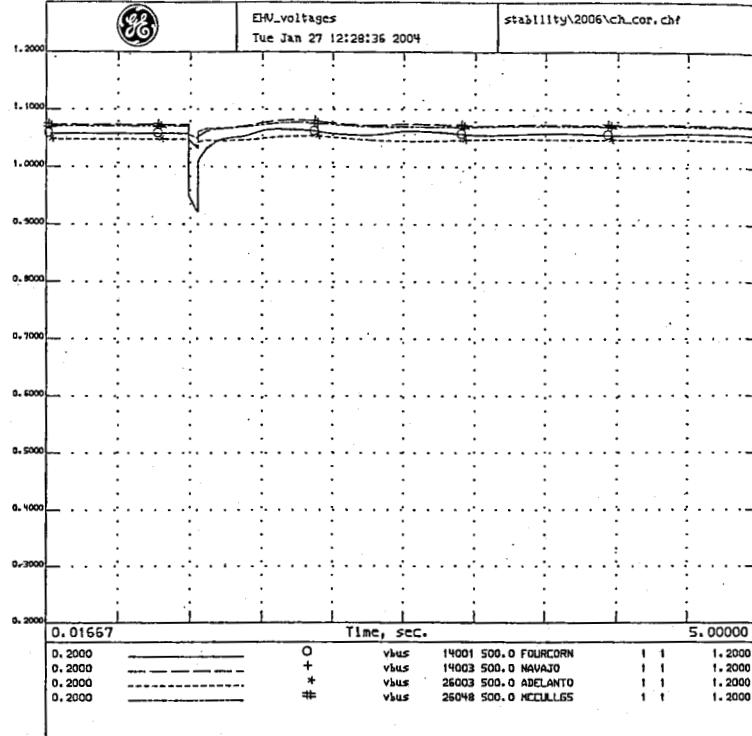
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ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
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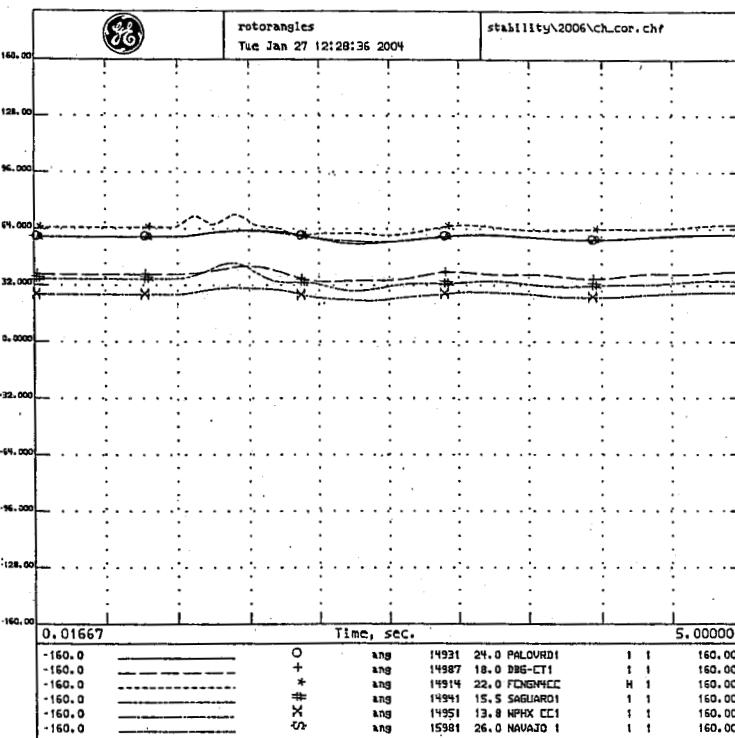
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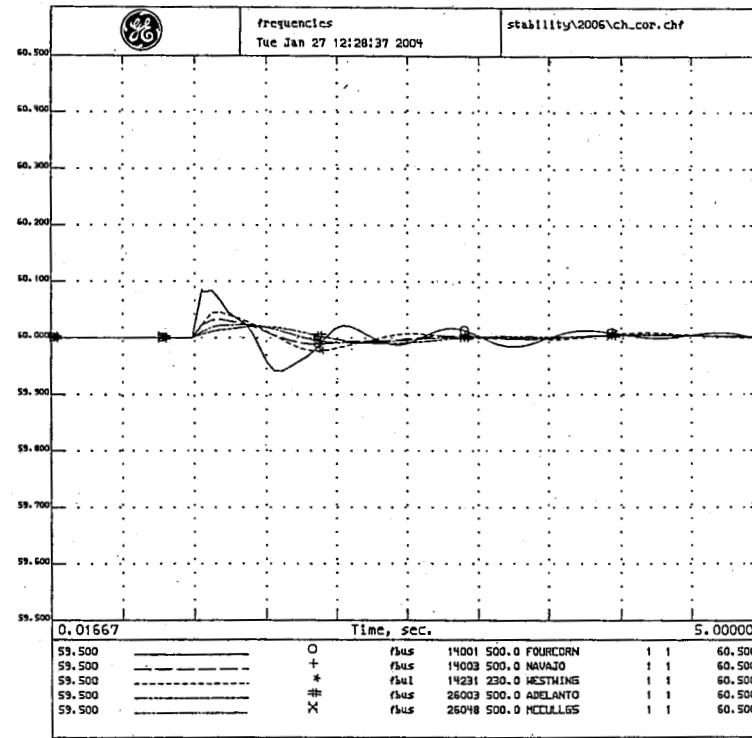
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W/CHO-COR;2006.d4d;NSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



CHOLLA 500KV FLT CH-COR LINE OUT  
HS3-SA APPROVED BASE CASE  
R 28, 2003  
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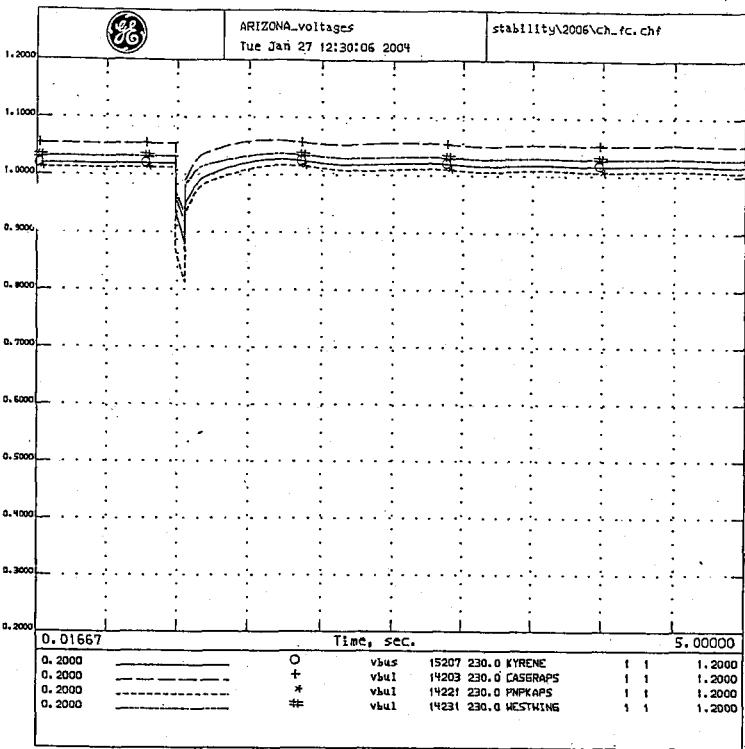
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2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
CHO-COR STAB1 1/03; T=0 3P FLT CH0500;4C CLR FLT  
W/CHO-COR;2006.d4d;NSCC.bpt

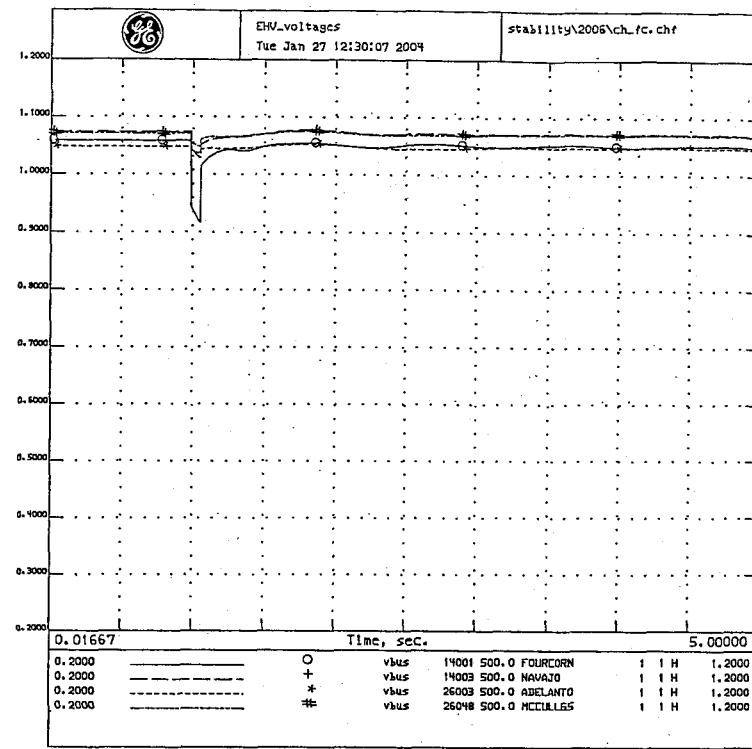
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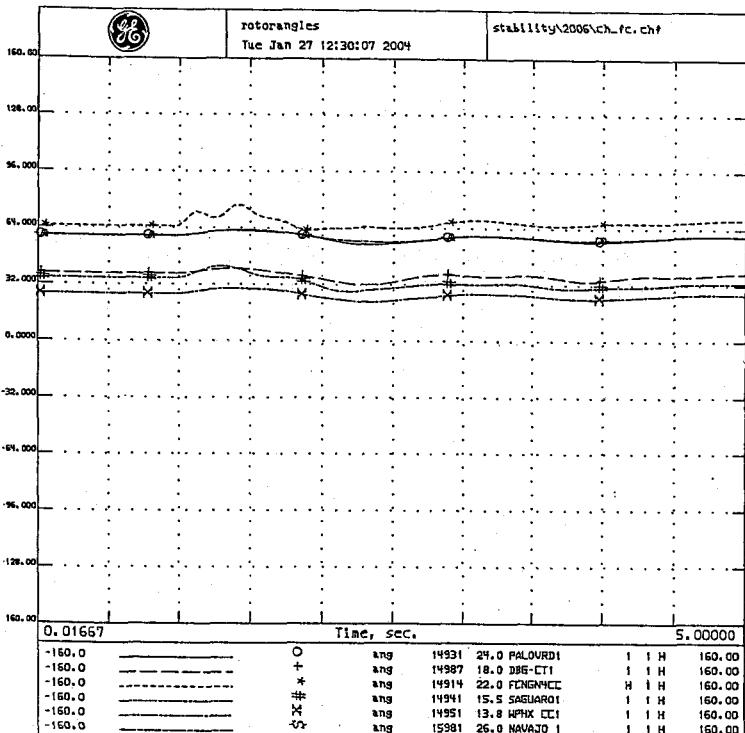
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ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



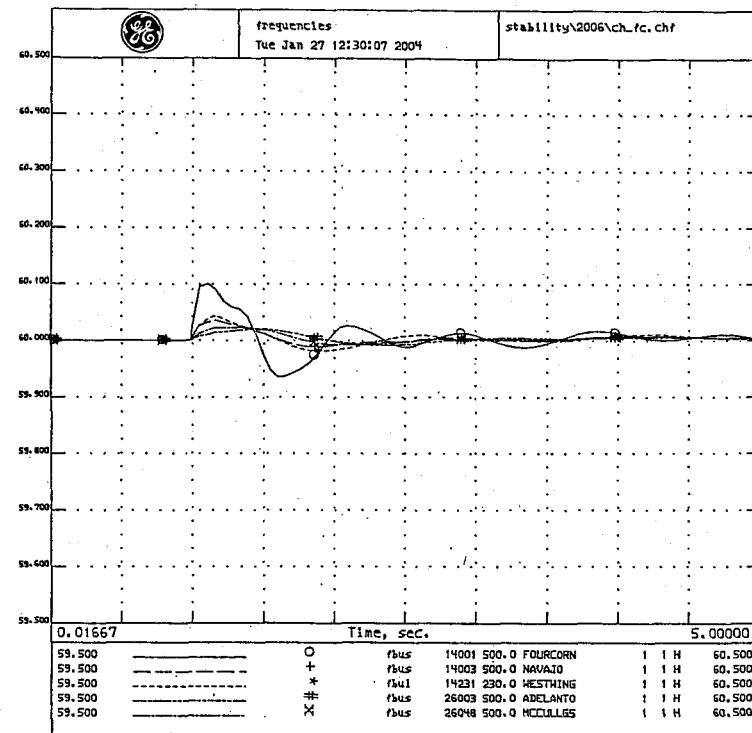
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ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



CHOLLA FLT CH-FC LINE OUTI  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
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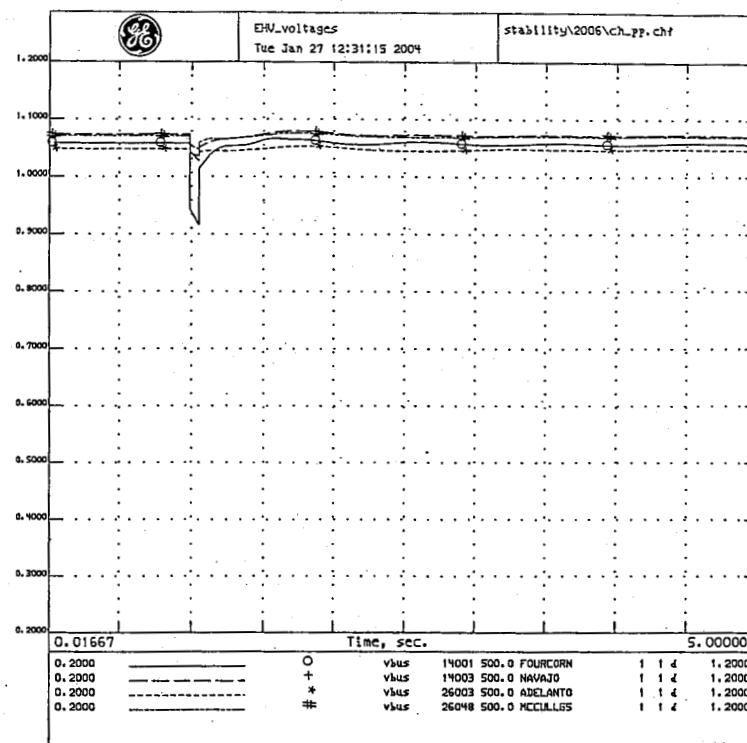
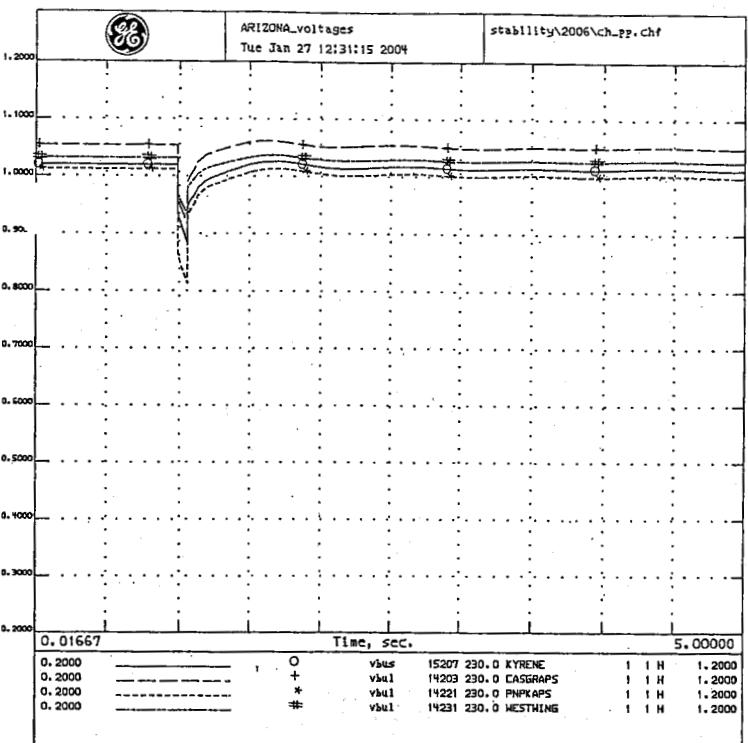
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CHOLLA FLT CH-FC LINE OUTI  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
CHO-FC #1 STAB; 01/03; T=0 3P FLT CHO345;FLSH FCN-CHO CAPS;  
4C CLR FLT W/CHO-FC #1;2006.4y4;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

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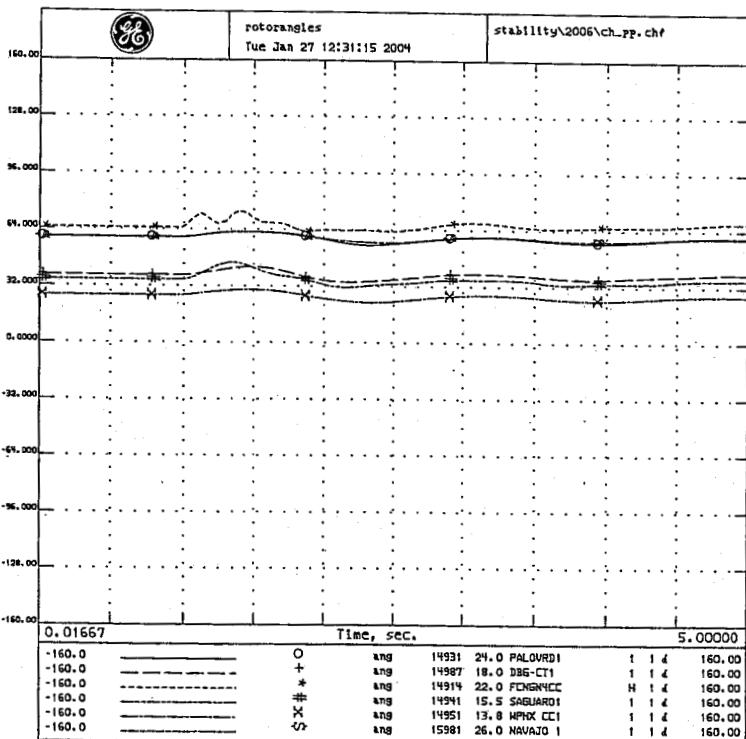


CHOLLA FLT CH-PPK LINE OUT!  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
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4C CLR FLT W/CHO-PPK #1;BC REIN CAPS;2006.4y4;HS3C.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

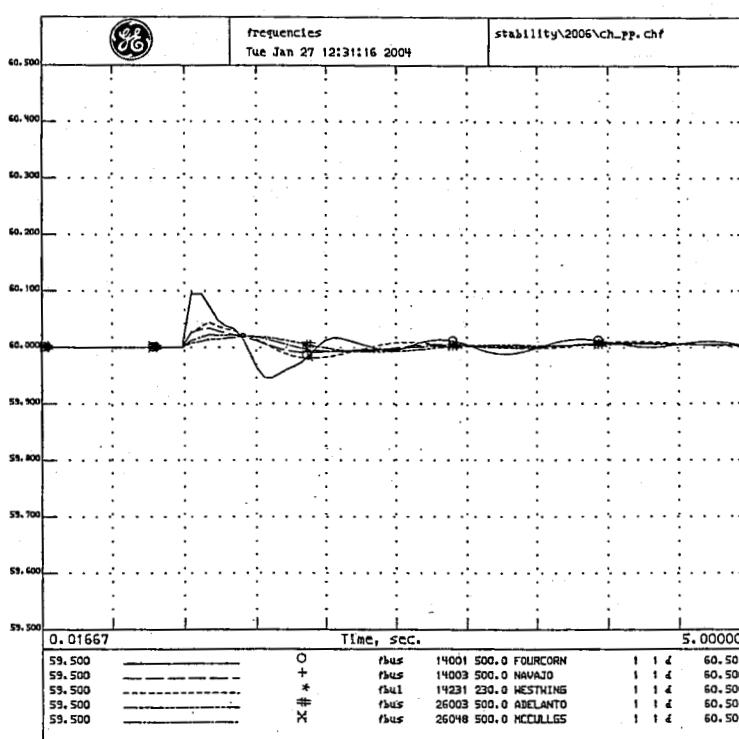
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4C CLR FLT W/CHO-PPK #1;BC REIN CAPS;2006.4y4;HS3C.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



CHOLLA FLT CH-PPK LINE OUT!  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
CHO-PPK #1 STAB; 01/03; T=0 3P FLT CH0345;FLSH FDN-CHO CAPS;  
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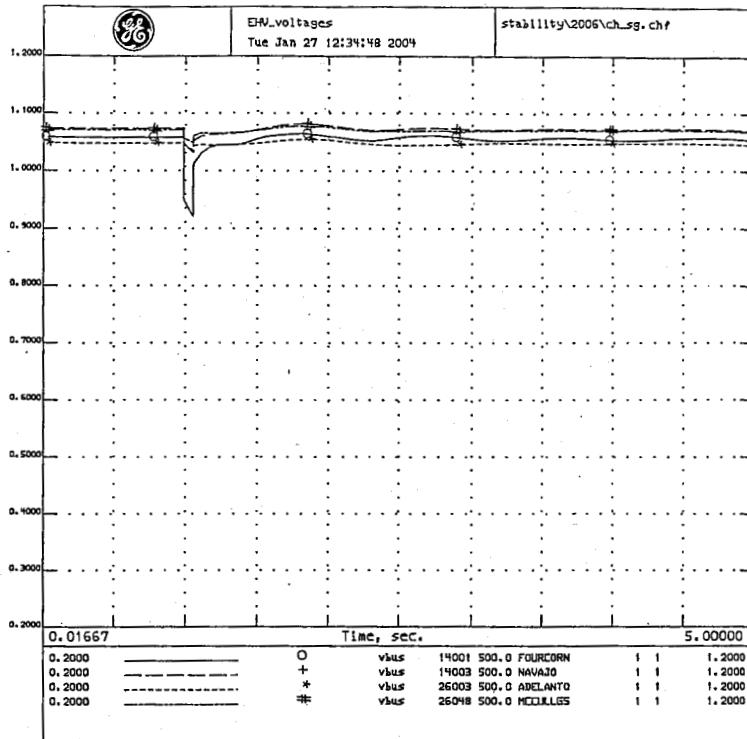
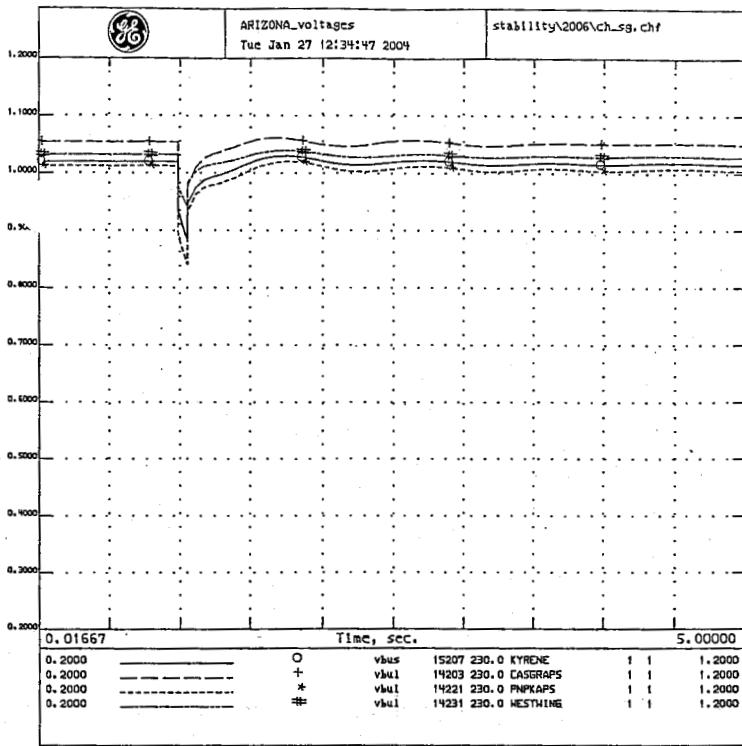
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MOST RECENT VERSION OF THE MDF USED.



CHOLLA FLT CH-PPK LINE OUT!  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
CHO-PPK #1 STAB; 01/03; T=0 3P FLT CH0345;FLSH FDN-CHO CAPS;  
4C CLR FLT W/CHO-PPK #1;BC REIN CAPS;2006.4y4;HS3C.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

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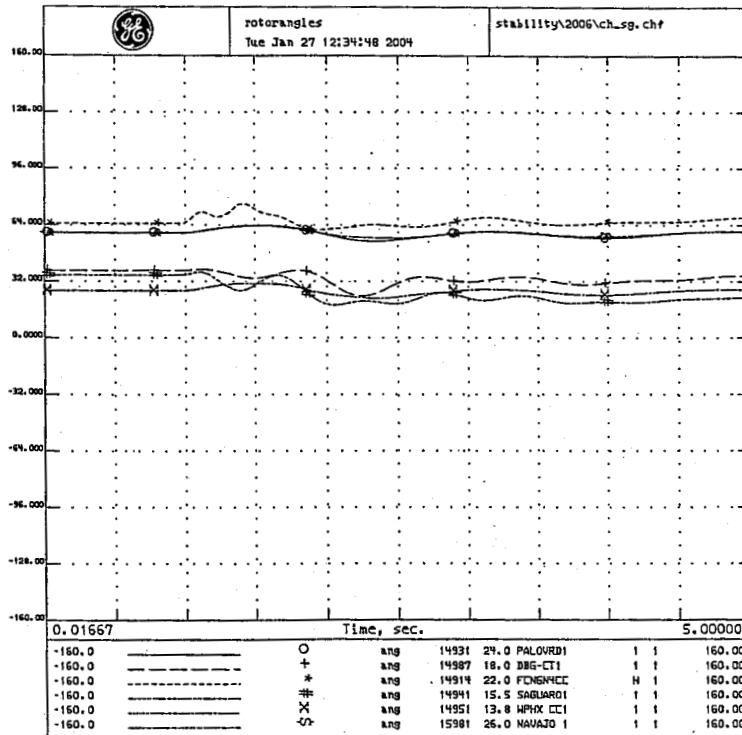


CHOLLA 500KV FLT CH-SAG LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
CHO-SAG STAB: 1/03; T=0 3P FLT CH0500;4C CLR FLT  
W/CHO-SAG|2006.dyd;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

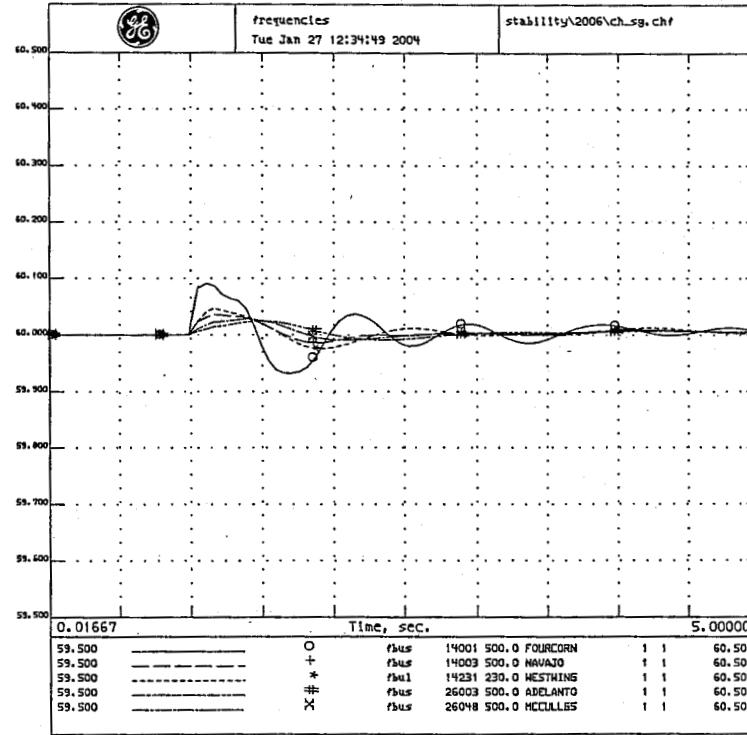
CHOLLA 500KV FLT CH-SAG LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
CHO-SAG STAB: 1/03; T=0 3P FLT CH0500;4C CLR FLT  
W/CHO-SAG|2006.dyd;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



CHOLLA 500KV FLT CH-SAG LINE OUT  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
CHO-SAG STAB: 1/03; T=0 3P FLT CH0500;4C CLR FLT  
W/CHO-SAG|2006.dyd;HSCC.bpt

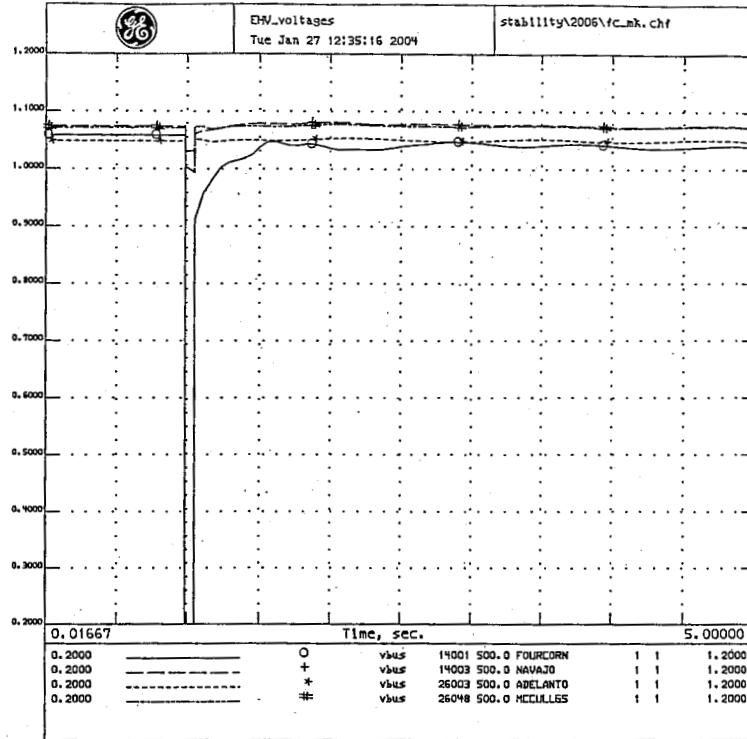
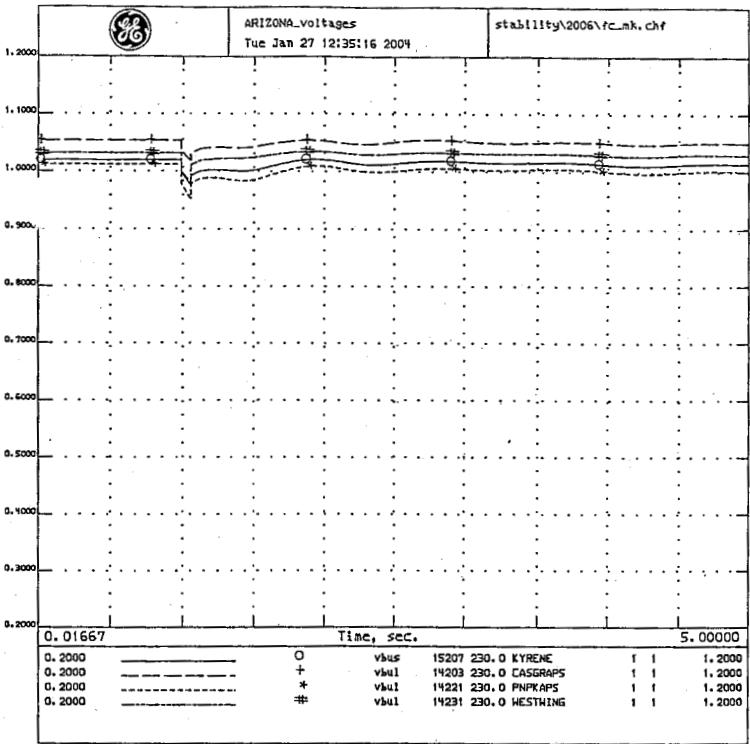
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HOST RECENT VERSION OF THE MDF USED.



CHOLLA 500KV FLT CH-SAG LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
CHO-SAG STAB: 1/03; T=0 3P FLT CH0500;4C CLR FLT  
W/CHO-SAG|2006.dyd;HSCC.bpt

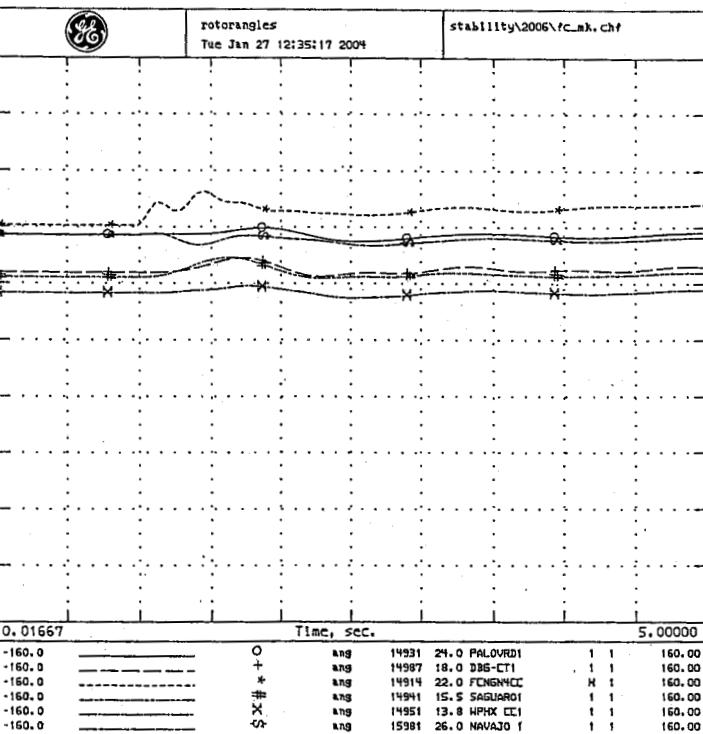
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HOST RECENT VERSION OF THE MDF USED.

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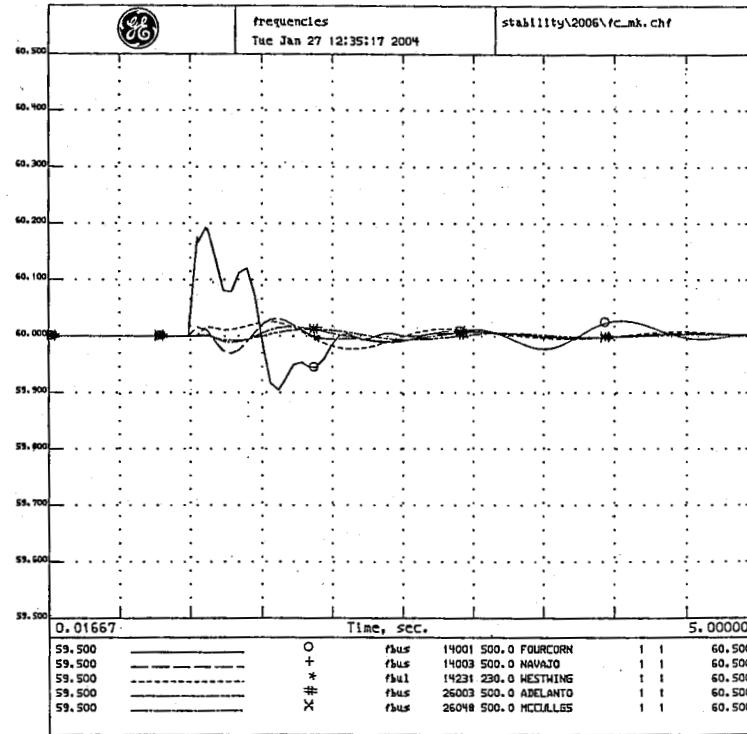
FCN FLTS00 FCN-MNK out  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
FOURCORN-MOENKOPPI STAB; 1/03; T=0 3P FLT FCN500;10X FLT DMPING;FLSH  
CAPS FCN-MKP/NAV-MKP;4C CLR FLT W/FCN-MKP;8C REIN CAPS;2006.4y4/HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



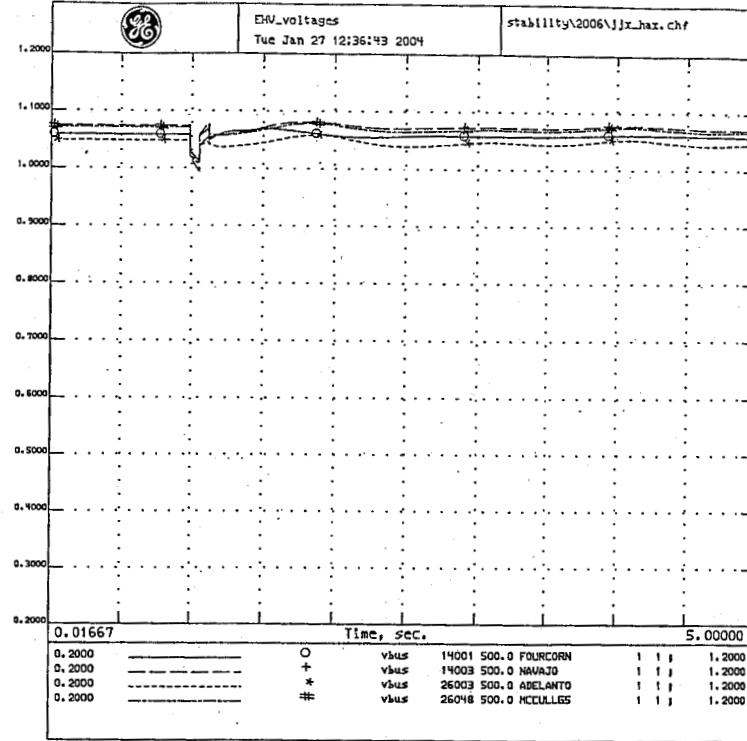
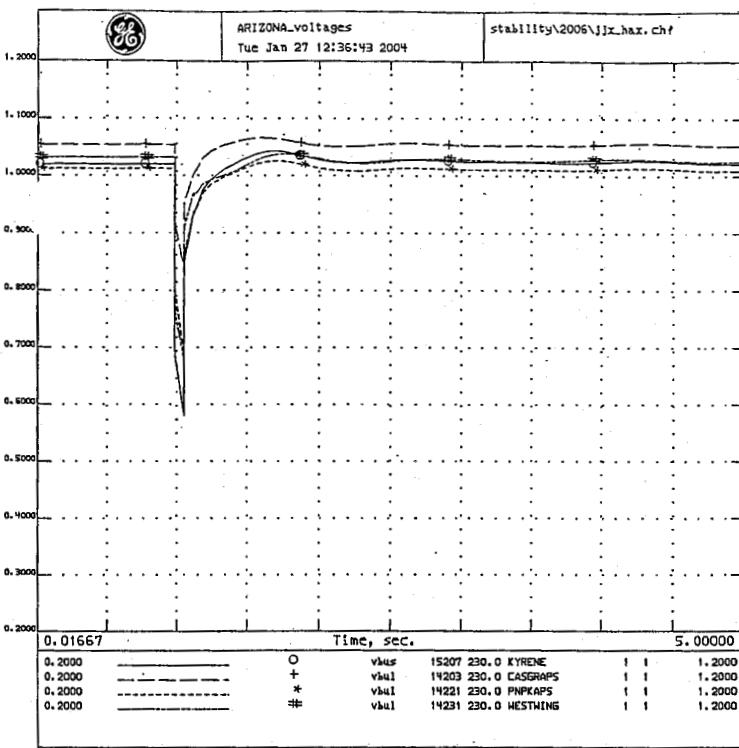
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28, 2003  
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CAPS FCN-MKP/NAV-MKP;4C CLR FLT W/FCN-MKP;8C REIN CAPS;2006.4y4/HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



FCN FLTS00 FCN-MNK out  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
FOURCORN-MOENKOPPI STAB; 1/03; T=0 3P FLT FCN500;10X FLT DMPING;FLSH  
CAPS FCN-MKP/NAV-MKP;4C CLR FLT W/FCN-MKP;8C REIN CAPS;2006.4y4/HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

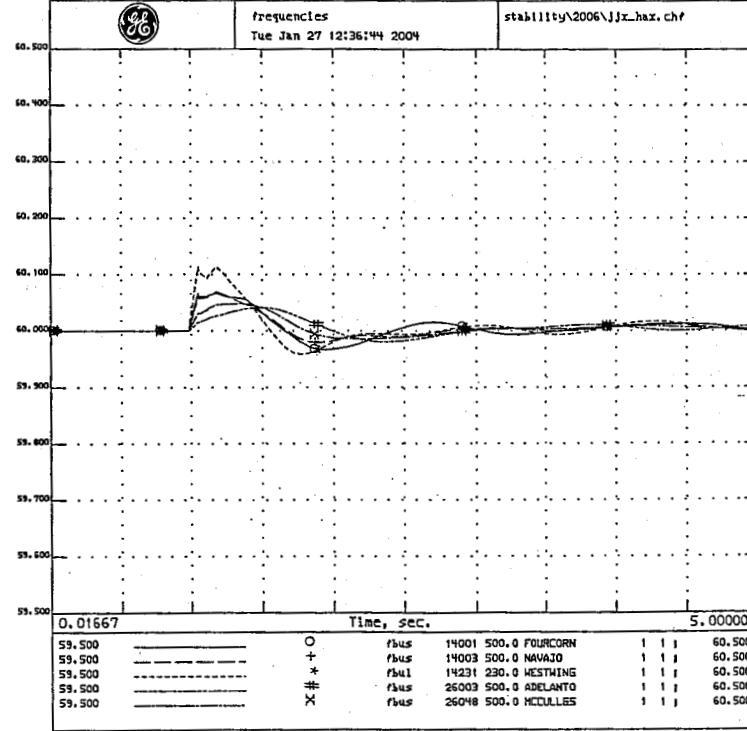
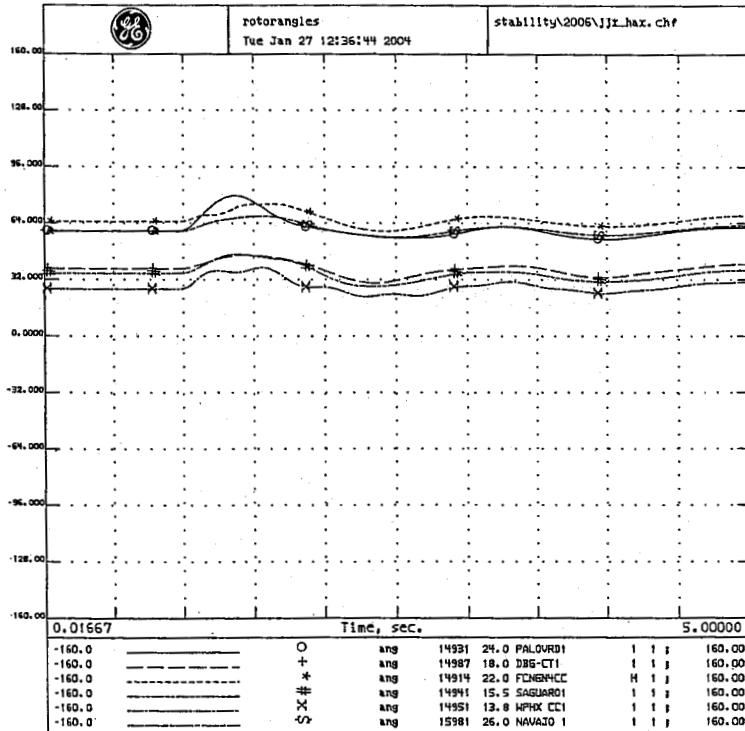


JOJOBA FLT JOJOBA-HASSY LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
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NAV-MKP/MKP-YAV,PV-DV/NG;YC CLR FLT W/HAS-JJ;BC REIN;2006.4y4;HSCE,bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

JOJOBA FLT JOJOBA-HASSY LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
HAS-JJ STAB +1; 01/03; T=0 3P FLT JJ500|10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;YC CLR FLT W/HAS-JJ;BC REIN;2006.4y4;HSCE,bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



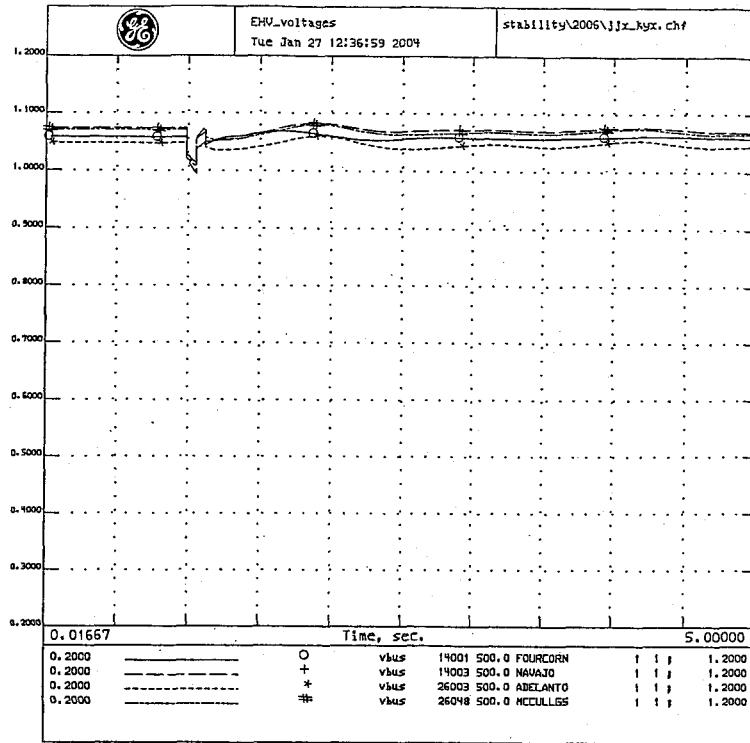
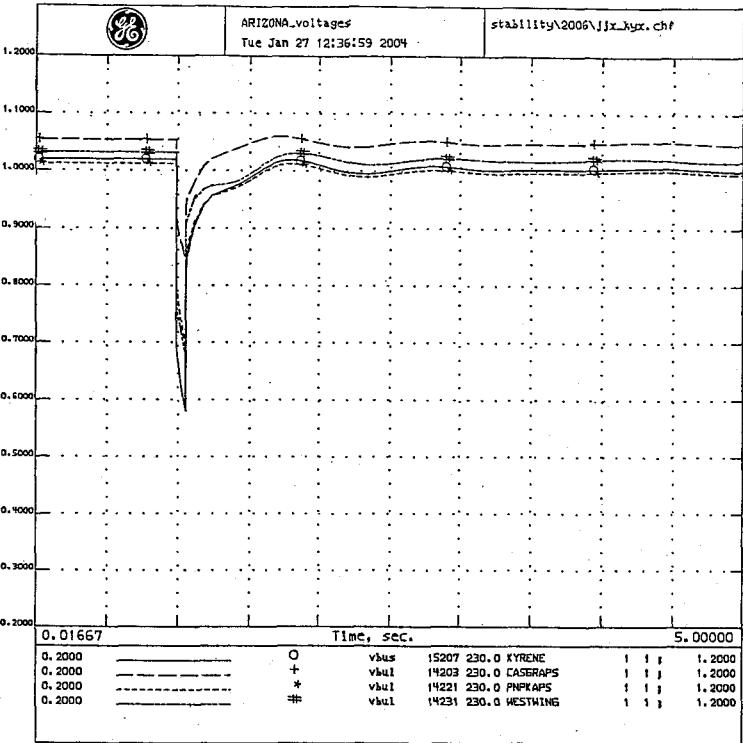
JOJOBA FLT JOJOBA-HASSY LINE OUT  
S3-SA APPROVED BASE CASE  
R 28, 2003  
J STAB +1; 01/03; T=0 3P FLT JJ500|10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;YC CLR FLT W/HAS-JJ;BC REIN;2006.4y4;HSCE,bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

JOJOBA FLT JOJOBA-HASSY LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
HAS-JJ STAB +1; 01/03; T=0 3P FLT JJ500|10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;YC CLR FLT W/HAS-JJ;BC REIN;2006.4y4;HSCE,bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B7

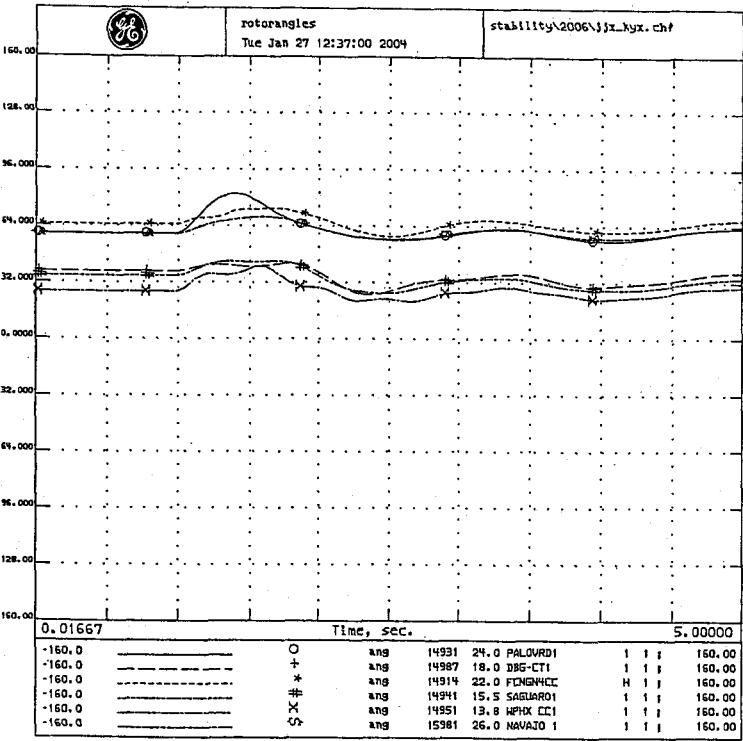


JOJOBA FLT JOJOBA-KYR LINE OUT  
2006 H53-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
JJ-KYR STAB +; 01/03; T=0 3P FLT JJ500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/JJ-KYR;BC REIN;2006.dyd;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

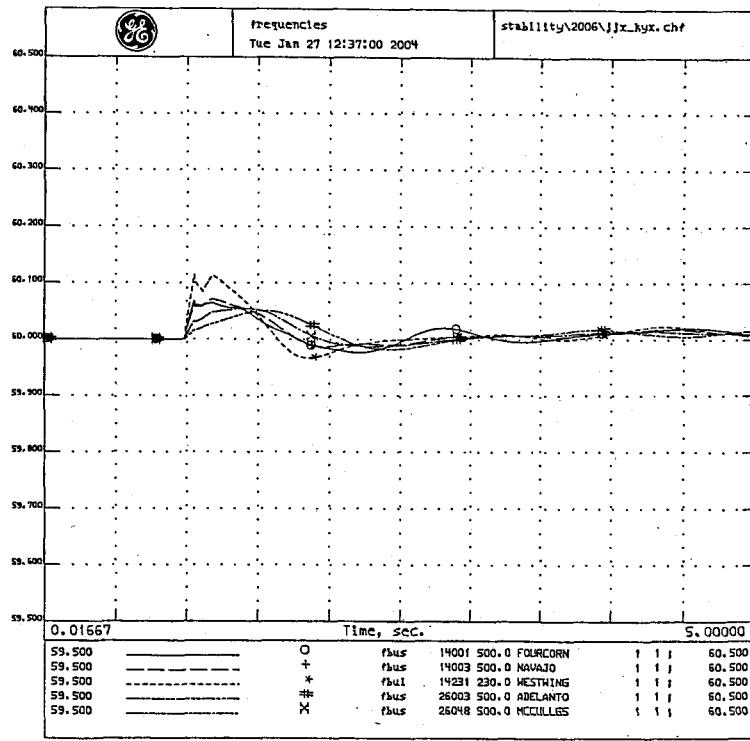
JOJOBA FLT JOJOBA-KYR LINE OUT  
2006 H53-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
JJ-KYR STAB +; 01/03; T=0 3P FLT JJ500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/JJ-KYR;BC REIN;2006.dyd;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



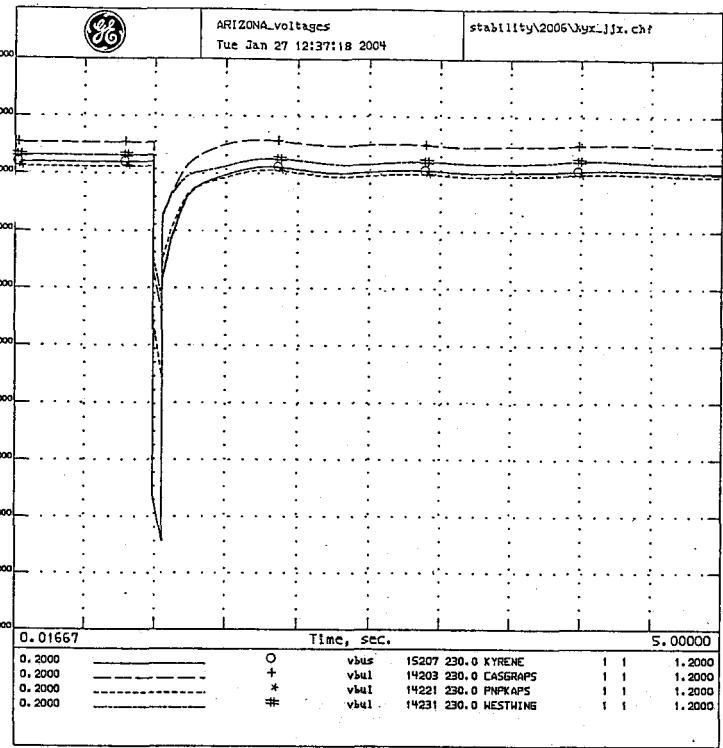
JJ-KYR FLT JOJOBA-KYR LINE OUT  
H53-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
JJ-KYR STAB +; 01/03; T=0 3P FLT JJ500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/JJ-KYR;BC REIN;2006.dyd;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



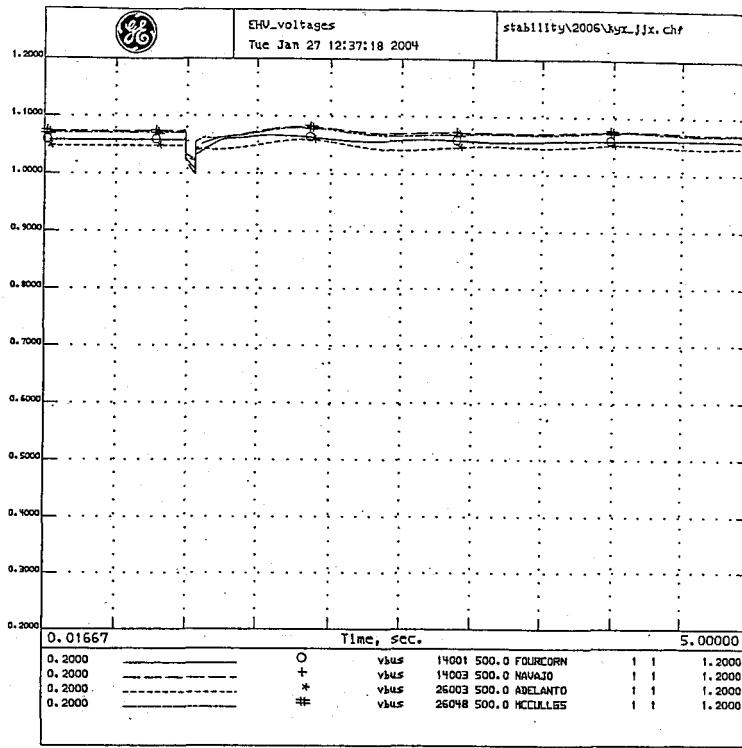
JJ-KYR FLT JOJOBA-KYR LINE OUT  
H53-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
JJ-KYR STAB +; 01/03; T=0 3P FLT JJ500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/JJ-KYR;BC REIN;2006.dyd;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



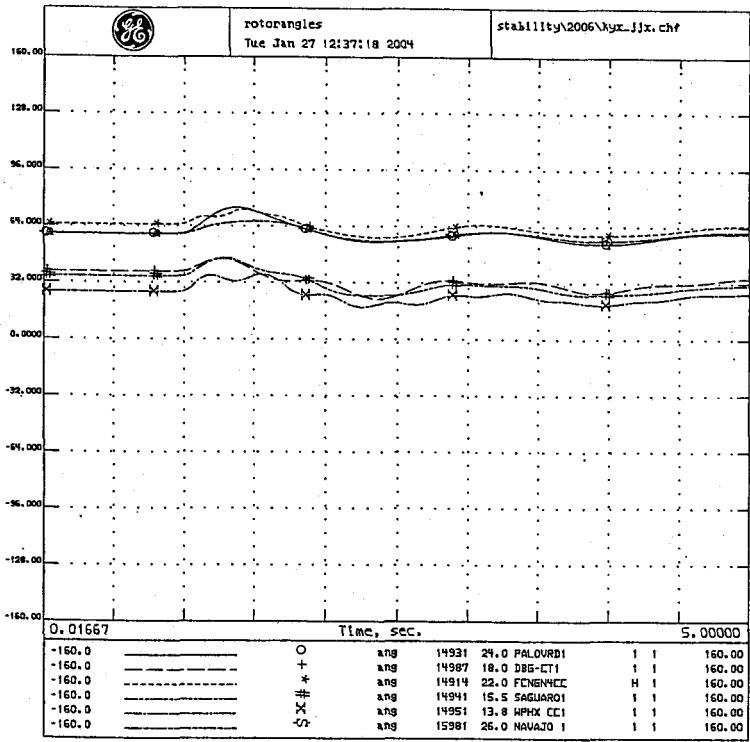
KYRENE FLT KYR-JOJOBA LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
JJ-KYR STAB #1; 01/03; T=0 3P FLT KYRS00;  
4C CLR FLT W/JJ-KYR|2006.4y4|HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



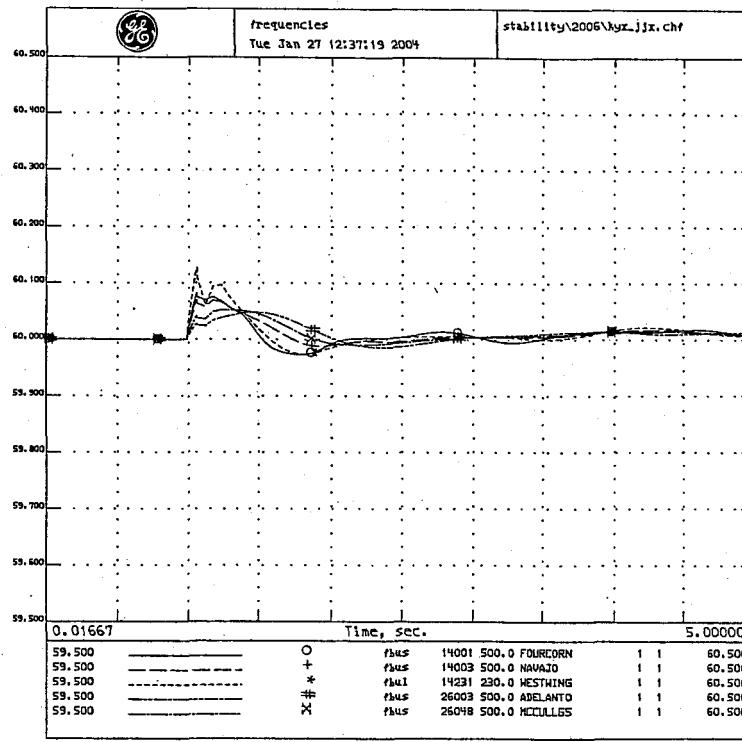
KYRENE FLT KYR-JOJOBA LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
JJ-KYR STAB #1; 01/03; T=0 3P FLT KYRS00;  
4C CLR FLT W/JJ-KYR|2006.4y4|HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



KYRENE FLT KYR-JOJOBA LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
JJ-KYR STAB #1; 01/03; T=0 3P FLT KYRS00;  
4C CLR FLT W/JJ-KYR|2006.4y4|HSCC.bpt

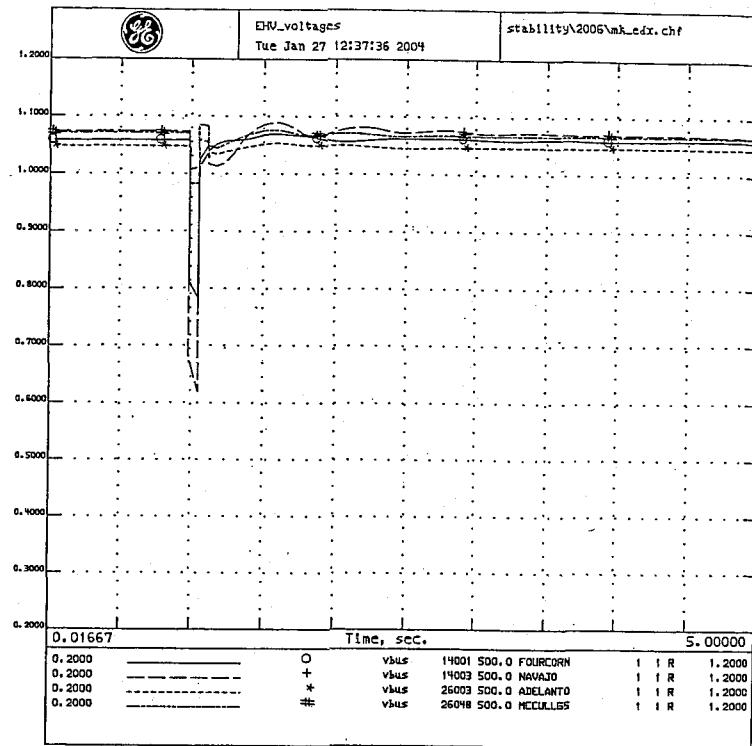
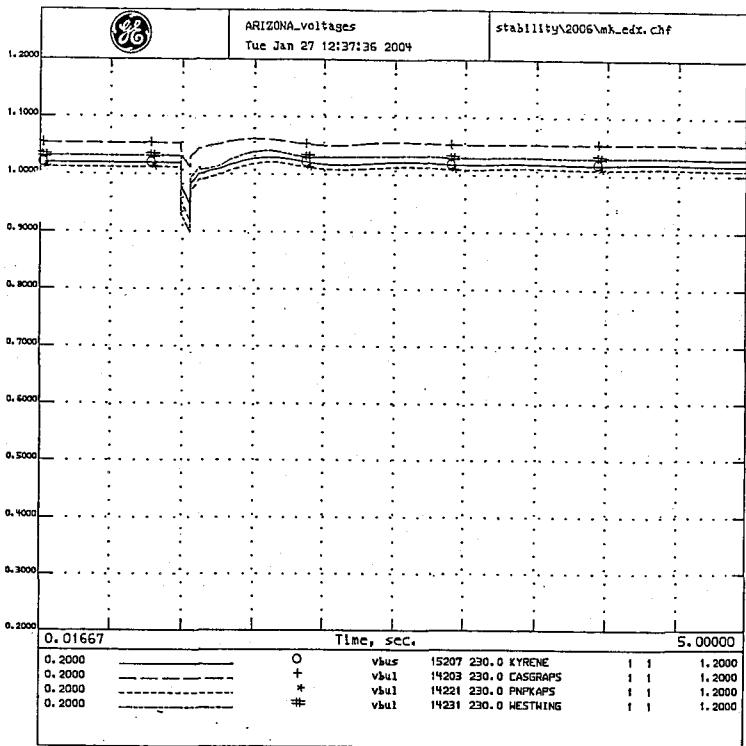
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



KYRENE FLT KYR-JOJOBA LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
JJ-KYR STAB #1; 01/03; T=0 3P FLT KYRS00;  
4C CLR FLT W/JJ-KYR|2006.4y4|HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B9

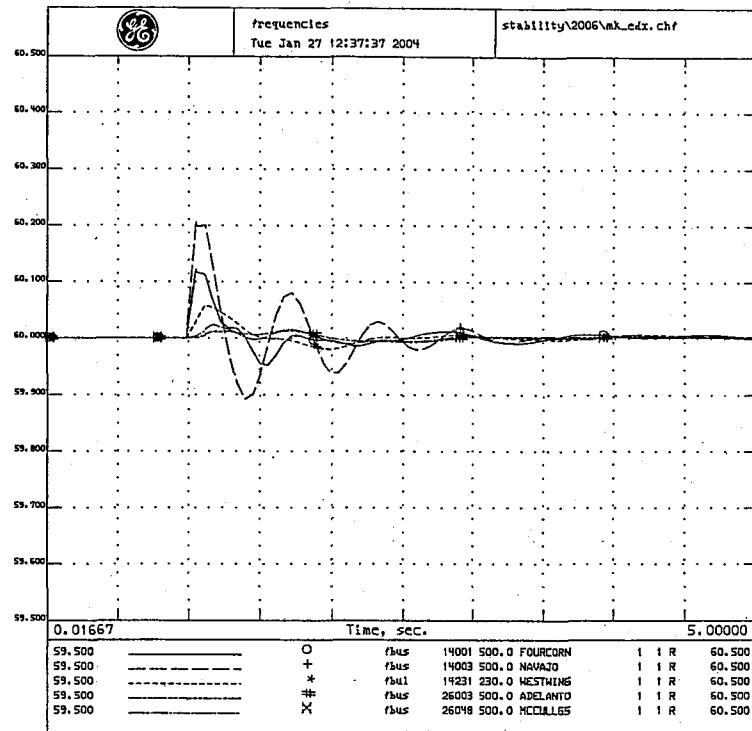
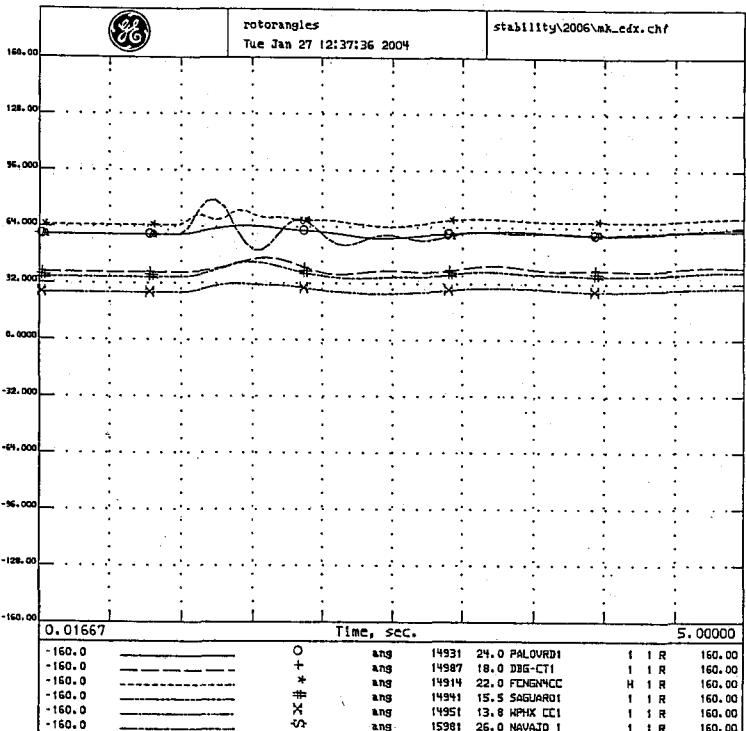


WESTERN ELECTRICITY COORDINATING COUNCIL  
MKP FLT. MKP-ELD line out  
OCTOBER 28, 2003  
MKP-ELD STAB1; 1/03; T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;HC CLR FLT H/MKP-ELD)8C REIN;2006.4y4;HSCL.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

WESTERN ELECTRICITY COORDINATING COUNCIL  
MKP FLT. MKP-ELD line out  
OCTOBER 28, 2003  
MKP-ELD STAB1; 1/03; T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;HC CLR FLT H/MKP-ELD)8C REIN;2006.4y4;HSCL.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



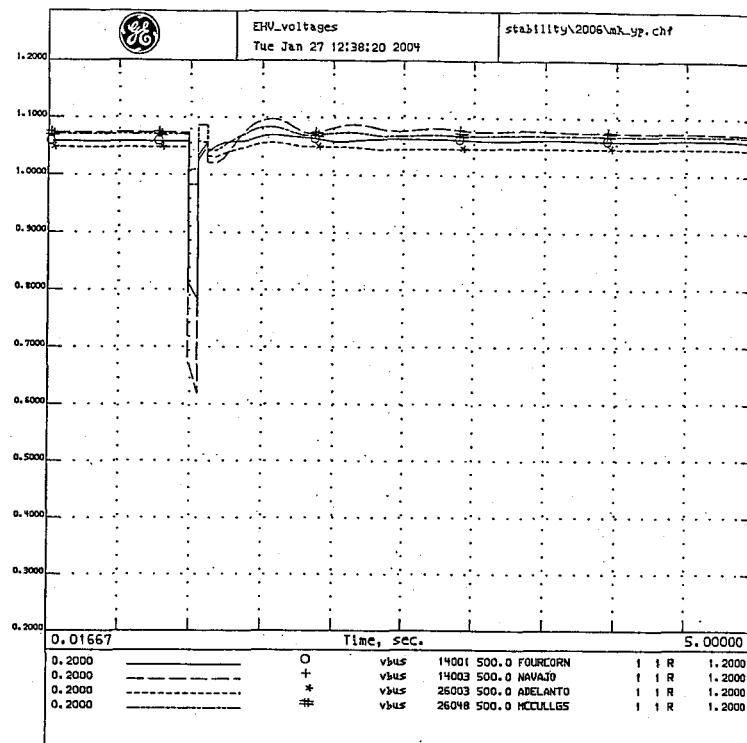
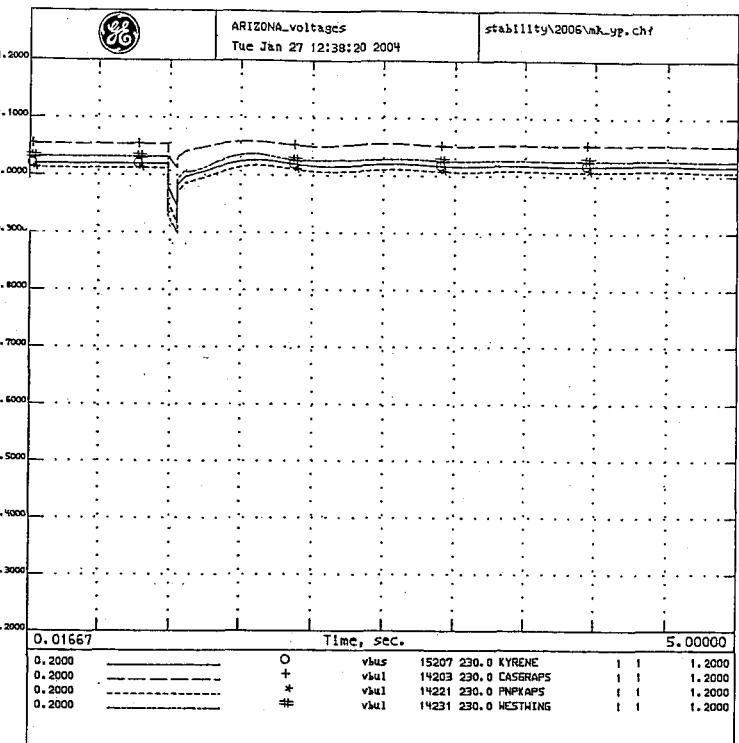
WESTERN ELECTRICITY COORDINATING COUNCIL  
LT. MKP line out  
OCTOBER 28, 2003  
MKP-ELD STAB1; 1/03; T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;HC CLR FLT H/MKP-ELD)8C REIN;2006.4y4;HSCL.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

WESTERN ELECTRICITY COORDINATING COUNCIL  
LT. MKP line out  
OCTOBER 28, 2003  
MKP-ELD STAB1; 1/03; T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;HC CLR FLT H/MKP-ELD)8C REIN;2006.4y4;HSCL.bat

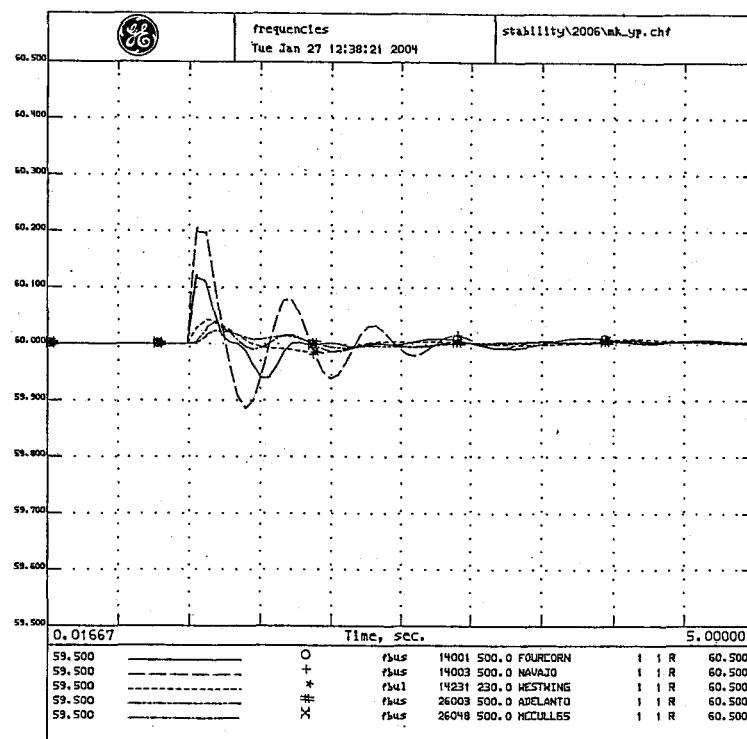
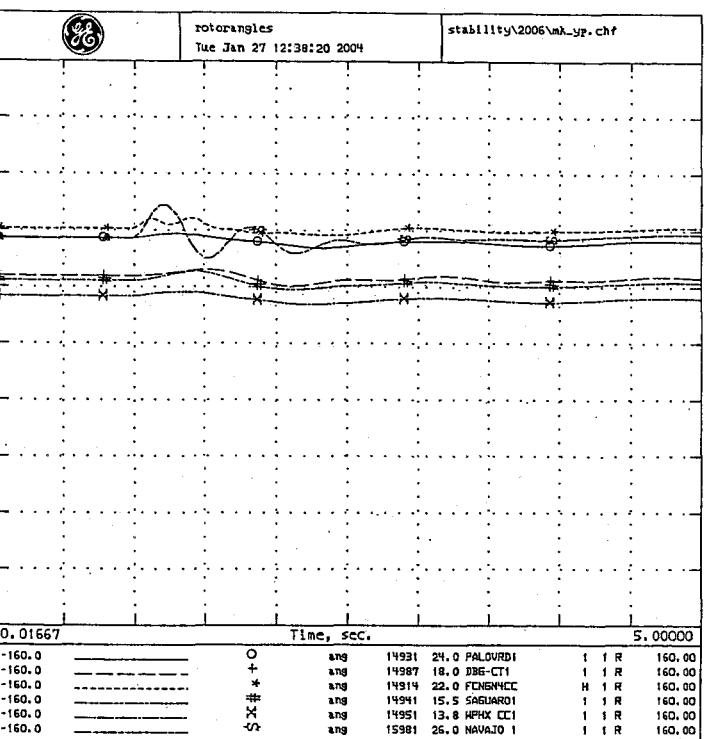
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B10



MKP. FLT MKP-YAV line out  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
MKP-YAV STAB; 1/03; T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-WNG,  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT H/MKP-YAV;8C REIN;2006.4y4;HSCL.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



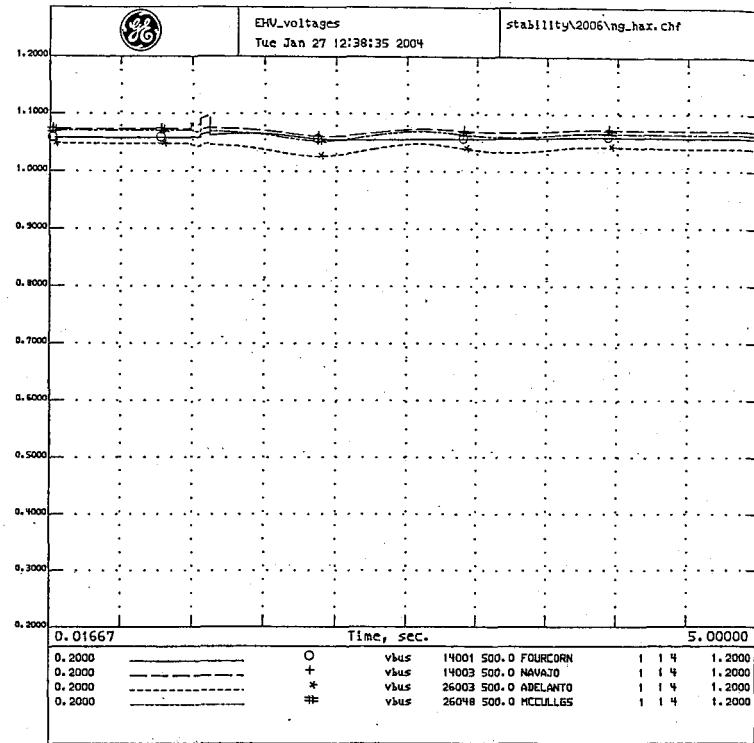
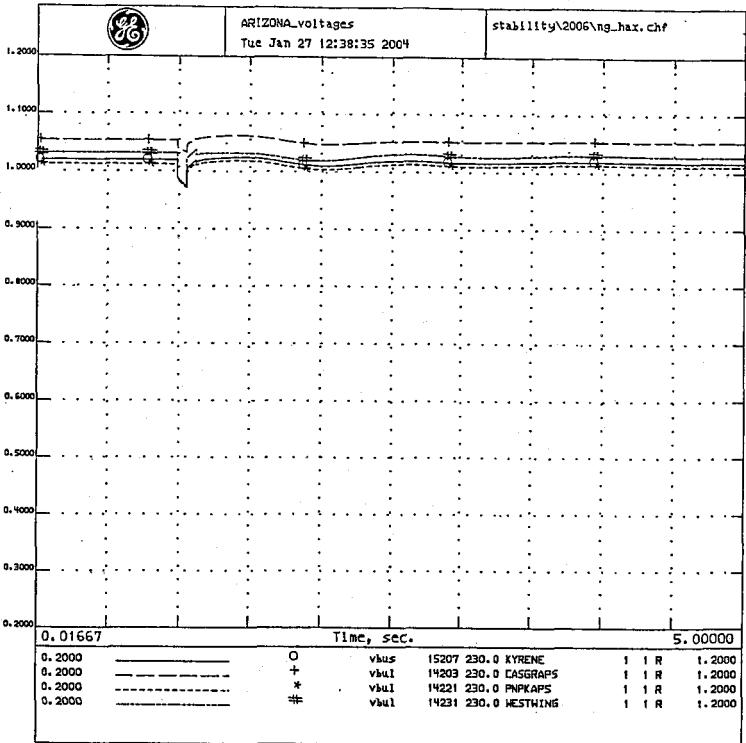
MKP. FLT MKP-YAV line out  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
MKP-YAV STAB; 1/03; T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-WNG,  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT H/MKP-YAV;8C REIN;2006.4y4;HSCL.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

MKP. FLT MKP-YAV line out  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
MKP-YAV STAB; 1/03; T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-WNG,  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT H/MKP-YAV;8C REIN;2006.4y4;HSCL.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B11

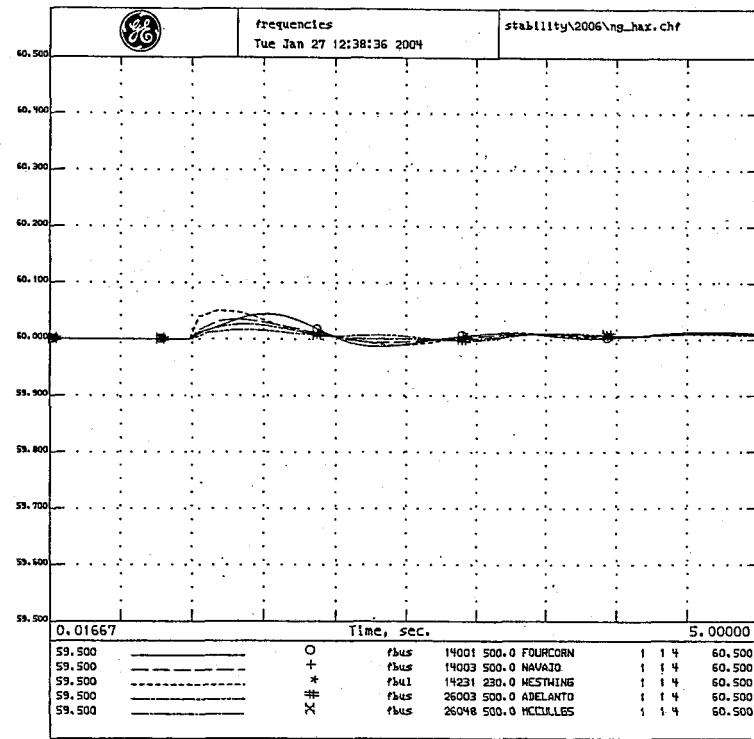
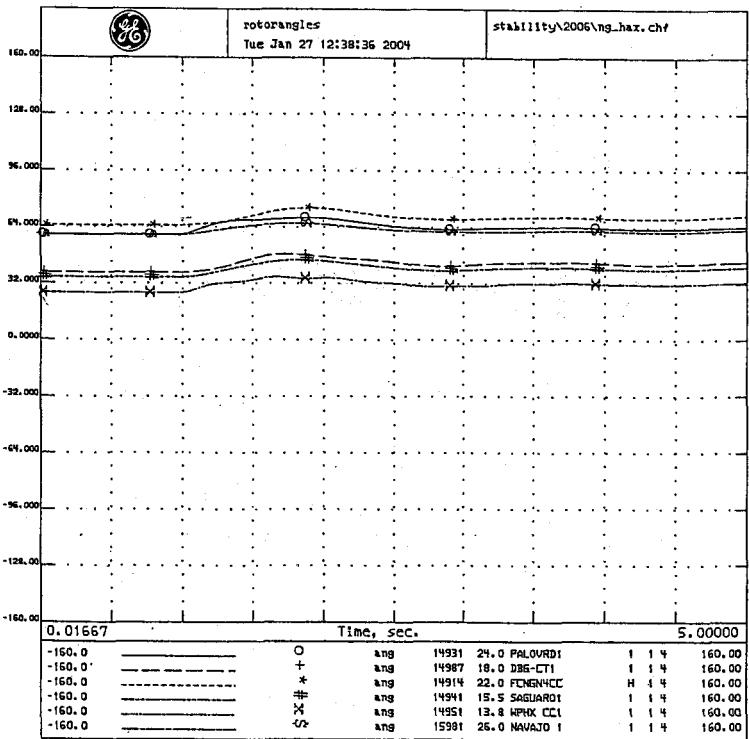


N. GILA FLT N. GILA-HASSY LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
N. GILA STAB, 3 PH FLT N. GILA 500KV  
FLASH CAPS, 4/4 CYC CLR FLT/HASSAYMPA-NG OUT; 4/8 CYC REIN CAPS

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

N. GILA FLT N. GILA-HASSY LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
N. GILA STAB, 3 PH FLT N. GILA 500KV  
FLASH CAPS, 4/4 CYC CLR FLT/HASSAYMPA-NG OUT; 4/8 CYC REIN CAPS

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



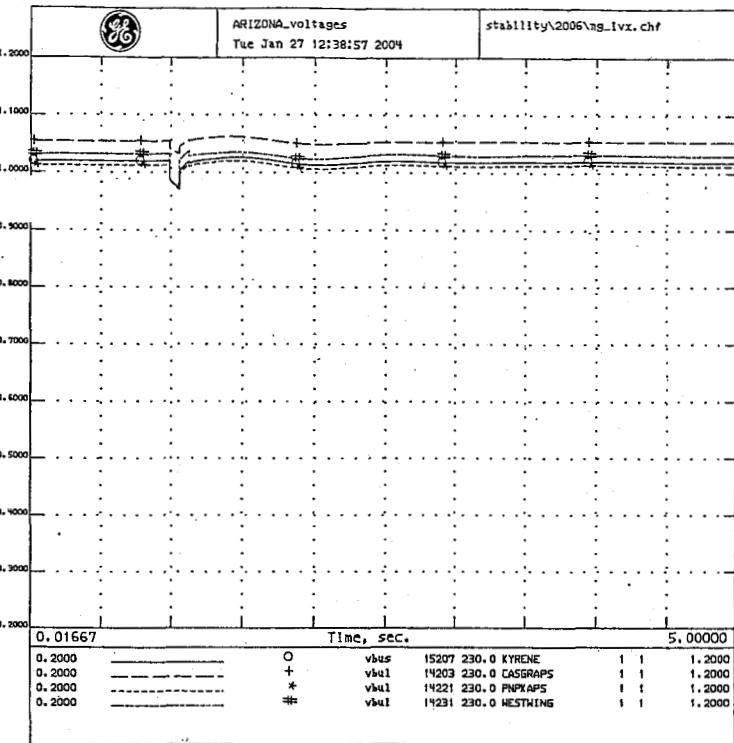
\*LA FLT N. GILA-HASSY LINE OUT  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
N. GILA STAB, 3 PH FLT N. GILA 500KV  
FLASH CAPS, 4/4 CYC CLR FLT/HASSAYMPA-NG OUT; 4/8 CYC REIN CAPS

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

\*LA FLT N. GILA-HASSY LINE OUT  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
N. GILA STAB, 3 PH FLT N. GILA 500KV  
FLASH CAPS, 4/4 CYC CLR FLT/HASSAYMPA-NG OUT; 4/8 CYC REIN CAPS

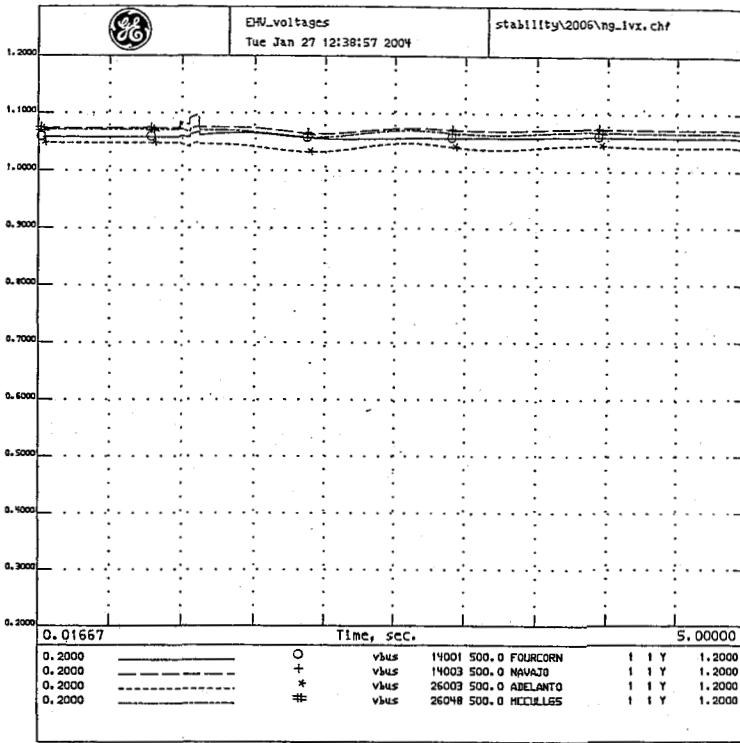
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

B12



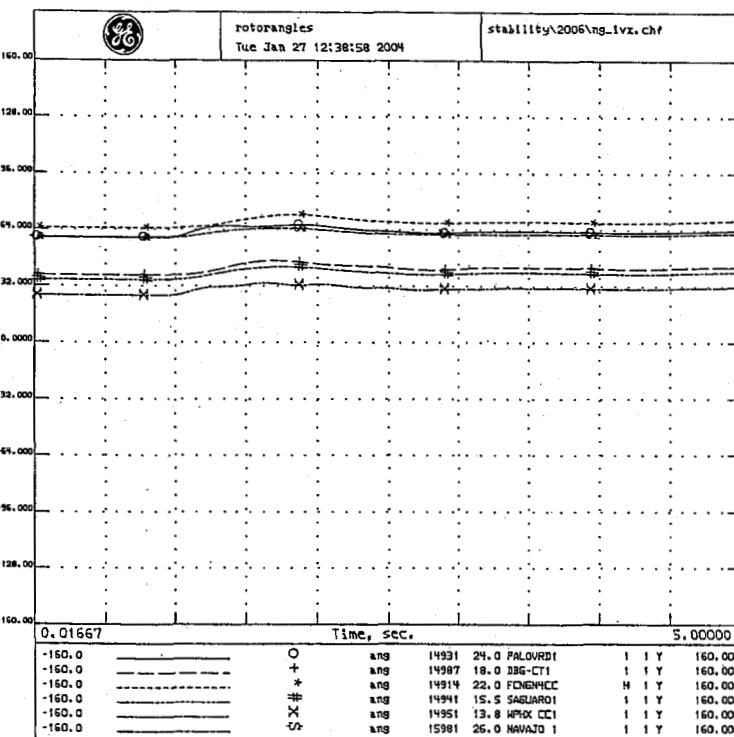
N.GILA FLT N.GILA-IMP. V LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
N.GILA STAB,3 PH FLT N.GILA 500KV  
FLASH CAPS,W/4 CYC CLR FLT;IMPU-NG OUT;4/8 CYC REIN CAPS

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



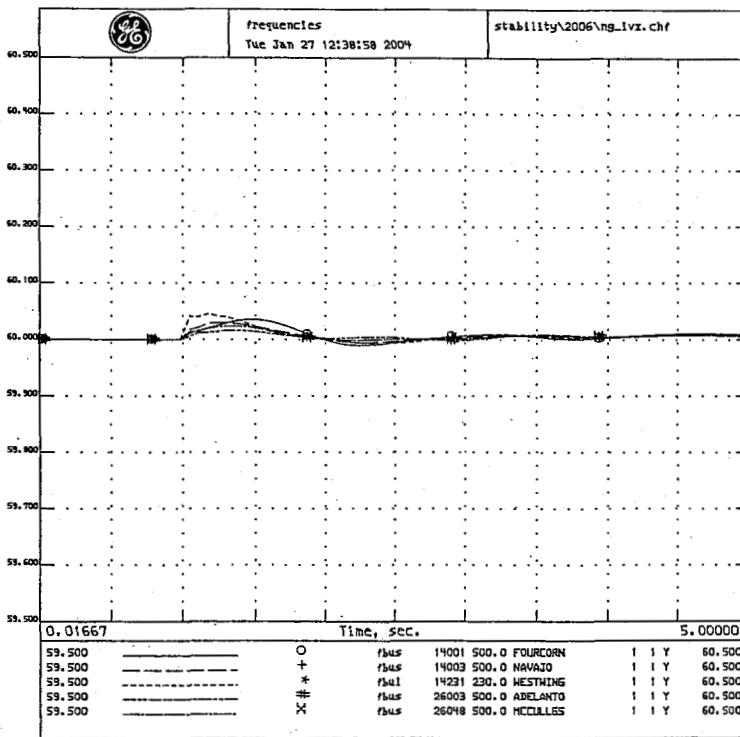
N.GILA FLT N.GILA-IMP. V LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
N.GILA STAB,3 PH FLT N.GILA 500KV  
FLASH CAPS,W/4 CYC CLR FLT;IMPU-NG OUT;4/8 CYC REIN CAPS

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



N.GILA FLT N.GILA-IMP. V LINE OUT  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
N.GILA STAB,3 PH FLT N.GILA 500KV  
FLASH CAPS,W/4 CYC CLR FLT;IMPU-NG OUT;4/8 CYC REIN CAPS

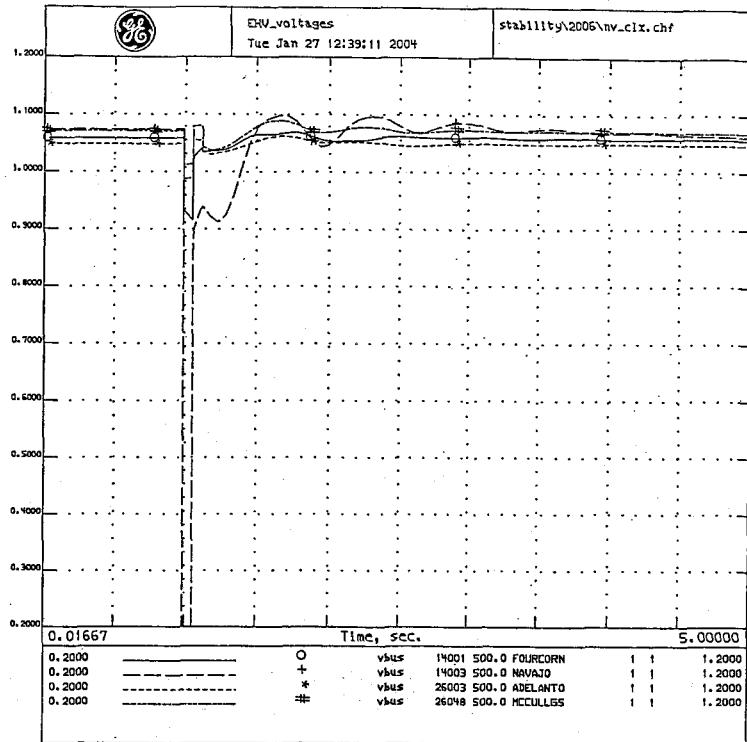
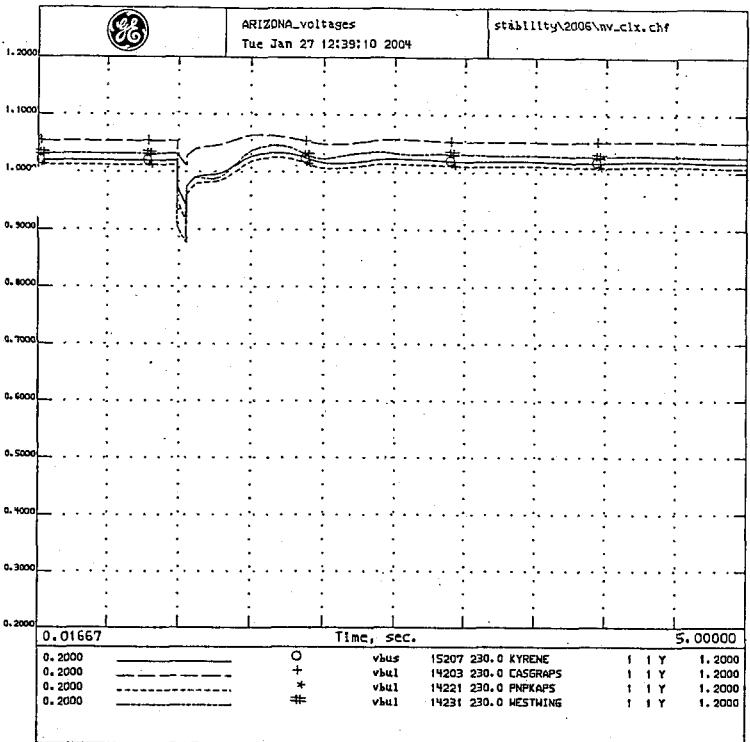
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



N.GILA FLT N.GILA-IMP. V LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
N.GILA STAB,3 PH FLT N.GILA 500KV  
FLASH CAPS,W/4 CYC CLR FLT;IMPU-NG OUT;4/8 CYC REIN CAPS

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

B13

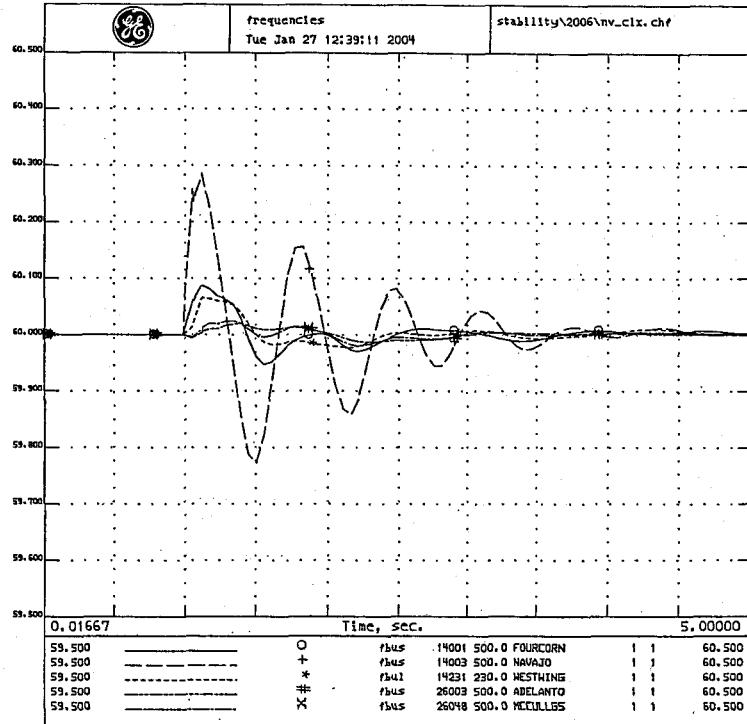
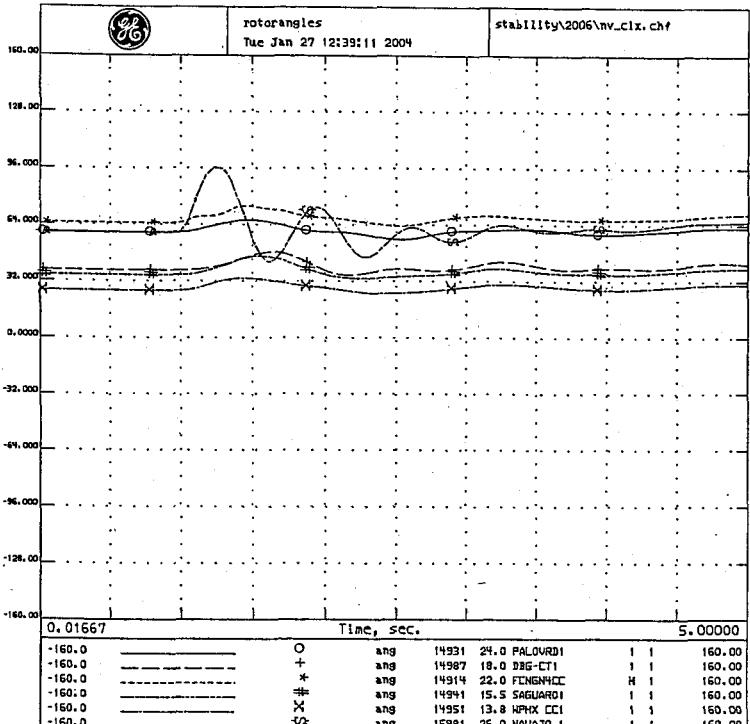


WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV\_FLT\_Nav-Crystal line out  
OCTOBER 28, 2003  
NAV-CRYS STAB: 1/03; T=0 3P FLT NAV500; 6% FLT DMPING;FLSH CAPS  
NAV-HLD/HKP,HKP-ELD)4C CLR FLT W/NAV-CRYS;BC REIN;2006\_dyd;WSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV\_FLT\_Nav-Crystal line out  
OCTOBER 28, 2003  
NAV-CRYS STAB: 1/03; T=0 3P FLT NAV500; 6% FLT DMPING;FLSH CAPS  
NAV-HLD/HKP,HKP-ELD)4C CLR FLT W/NAV-CRYS;BC REIN;2006\_dyd;WSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



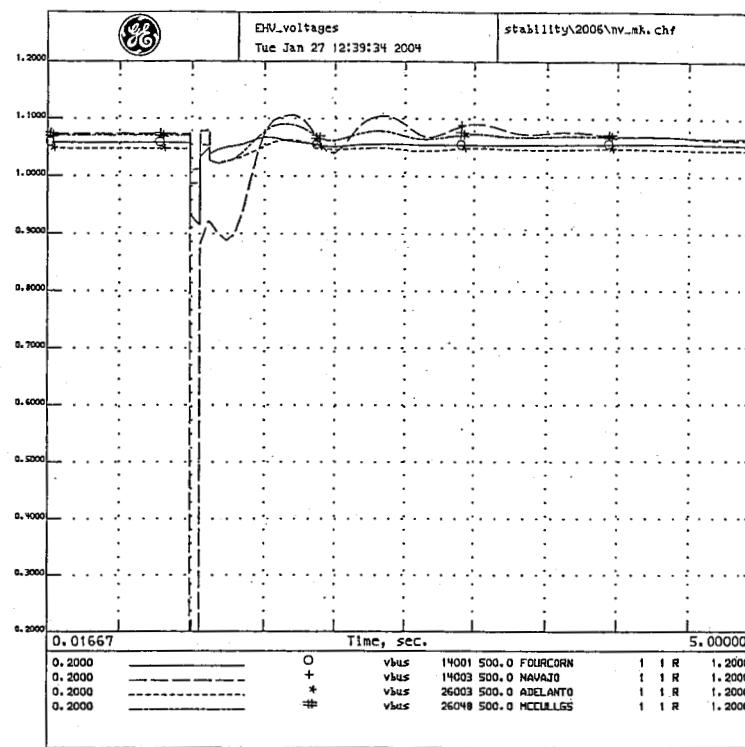
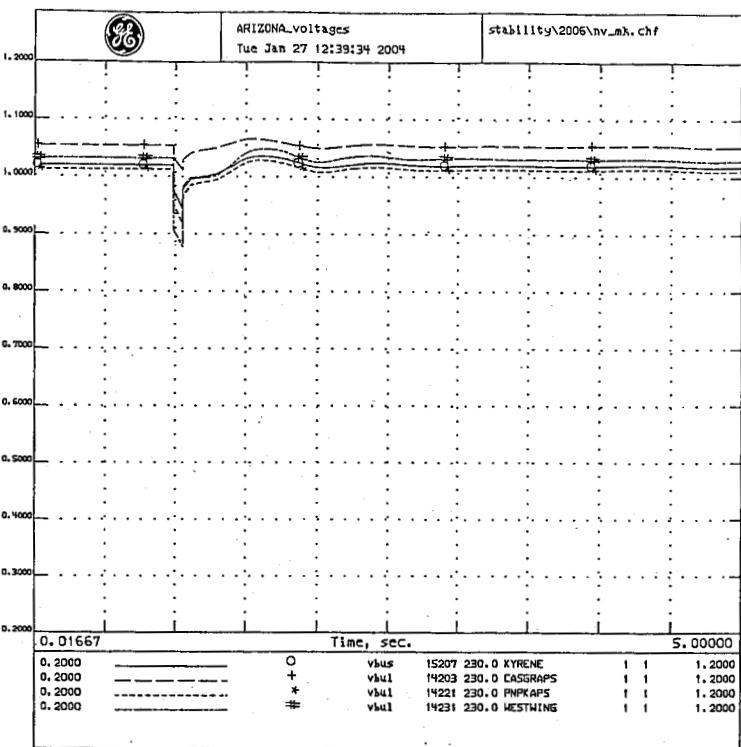
WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV\_FLT\_Nav-Crystal line out  
OCTOBER 28, 2003  
NAV-CRYS STAB: 1/03; T=0 3P FLT NAV500; 6% FLT DMPING;FLSH CAPS  
NAV-HLD/HKP,HKP-ELD)4C CLR FLT W/NAV-CRYS;BC REIN;2006\_dyd;WSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV\_FLT\_Nav-Crystal line out  
OCTOBER 28, 2003  
NAV-CRYS STAB: 1/03; T=0 3P FLT NAV500; 6% FLT DMPING;FLSH CAPS  
NAV-HLD/HKP,HKP-ELD)4C CLR FLT W/NAV-CRYS;BC REIN;2006\_dyd;WSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

B14

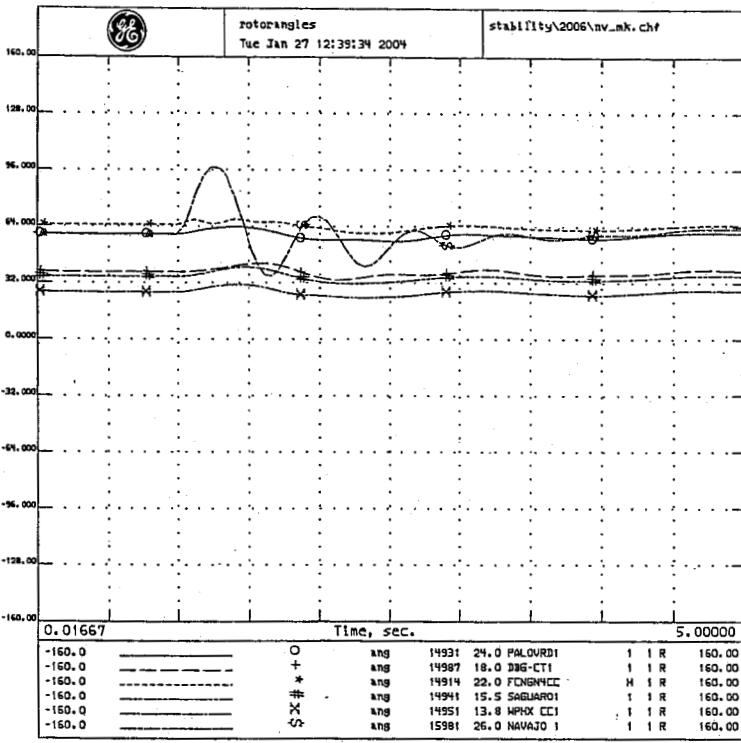


WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV. FLT. Navajo-Mnk. line out  
OCTOBER 28, 2003  
NAV-MKP STAB1 1/03; T=0 3P FLT NAV500; 6X FLT IMPING;FLSH CAPS  
NAV-HCC/MKP,MKP-ELD;4C CLR FLT W/NAV-MKP;8C REIN;2006.4y4;HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

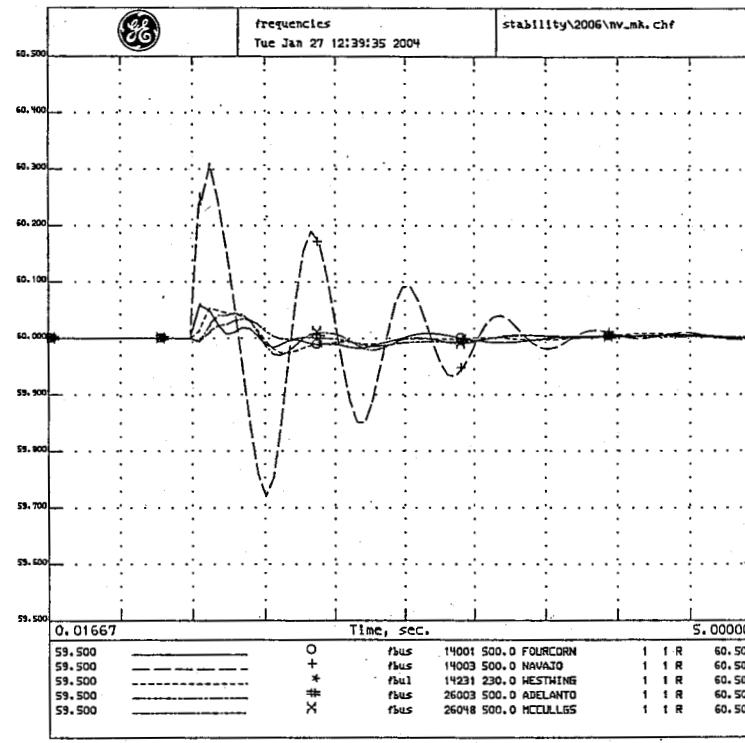
WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV. FLT. Navajo-Mnk. line out  
OCTOBER 28, 2003  
NAV-MKP STAB1 1/03; T=0 3P FLT NAV500; 6X FLT IMPING;FLSH CAPS  
NAV-HCC/MKP,MKP-ELD;4C CLR FLT W/NAV-MKP;8C REIN;2006.4y4;HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
FLT. Navajo-Mnk. line out  
ER 28, 2003  
----MKP STAB1 1/03; T=0 3P FLT NAV500; 6X FLT IMPING;FLSH CAPS  
NAV-HCC/MKP,MKP-ELD;4C CLR FLT W/NAV-MKP;8C REIN;2006.4y4;HSCC.bat

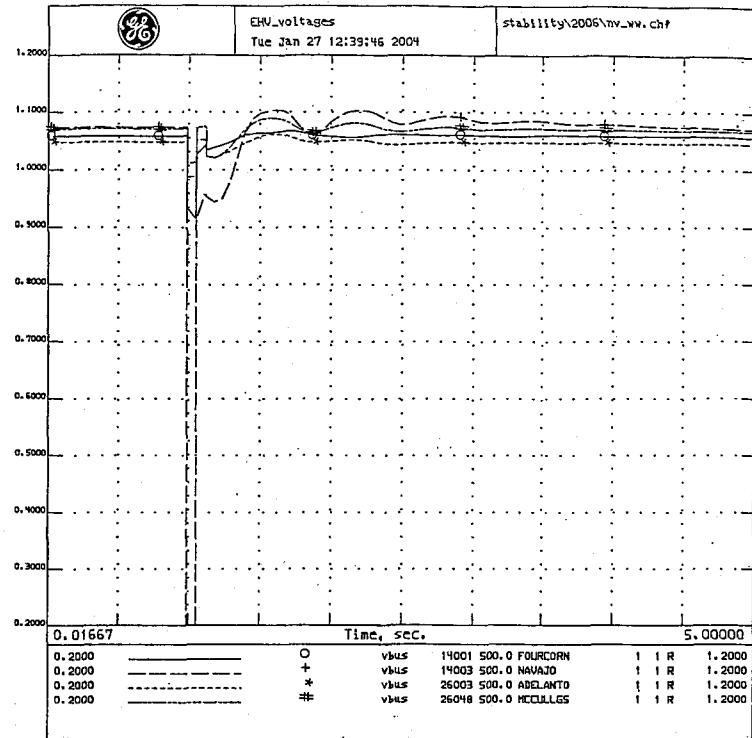
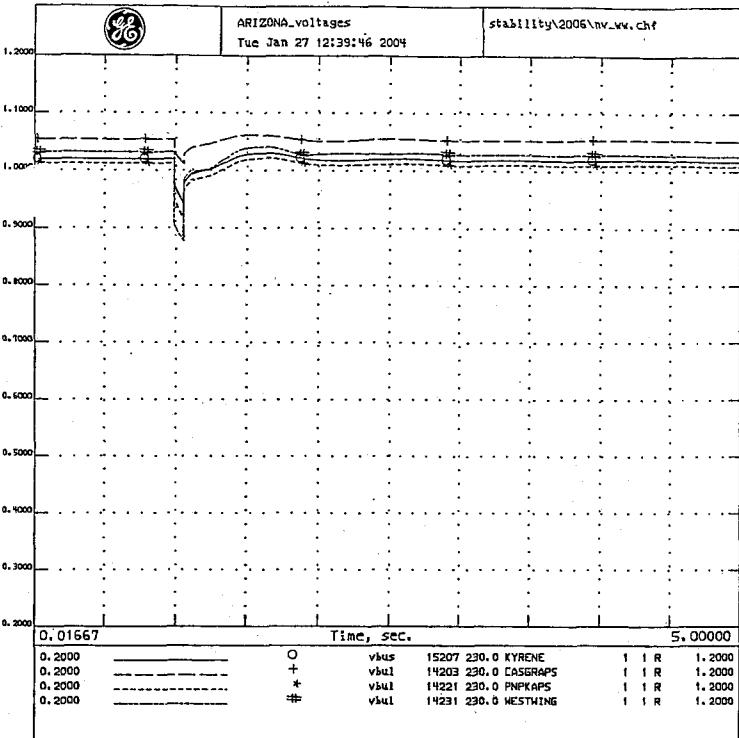
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV. FLT. Navajo-Mnk. line out  
OCTOBER 28, 2003  
NAV-MKP STAB1 1/03; T=0 3P FLT NAV500; 6X FLT IMPING;FLSH CAPS  
NAV-HCC/MKP,MKP-ELD;4C CLR FLT W/NAV-MKP;8C REIN;2006.4y4;HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

B15

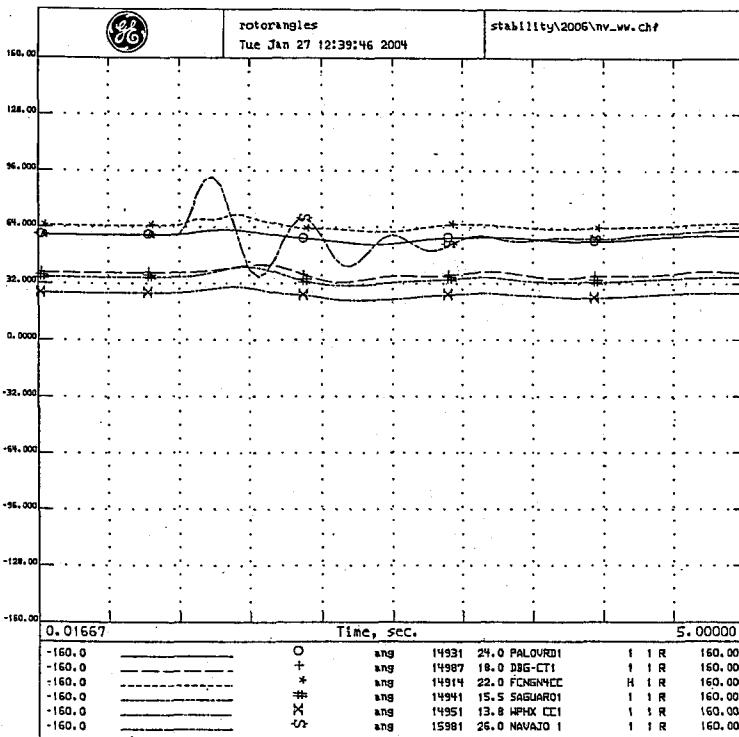


NAU FLT NAV-HM LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
NAU-HMG STAB1 1/03; T=0 3P FLT NAV500; 6% FLT IMPING; FLSH CAPS  
NAV-MCC/MKP,MKP-ELD)4C CLR FLT W/NAV-HMG;BC REIN;2006.4y4;HSCL.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

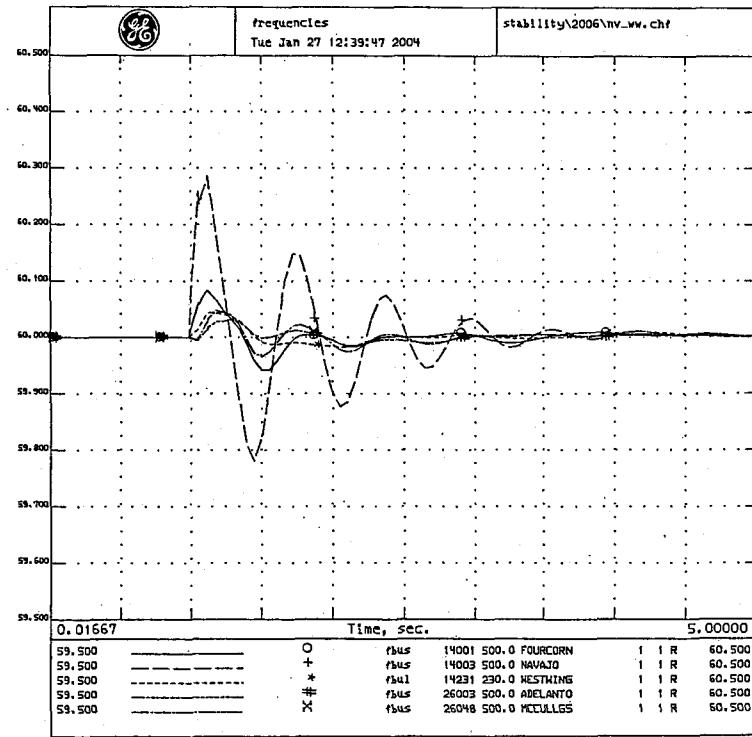
NAU FLT NAV-HM LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
NAU-HMG STAB1 1/03; T=0 3P FLT NAV500; 6% FLT IMPING; FLSH CAPS  
NAV-MCC/MKP,MKP-ELD)4C CLR FLT W/NAV-HMG;BC REIN;2006.4y4;HSCL.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



FLT NAV-HM LINE OUT  
HS3-SA APPROVED BASE CASE  
OCT 28, 2003  
NAU-HMG STAB1 1/03; T=0 3P FLT NAV500; 6% FLT IMPING; FLSH CAPS  
NAV-MCC/MKP,MKP-ELD)4C CLR FLT W/NAV-HMG;BC REIN;2006.4y4;HSCL.bat

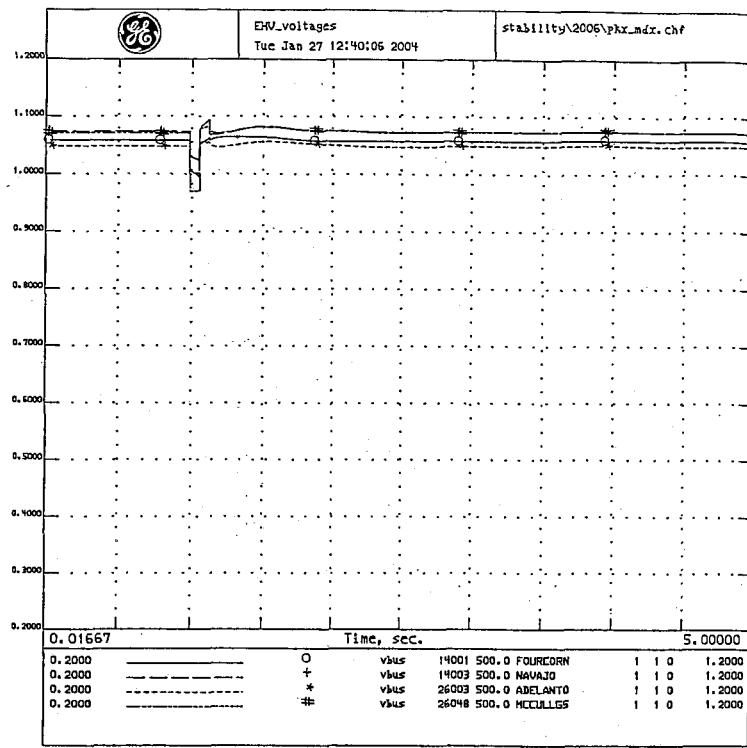
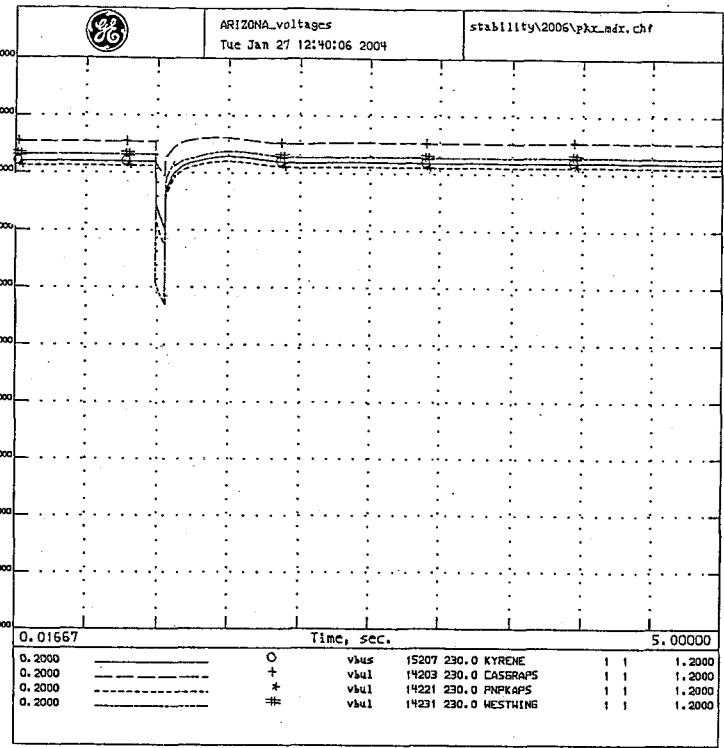
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



NAU FLT NAV-HM LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
NAU-HMG STAB1 1/03; T=0 3P FLT NAV500; 6% FLT IMPING; FLSH CAPS  
NAV-MCC/MKP,MKP-ELD)4C CLR FLT W/NAV-HMG;BC REIN;2006.4y4;HSCL.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B16

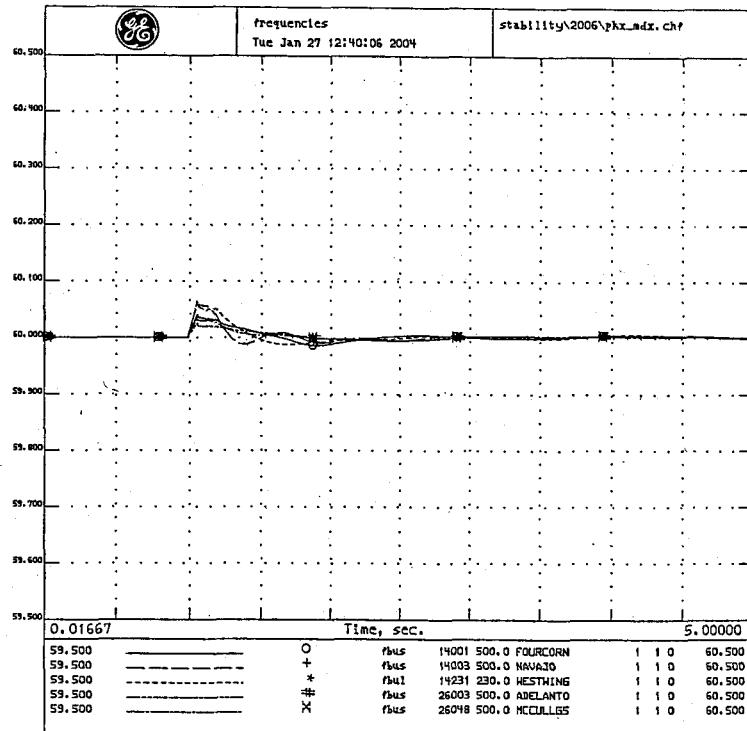
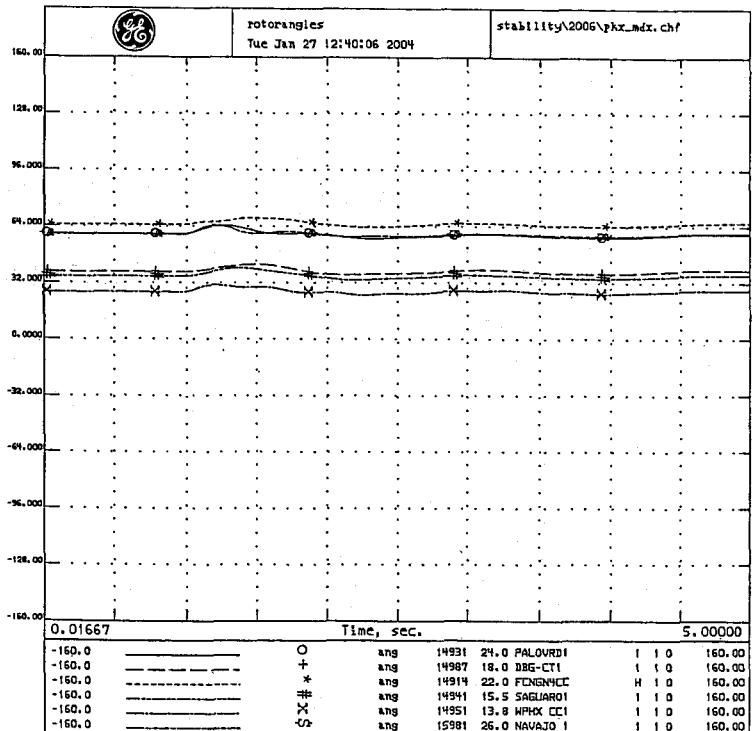


PERKINS FLT PERKINS-MEAD LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PERK-MEAD STAB; 01/03; T=0 3P FLT PERKS00;FLSH CAPS MKP-YAU/YAU-HNG,  
NAV-MKP/HNG;4C CLR FLT W/PERK-MEAD;8C REIN;2006, d4d1HSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

PERKINS FLT PERKINS-MEAD LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PERK-MEAD STAB; 01/03; T=0 3P FLT PERKS00;FLSH CAPS MKP-YAU/YAU-HNG,  
NAV-MKP/HNG;4C CLR FLT W/PERK-MEAD;8C REIN;2006, d4d1HSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



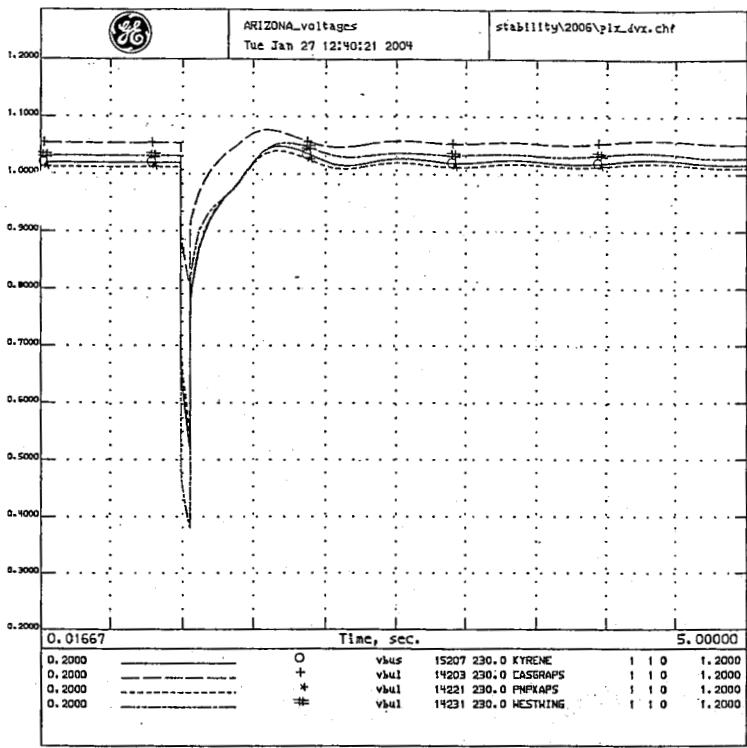
PERKINS FLT PERKINS-MEAD LINE OUT  
HS3-SA APPROVED BASE CASE  
ER 28, 2003  
PERK-MEAD STAB; 01/03; T=0 3P FLT PERKS00;FLSH CAPS MKP-YAU/YAU-HNG,  
NAV-MKP/HNG;4C CLR FLT W/PERK-MEAD;8C REIN;2006, d4d1HSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

PERKINS FLT PERKINS-MEAD LINE OUT  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PERK-MEAD STAB; 01/03; T=0 3P FLT PERKS00;FLSH CAPS MKP-YAU/YAU-HNG,  
NAV-MKP/HNG;4C CLR FLT W/PERK-MEAD;8C REIN;2006, d4d1HSCE.bat

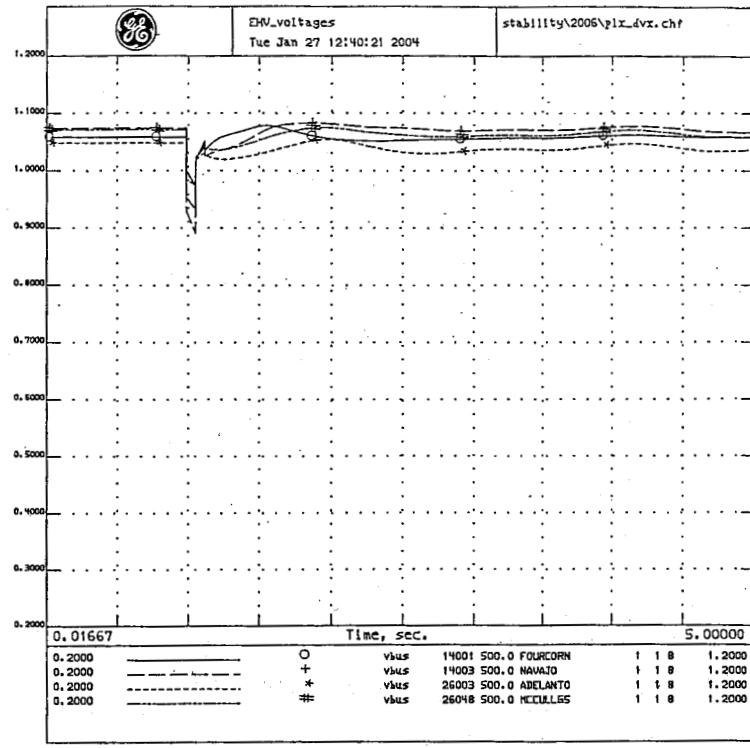
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B17



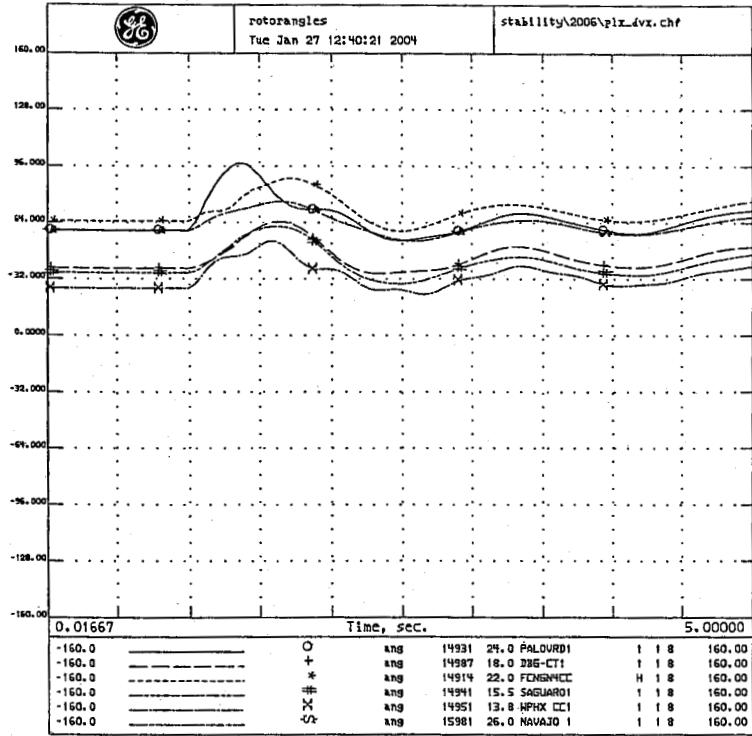
WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. w/PV - Devers line out  
OCTOBER 28, 2003  
PV-DEV STAB1 1/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG;4C CLR FLT W/PV-DEVBC REIN;2006.4y4;HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



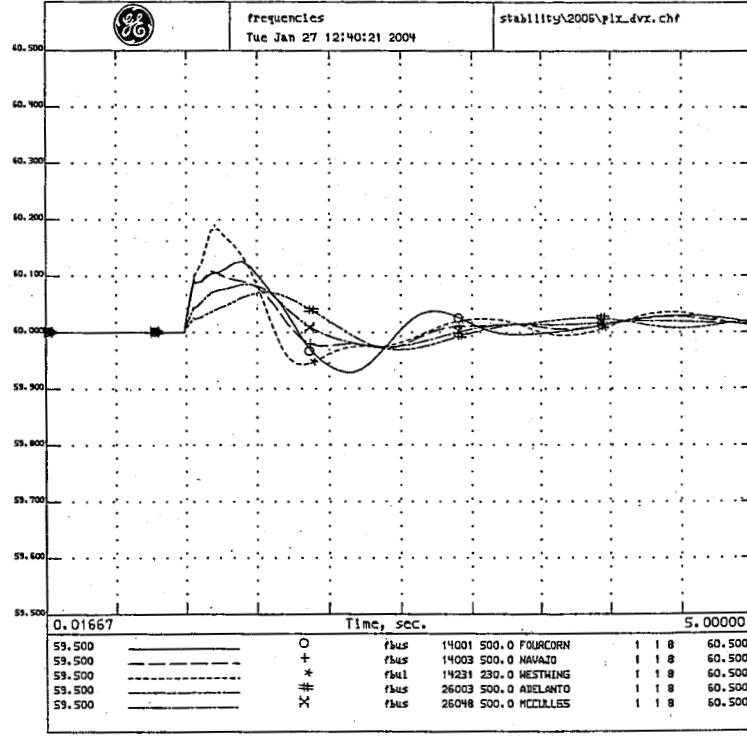
WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. w/PV - Devers line out  
OCTOBER 28, 2003  
PV-DEV STAB1 1/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG;4C CLR FLT W/PV-DEVBC REIN;2006.4y4;HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
LT. w/PV - Devers line out  
OCTOBER 28, 2003  
PV-DEV STAB1 1/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG;4C CLR FLT W/PV-DEVBC REIN;2006.4y4;HSCC.bat

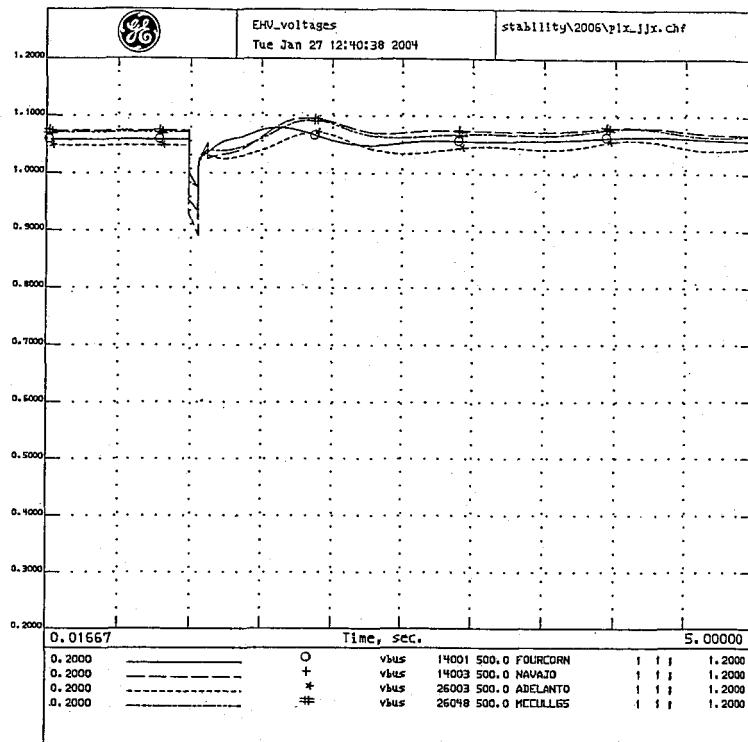
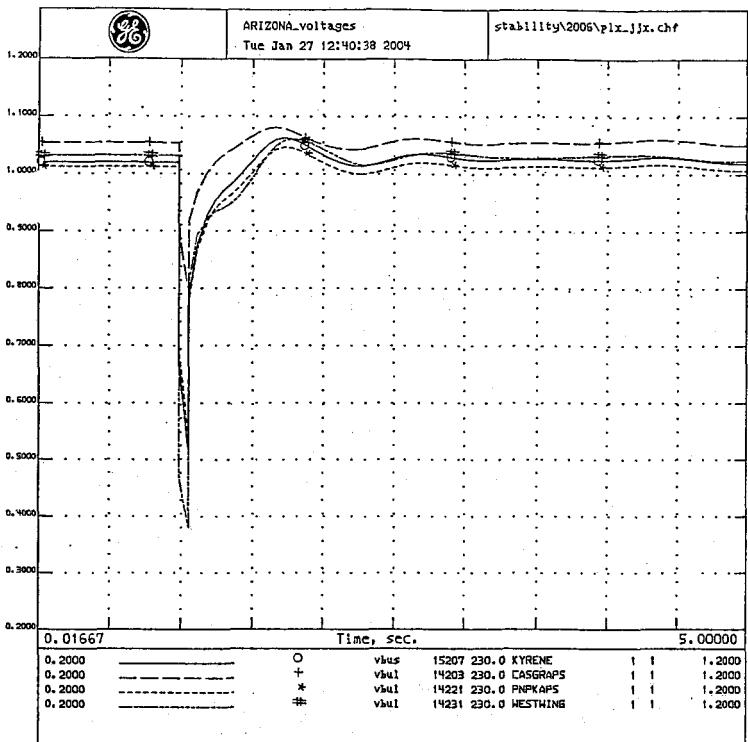
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. w/PV - Devers line out  
OCTOBER 28, 2003  
PV-DEV STAB1 1/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG;4C CLR FLT W/PV-DEVBC REIN;2006.4y4;HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

B18

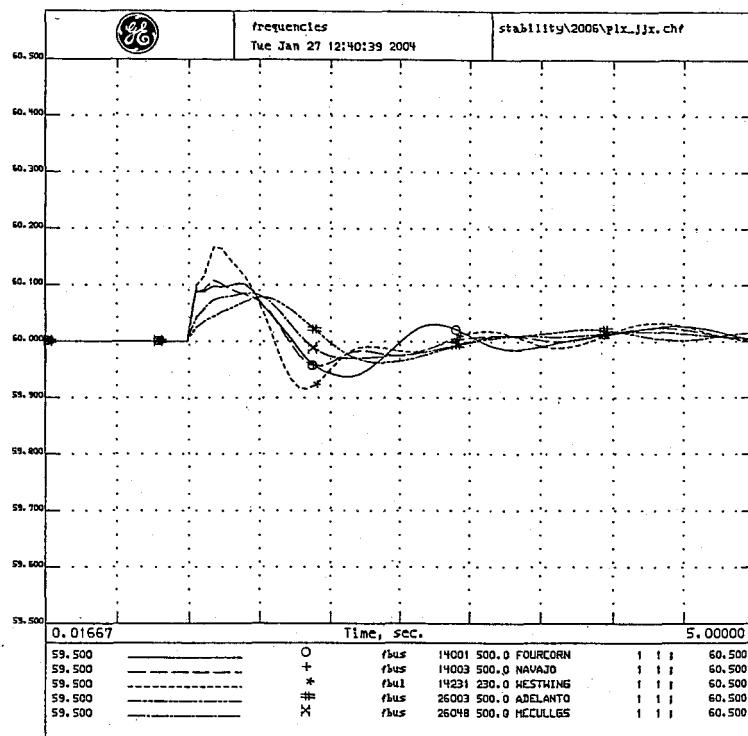
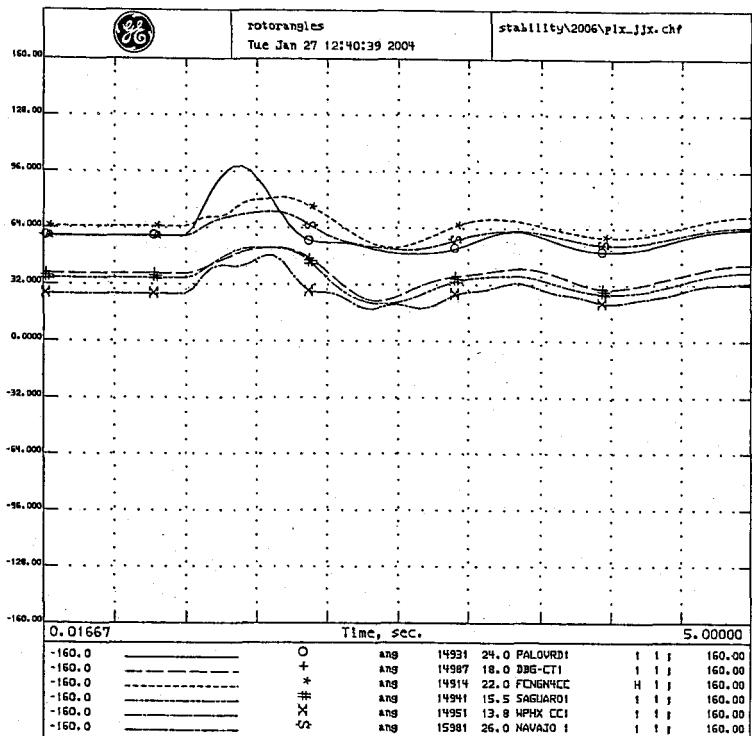


PALO VERDE FLT HASSY-JOJOBA LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
HAS-JJ STAB +11 01/03; T=0 3P FLT PV500;10X FLT DMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/HAS-JJ;8C REIN;2006.4y4;HSCE.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

PALO VERDE FLT HASSY-JOJOBA LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
HAS-JJ STAB +11 01/03; T=0 3P FLT PV500;10X FLT DMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/HAS-JJ;8C REIN;2006.4y4;HSCE.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



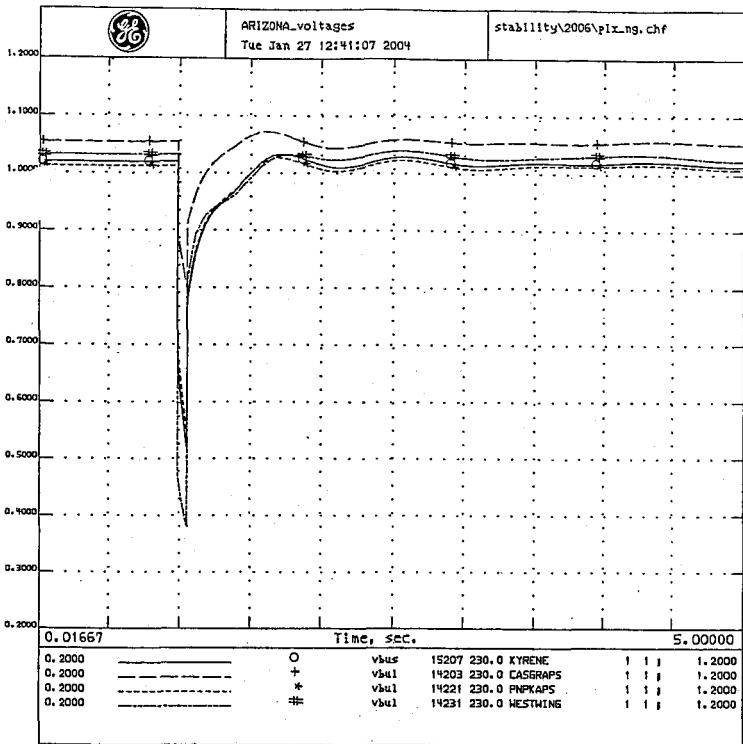
PALO VERDE FLT HASSY-JOJOBA LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
HAS-JJ STAB +11 01/03; T=0 3P FLT PV500;10X FLT DMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/HAS-JJ;8C REIN;2006.4y4;HSCE.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

PALO VERDE FLT HASSY-JOJOBA LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
HAS-JJ STAB +11 01/03; T=0 3P FLT PV500;10X FLT DMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/HAS-JJ;8C REIN;2006.4y4;HSCE.bpt

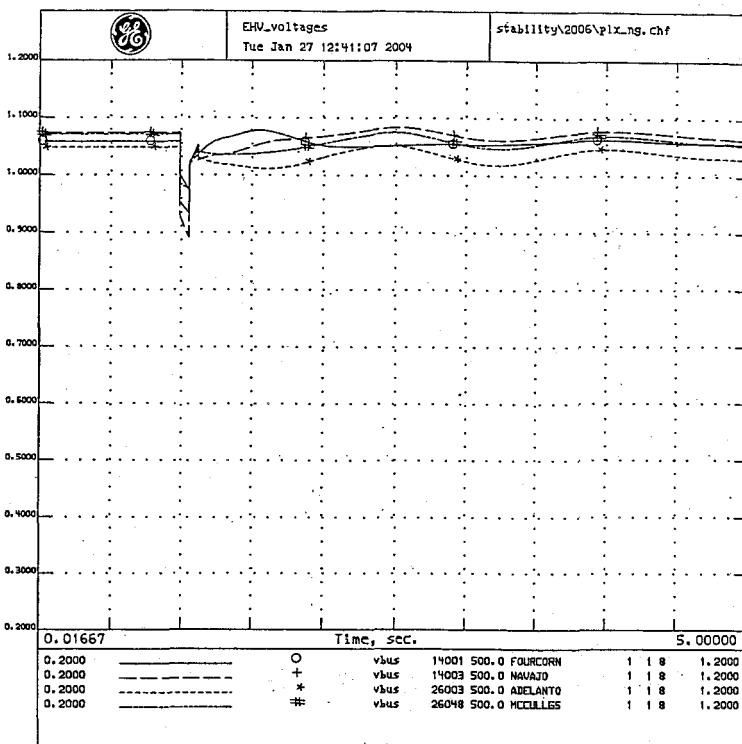
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

B19



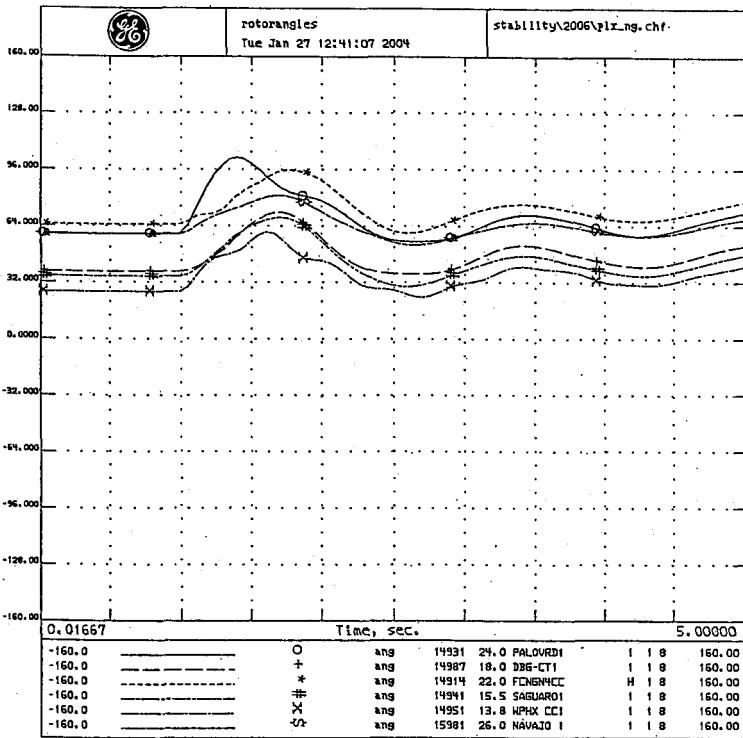
WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. W/HASSY-N.GILA line out  
OCTOBER 28, 2003  
PV-NGILA STAB1 1/03; T=0 3P FLT PV500;10X FLT DMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG;4C CLR FLT W/PV-NG1BC REIN12006.4y4;HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



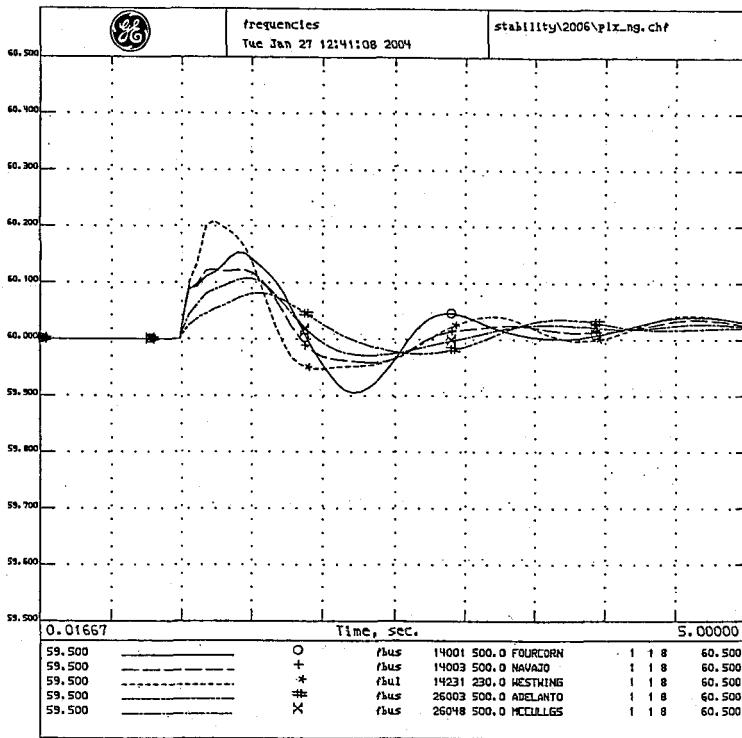
WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. W/HASSY-N.GILA line out  
OCTOBER 28, 2003  
PV-NGILA STAB1 1/03; T=0 3P FLT PV500;10X FLT DMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG;4C CLR FLT W/PV-NG1BC REIN12006.4y4;HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. W/HASSY-N.GILA line out  
OCTOBER 28, 2003  
PV-NGILA STAB1 1/03; T=0 3P FLT PV500;10X FLT DMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG;4C CLR FLT W/PV-NG1BC REIN12006.4y4;HSCC.bat

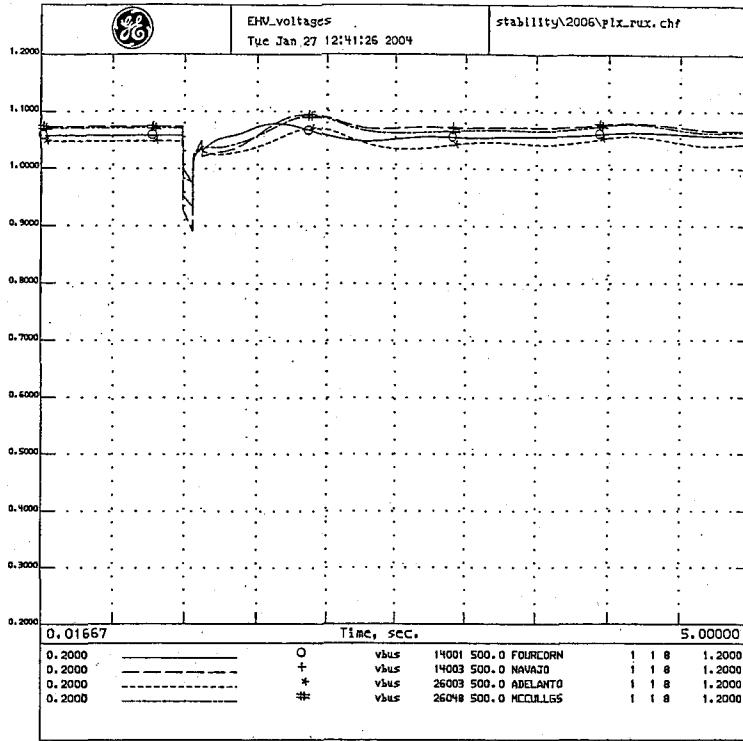
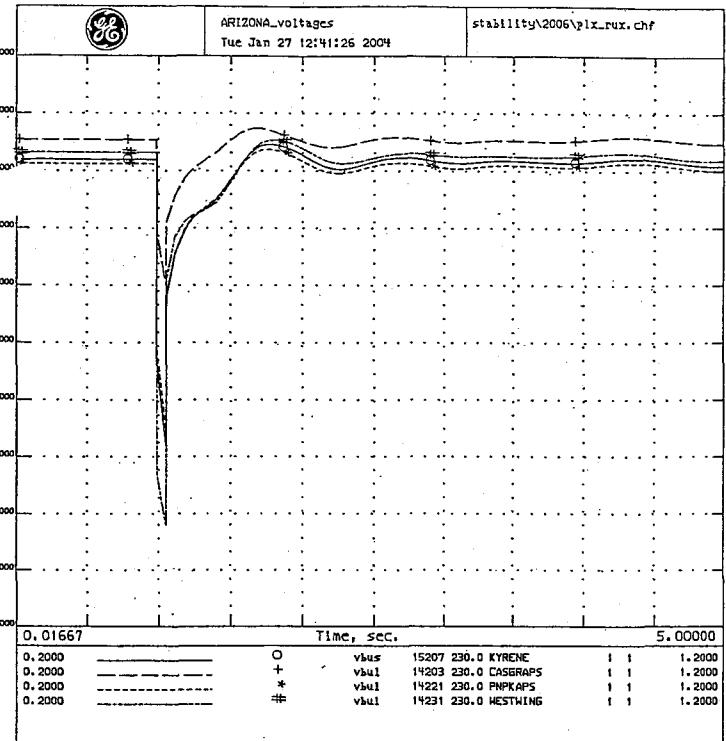
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. W/HASSY-N.GILA line out  
OCTOBER 28, 2003  
PV-NGILA STAB1 1/03; T=0 3P FLT PV500;10X FLT DMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG;4C CLR FLT W/PV-NG1BC REIN12006.4y4;HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B20

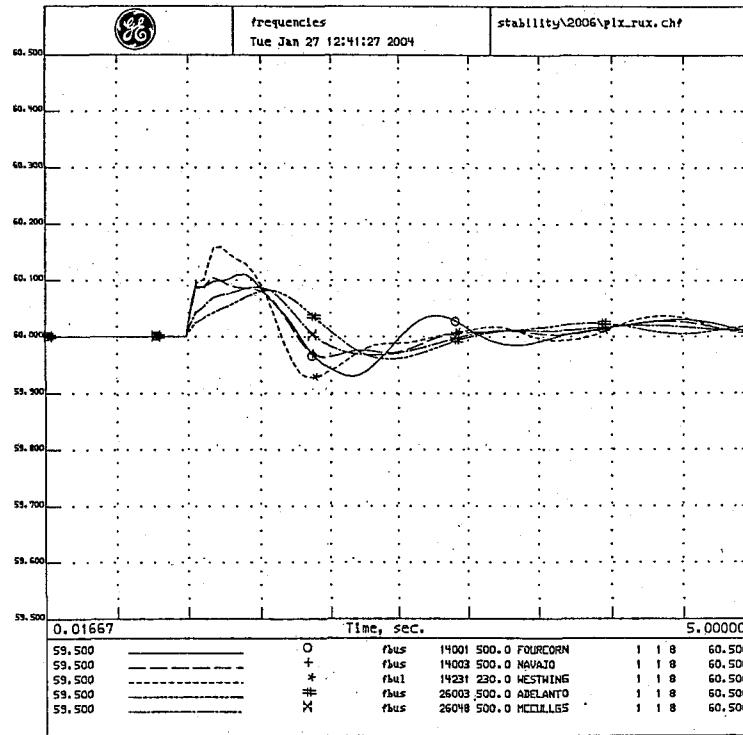
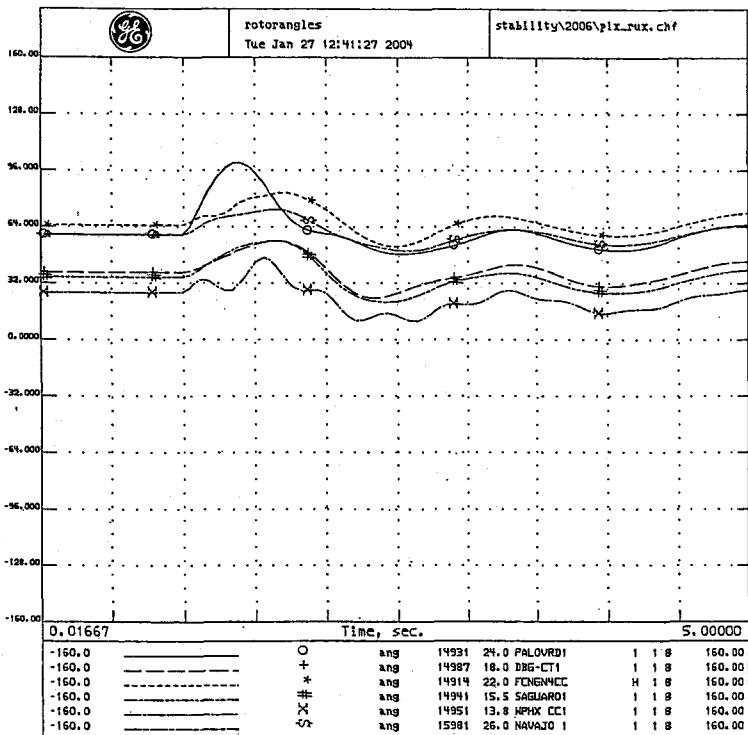


PALO VERDE FLT PV-RUDD LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT PV500;10% FLT DMPNG;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/PV-RD;8C REIN;2006.4y4;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

PALO VERDE FLT PV-RUDD LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT PV500;10% FLT DMPNG;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/PV-RD;8C REIN;2006.4y4;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



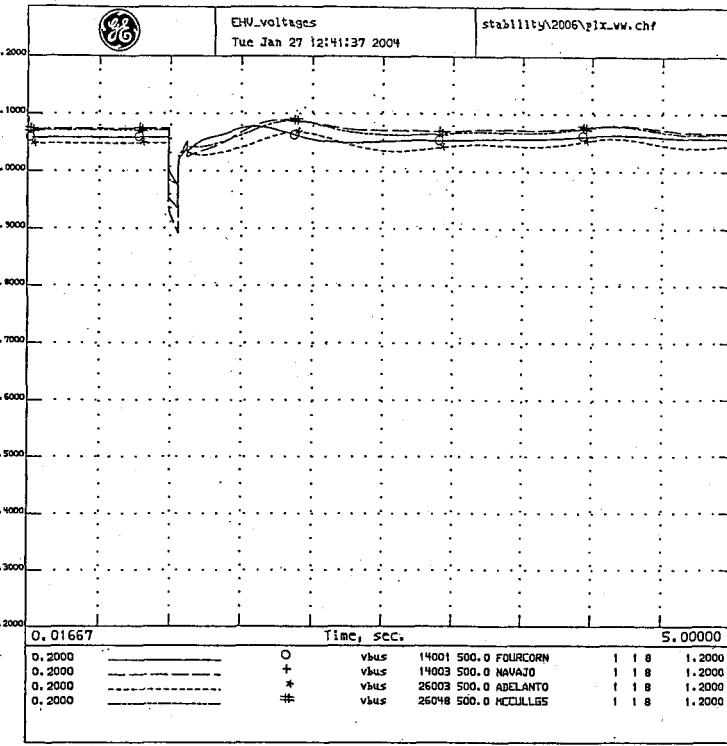
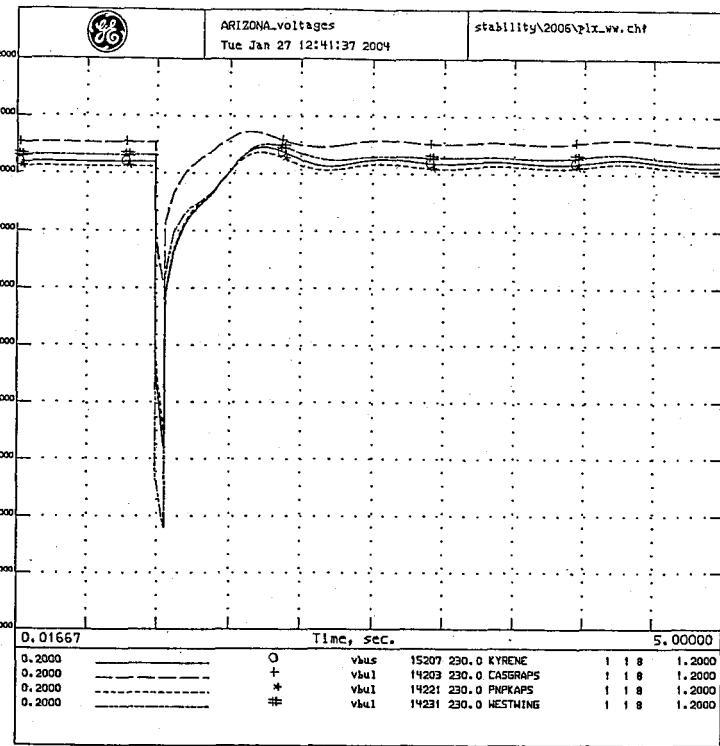
PALO VERDE FLT PV-RUDD LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT PV500;10% FLT DMPNG;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/PV-RD;8C REIN;2006.4y4;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

PALO VERDE FLT PV-RUDD LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT PV500;10% FLT DMPNG;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/PV-RD;8C REIN;2006.4y4;HSCC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

B21

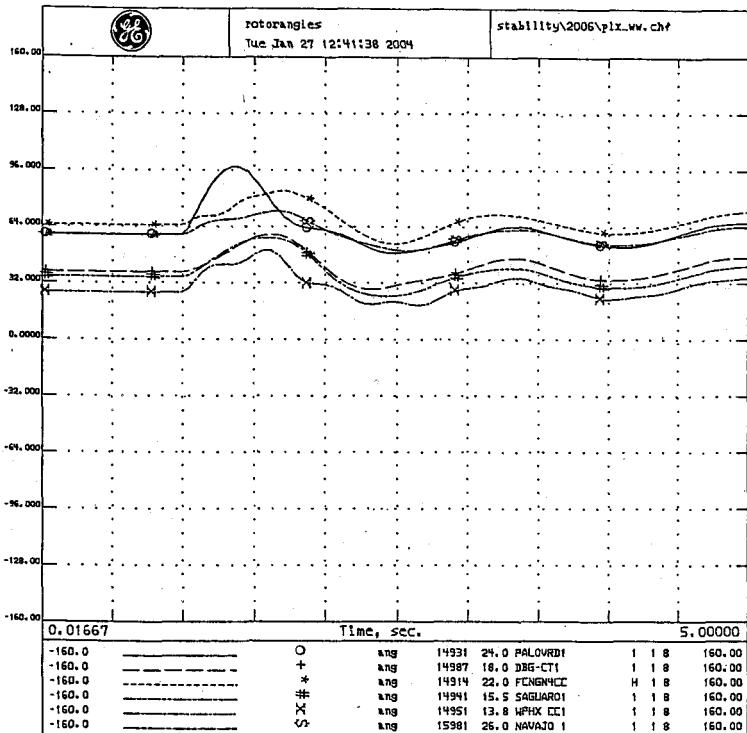


WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT W/PV-WH line out  
OCTOBER 28, 2003  
PV-HWG STAB1 1/03; T=0 3P FLT PV500|10% FLT DMPNG;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NGHC CLR FLT W/PV-WH;BC REIN|2006.4y4;WSCC,bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

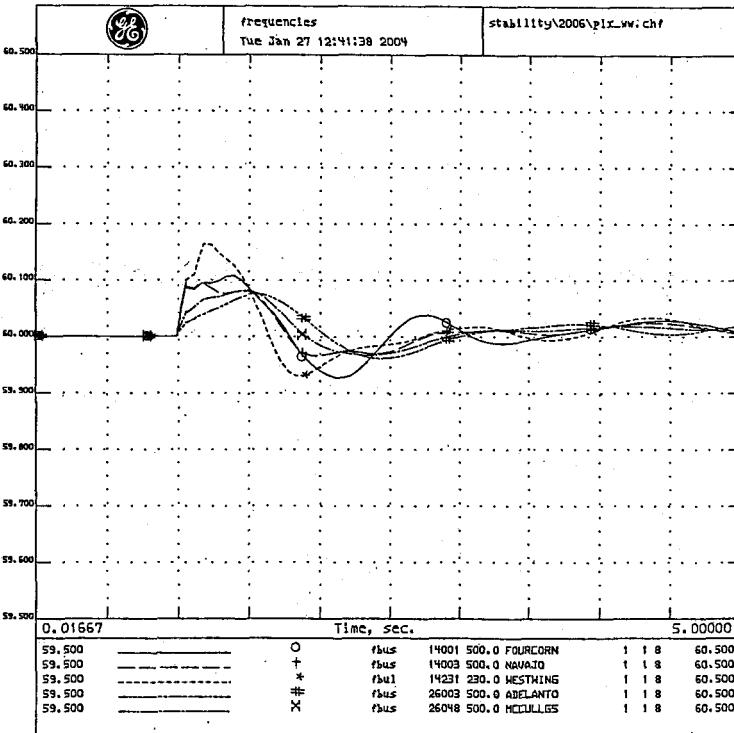
WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT W/PV-WH line out  
OCTOBER 28, 2003  
PV-HWG STAB1 1/03; T=0 3P FLT PV500|10% FLT DMPNG;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NGHC CLR FLT W/PV-WH;BC REIN|2006.4y4;WSCC,bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT W/PV-WH line out  
OCTOBER 28, 2003  
PV-HWG STAB1 1/03; T=0 3P FLT PV500|10% FLT DMPNG;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NGHC CLR FLT W/PV-WH;BC REIN|2006.4y4;WSCC,bat

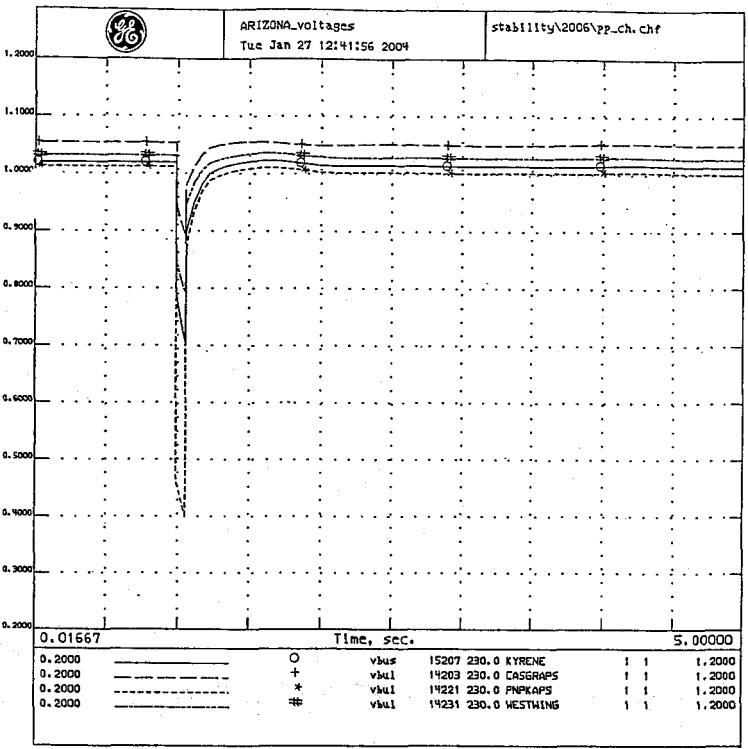
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT W/PV-WH line out  
OCTOBER 28, 2003  
PV-HWG STAB1 1/03; T=0 3P FLT PV500|10% FLT DMPNG;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NGHC CLR FLT W/PV-WH;BC REIN|2006.4y4;WSCC,bat

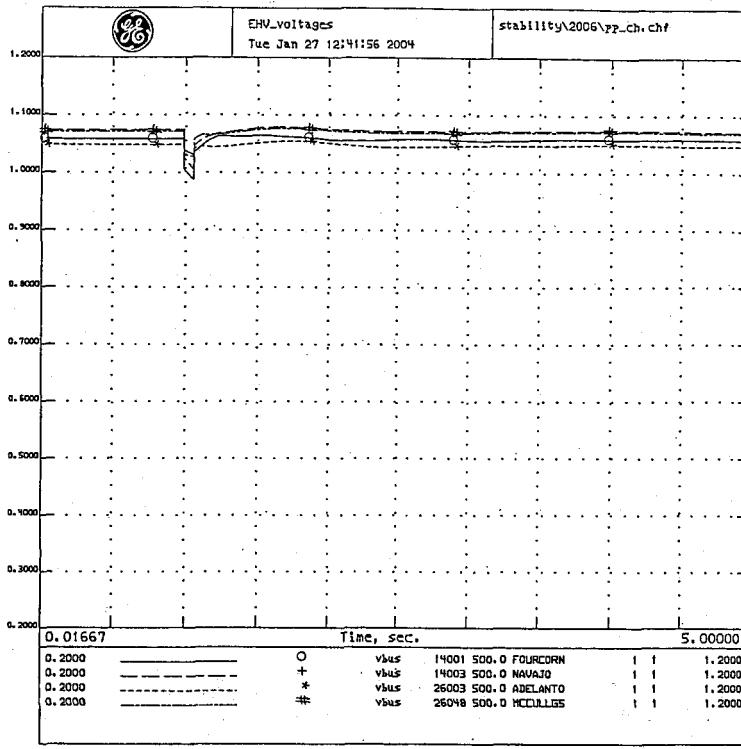
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MOST RECENT VERSION OF THE MDF USED.

B22



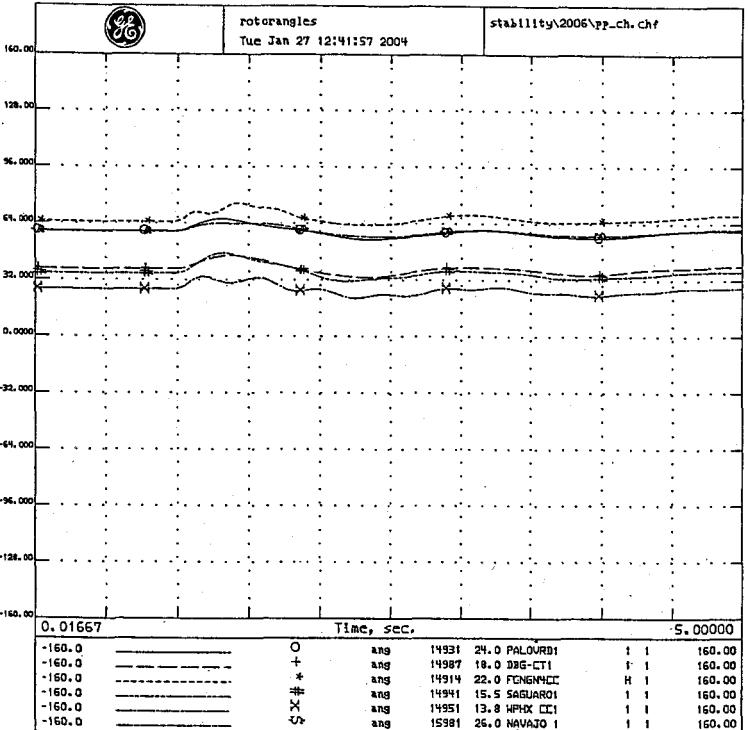
PNPK 345KV FLT PP-CH LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PP-CH STAB #1 01/03; T=0 3P FLT PP345;  
4C CLR FLT W/PP-CH|2006.dyd;WSCC,bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



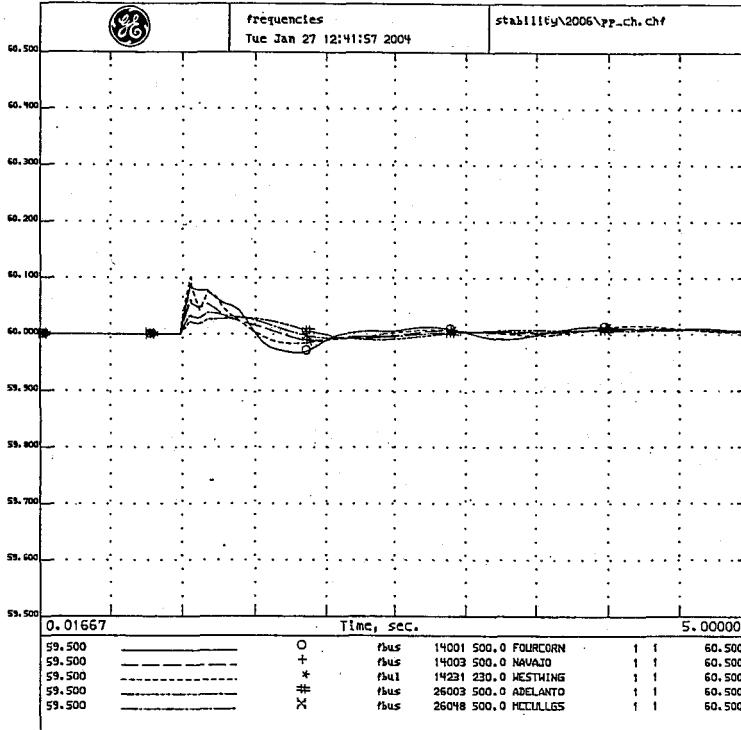
PNPK 345KV FLT PP-CH LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PP-CH STAB #1 01/03; T=0 3P FLT PP345;  
4C CLR FLT W/PP-CH|2006.dyd;WSCC,bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



345KV FLT PP-CH LINE OUT  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PP-CH STAB #1 01/03; T=0 3P FLT PP345;  
4C CLR FLT W/PP-CH|2006.dyd;WSCC,bpt

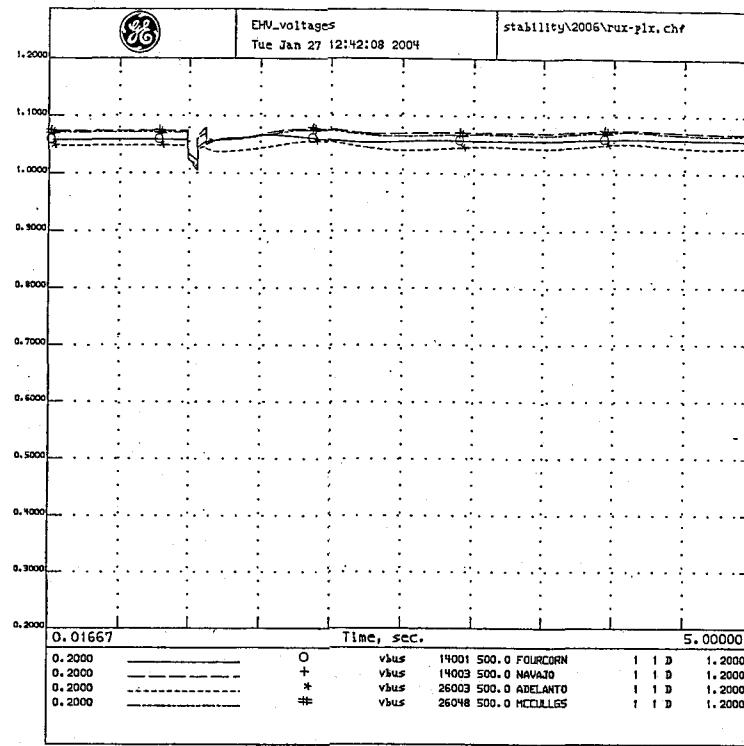
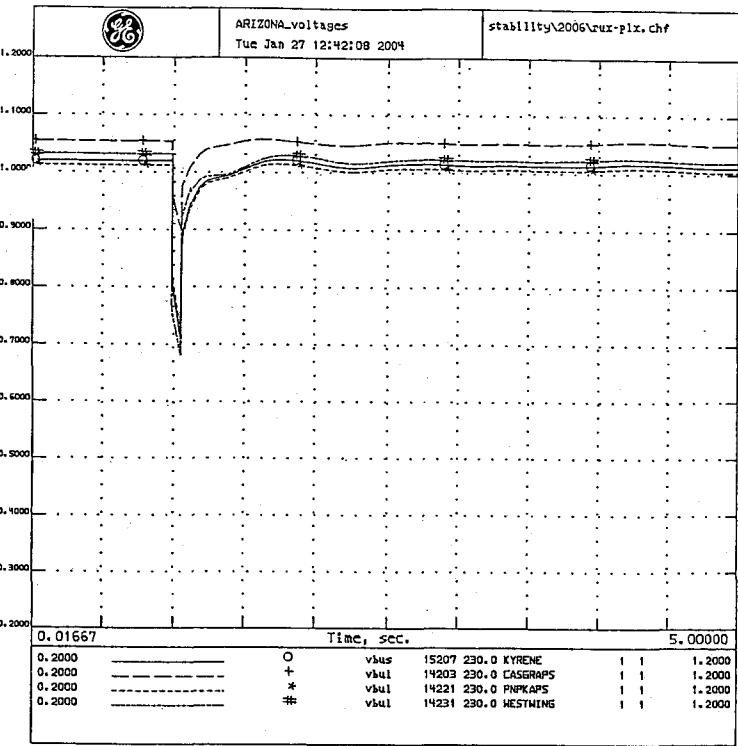
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



PNPK 345KV FLT PP-CH LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PP-CH STAB #1 01/03; T=0 3P FLT PP345;  
4C CLR FLT W/PP-CH|2006.dyd;WSCC,bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B23

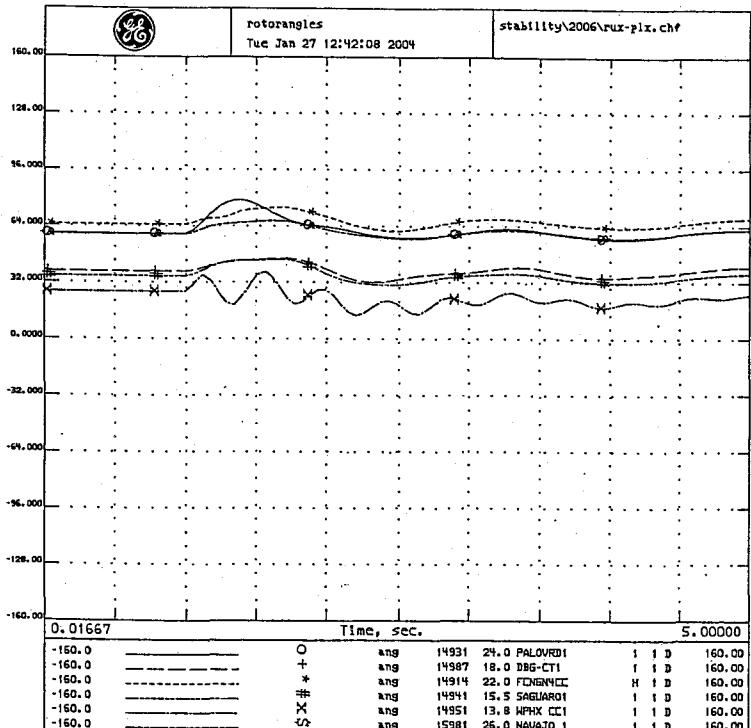


RUDD FLT RUDD-PV LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT RUDD500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-RUDD;BC REIN;2006.4y41MSEC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

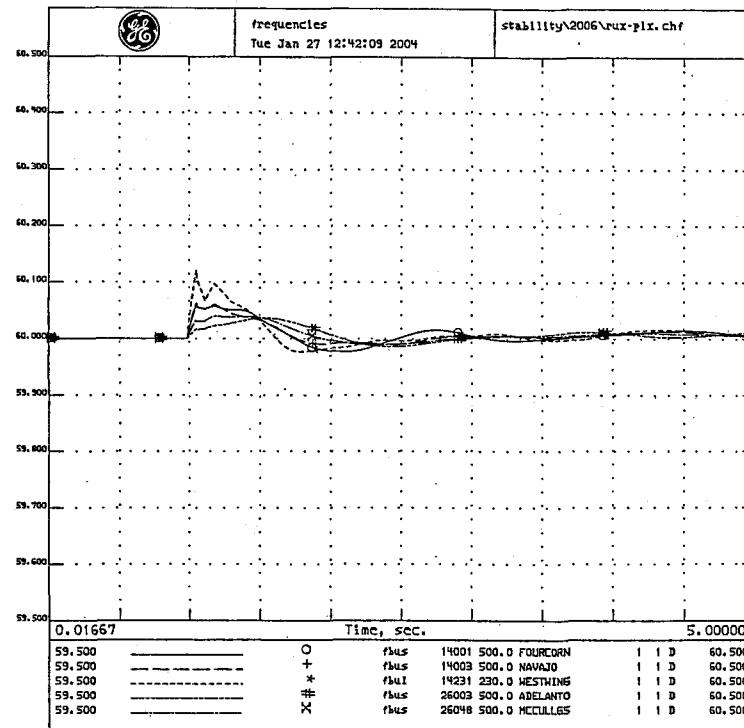
RUDD FLT RUDD-PV LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT RUDD500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-RUDD;BC REIN;2006.4y41MSEC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



RUDD FLT RUDD-PV LINE OUT  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT RUDD500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-RUDD;BC REIN;2006.4y41MSEC.bpt

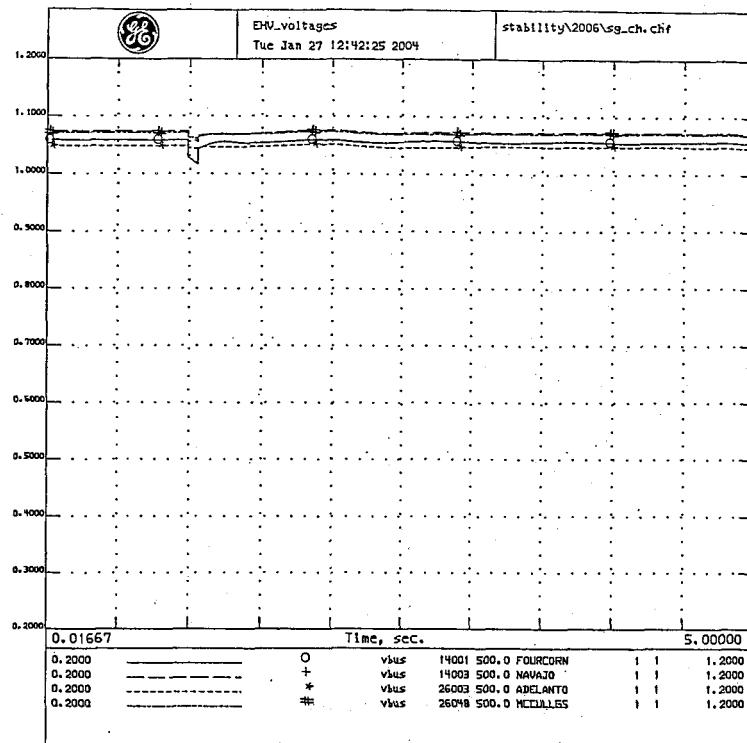
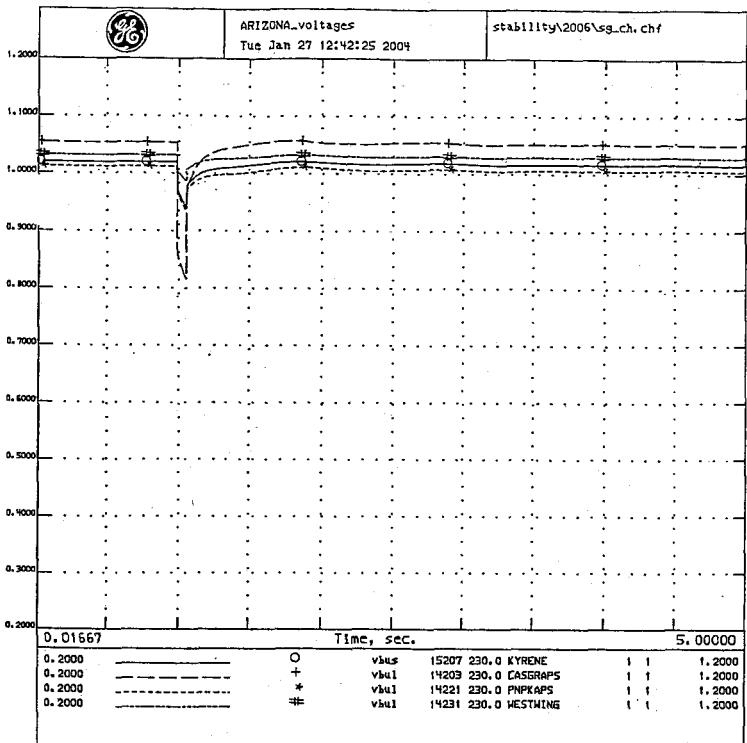
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



RUDD FLT RUDD-PV LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT RUDD500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-RUDD;BC REIN;2006.4y41MSEC.bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B24

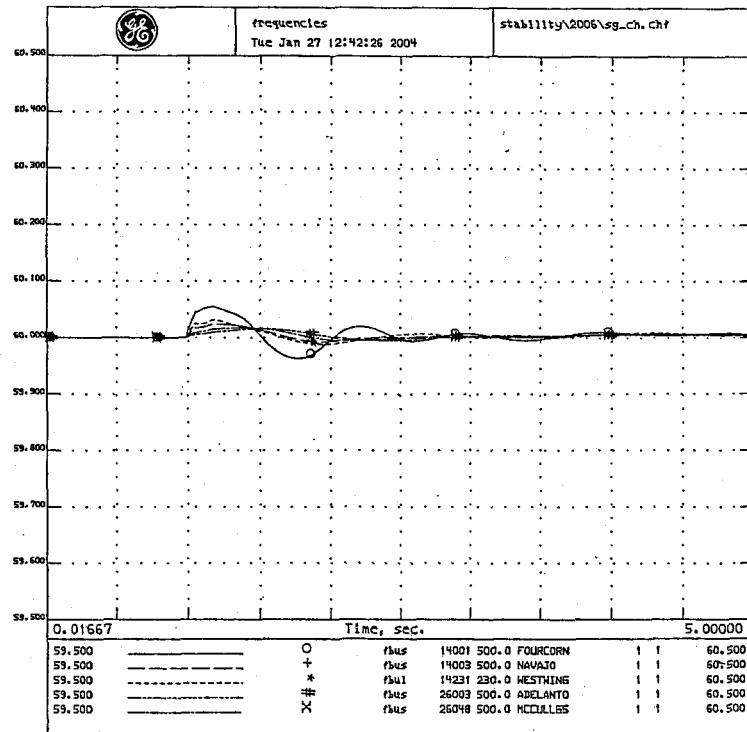
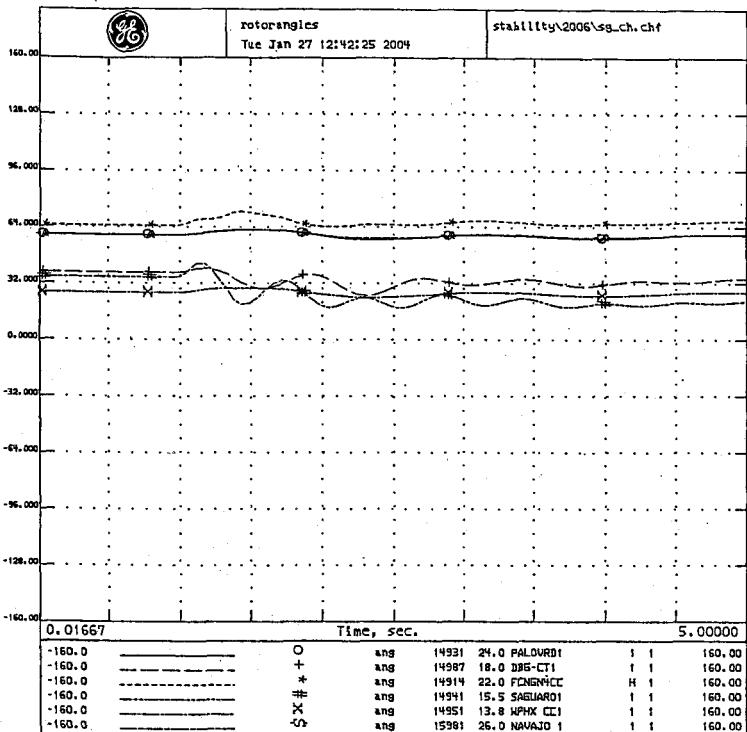


SABUARO FLT SAG-CH LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
SAG-CH STAB #1 01/03; T=0 3P FLT SAG500;  
4C CLR FLT W/SAG-CH|2006, dy4|HSCE, bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

SABUARO FLT SAG-CH LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
SAG-CH STAB #1 01/03; T=0 3P FLT SAG500;  
4C CLR FLT W/SAG-CH|2006, dy4|HSCE, bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



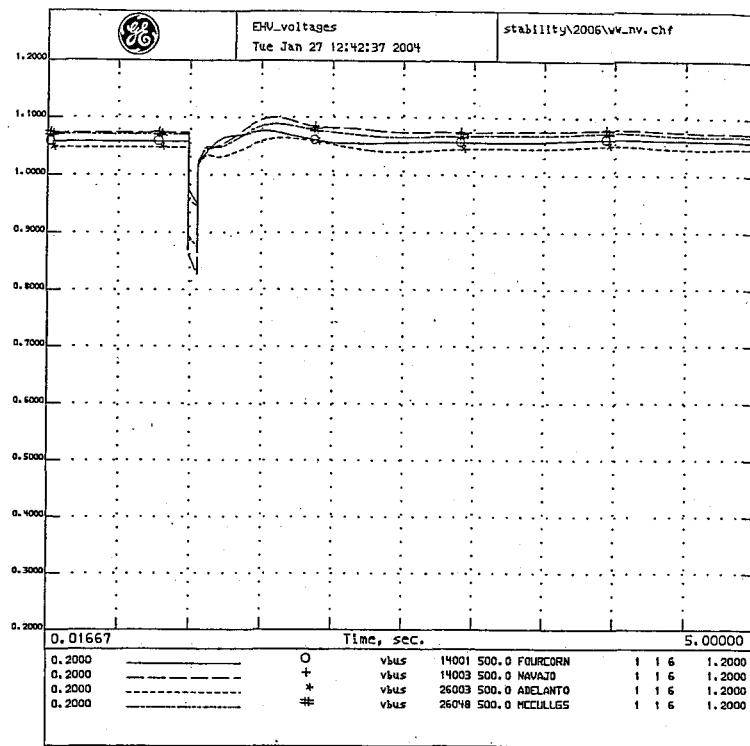
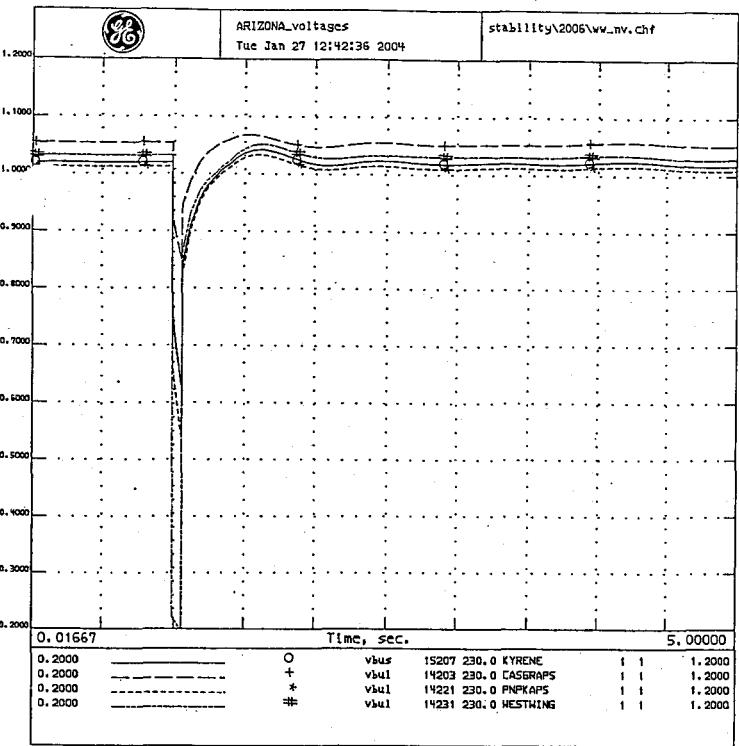
1400 FLT SAG-CH LINE OUT  
HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
SAG-CH STAB #1 01/03; T=0 3P FLT SAG500;  
4C CLR FLT W/SAG-CH|2006, dy4|HSCE, bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

SABUARO FLT SAG-CH LINE OUT  
2006 HS3-SA APPROVED BASE CASE  
OCTOBER 28, 2003  
SAG-CH STAB #1 01/03; T=0 3P FLT SAG500;  
4C CLR FLT W/SAG-CH|2006, dy4|HSCE, bpt

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B25

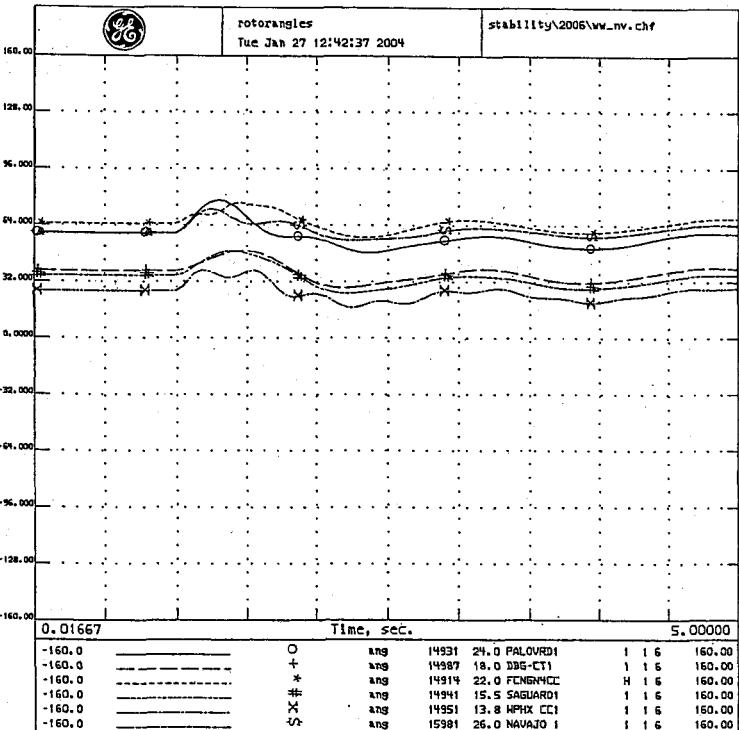


WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW-Nav line out  
OCTOBER 28, 2003  
WWG-NAV STAB; 1/03; T=0 3P FLT WWG500;FLSH CAPS MKP-YAU/YAU-WWG,  
NAU-MKP/WWG;4C CLR FLT W/WWG-NAV;8C REIN;2006.4y4 HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

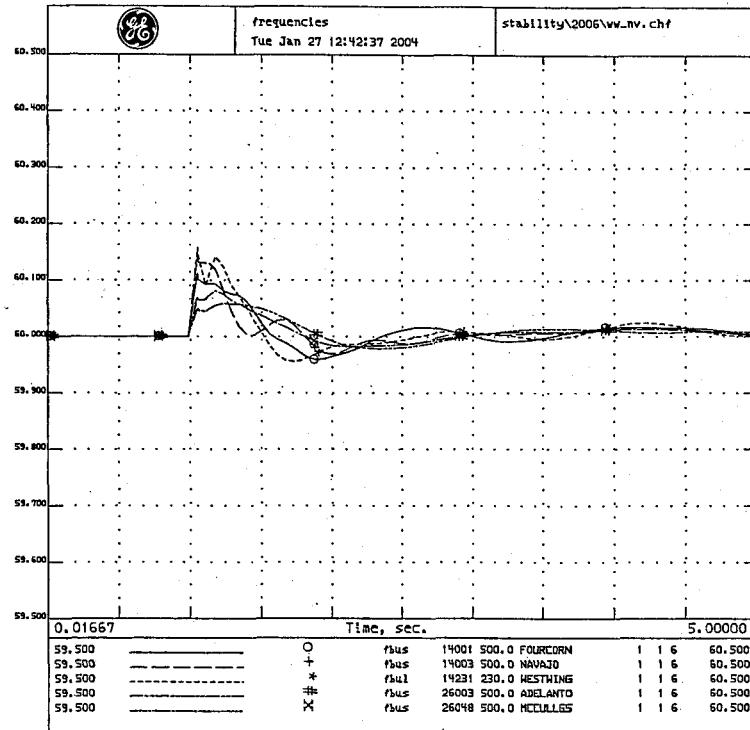
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WW\_FLT\_WW-Nav line out  
OCTOBER 28, 2003  
WWG-NAV STAB; 1/03; T=0 3P FLT WWG500;FLSH CAPS MKP-YAU/YAU-WWG,  
NAU-MKP/WWG;4C CLR FLT W/WWG-NAV;8C REIN;2006.4y4 HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW-Nav line out  
OCTOBER 28, 2003  
WWG-NAV STAB; 1/03; T=0 3P FLT WWG500;FLSH CAPS MKP-YAU/YAU-WWG,  
NAU-MKP/WWG;4C CLR FLT W/WWG-NAV;8C REIN;2006.4y4 HSCC.bat

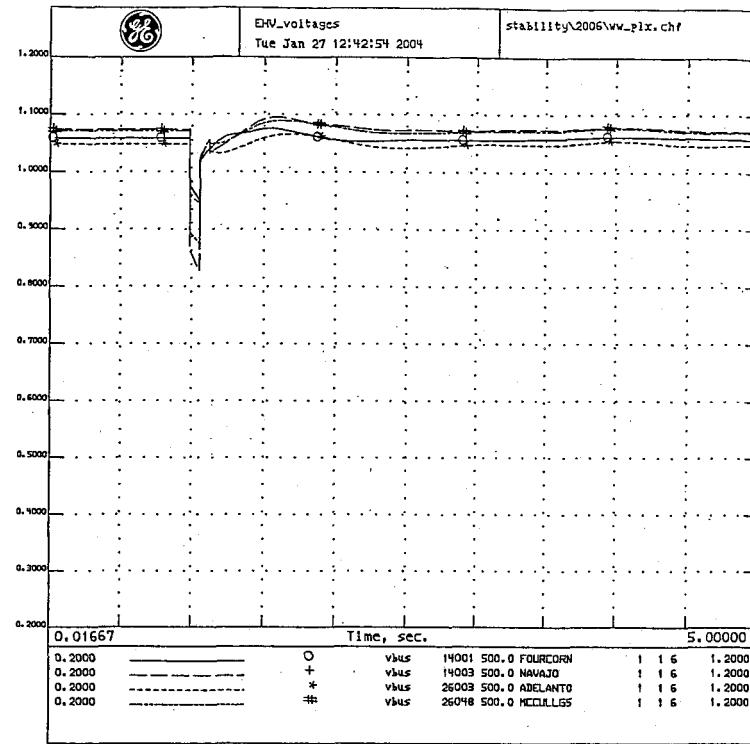
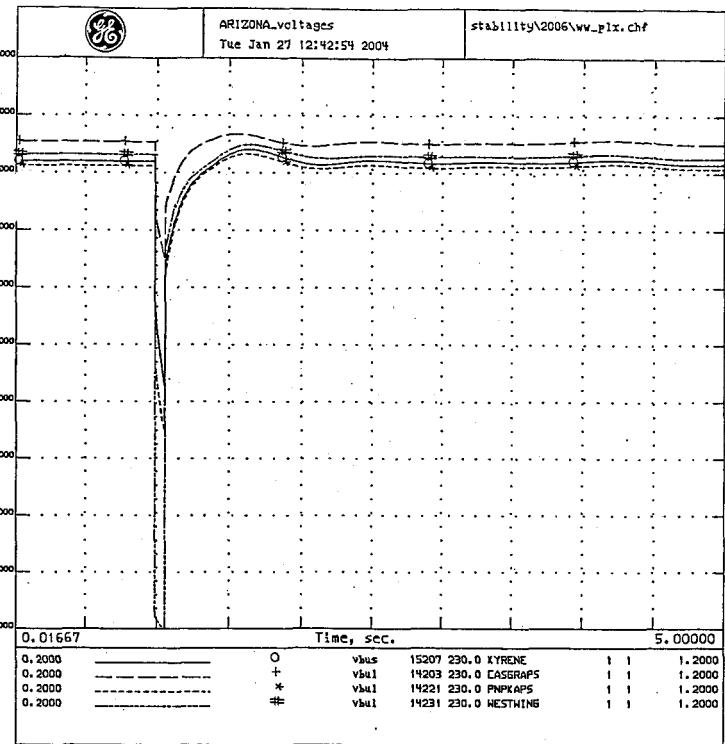
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW-Nav line out  
OCTOBER 28, 2003  
WWG-NAV STAB; 1/03; T=0 3P FLT WWG500;FLSH CAPS MKP-YAU/YAU-WWG,  
NAU-MKP/WWG;4C CLR FLT W/WWG-NAV;8C REIN;2006.4y4 HSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B26

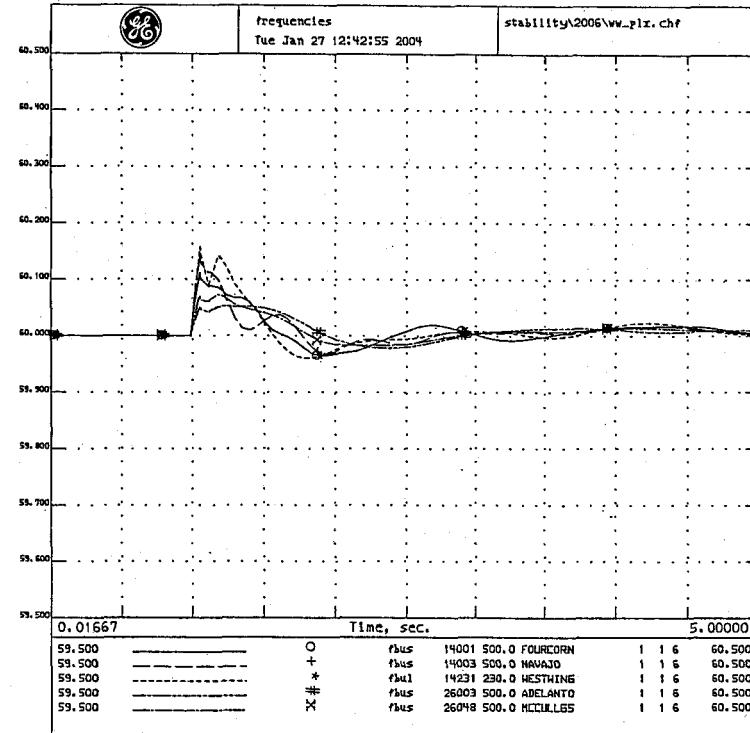
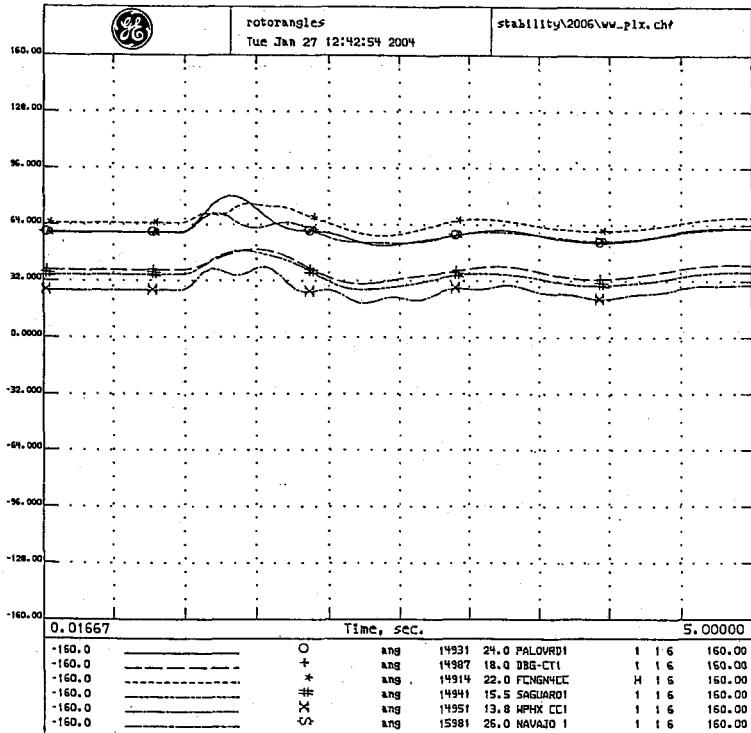


WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW\_PV line out  
OCTOBER 28, 2003  
HNG-YAV STAB; 1/03; T=0 3P FLT HNG500;FLSH CAPS MKP-YAV/YAV-HNG;  
NAV-MKP/HNG;4C CLR FLT W/HNG-PAL;8C REIN;2006..dy4 WSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW\_PV line out  
OCTOBER 28, 2003  
HNG-YAV STAB; 1/03; T=0 3P FLT HNG500;FLSH CAPS MKP-YAV/YAV-HNG;  
NAV-MKP/HNG;4C CLR FLT W/HNG-PAL;8C REIN;2006..dy4 WSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



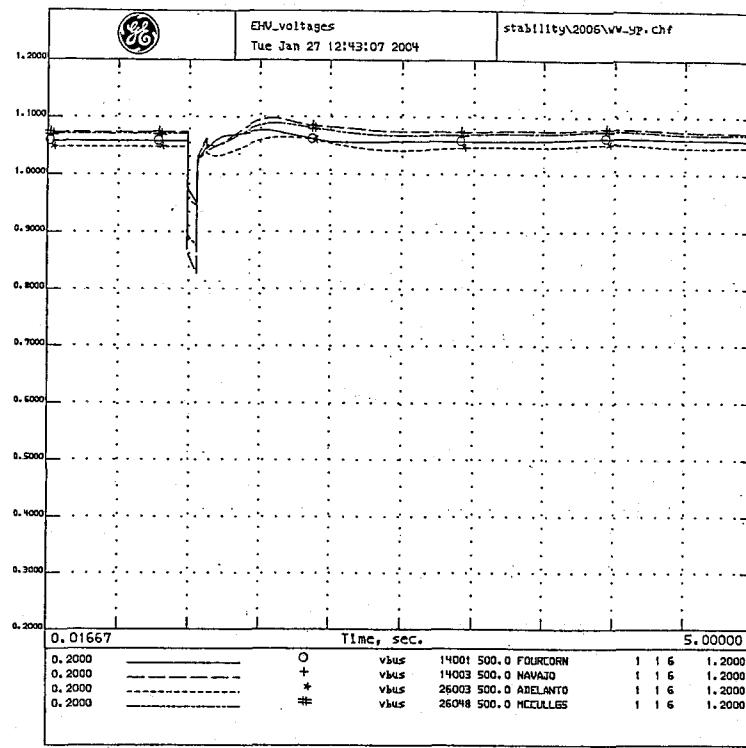
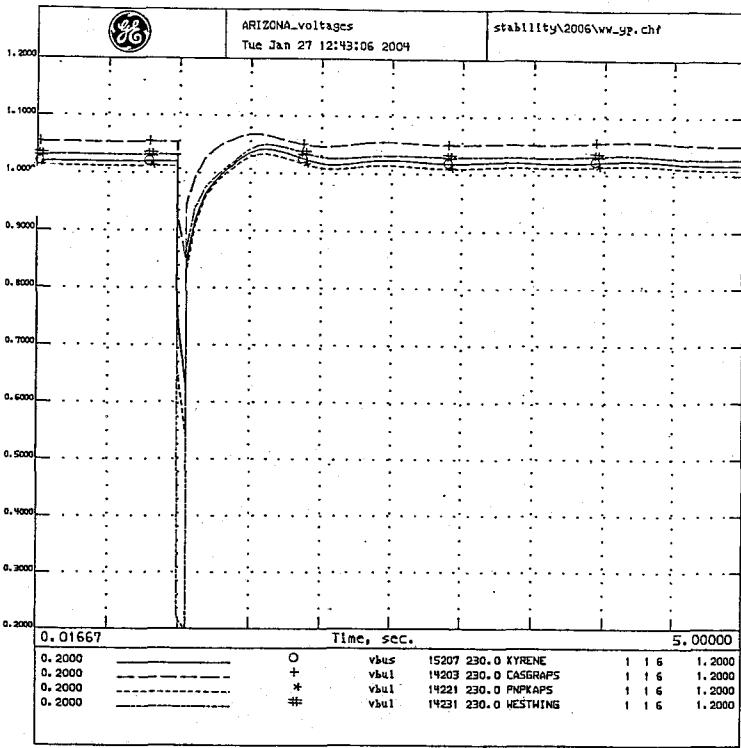
WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW\_PV line out  
OCTOBER 28, 2003  
HNG-YAV STAB; 1/03; T=0 3P FLT HNG500;FLSH CAPS MKP-YAV/YAV-HNG;  
NAV-MKP/HNG;4C CLR FLT W/HNG-PAL;8C REIN;2006..dy4 WSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW\_PV line out  
OCTOBER 28, 2003  
HNG-YAV STAB; 1/03; T=0 3P FLT HNG500;FLSH CAPS MKP-YAV/YAV-HNG;  
NAV-MKP/HNG;4C CLR FLT W/HNG-PAL;8C REIN;2006..dy4 WSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

B27

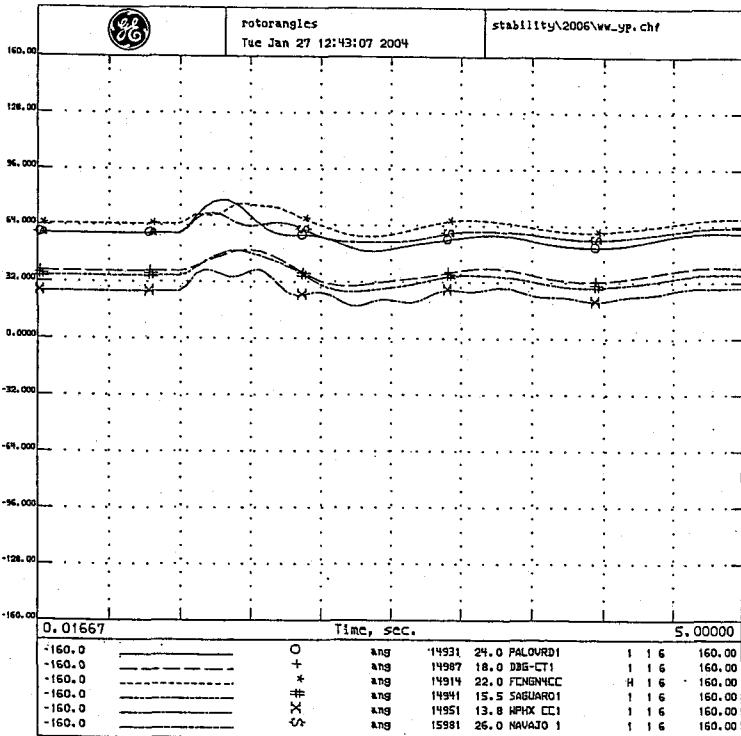


WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW-YAV line out  
OCTOBER 28, 2003  
WWG-YAV STAB1 1/03; T=0 3P FLT WWG500;FLSH CAPS MKP-YAV/YAV-WHG,  
NAU-MKP/WHG;4C CLR FLT W/HWG-YAV;8C REIN;2006,4y4 WSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

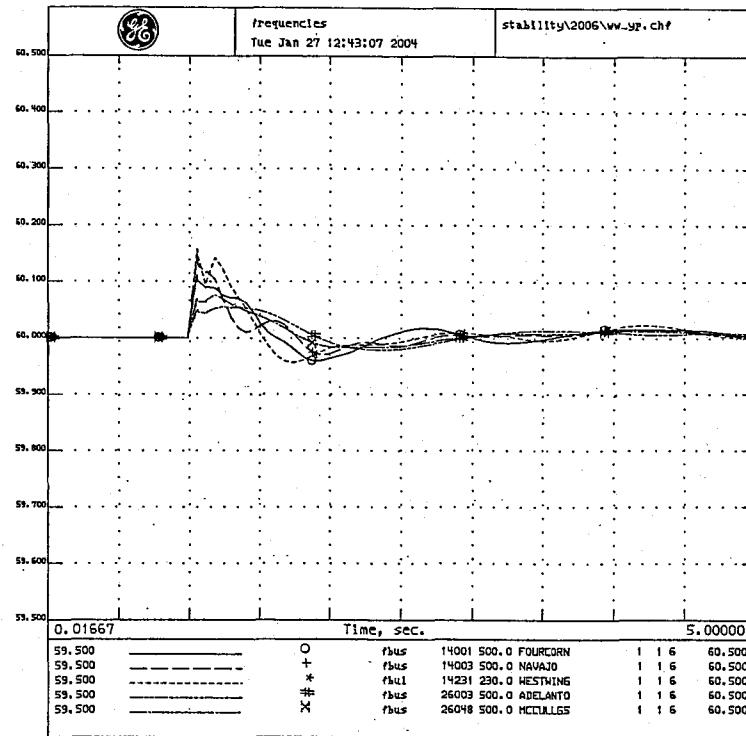
WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW-YAV line out  
OCTOBER 28, 2003  
WWG-YAV STAB1 1/03; T=0 3P FLT WWG500;FLSH CAPS MKP-YAV/YAV-WHG,  
NAU-MKP/WHG;4C CLR FLT W/HWG-YAV;8C REIN;2006,4y4 WSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW-YAV line out  
OCTOBER 28, 2003  
WWG-YAV STAB1 1/03; T=0 3P FLT WWG500;FLSH CAPS MKP-YAV/YAV-WHG,  
NAU-MKP/WHG;4C CLR FLT W/HWG-YAV;8C REIN;2006,4y4 WSCC.bat

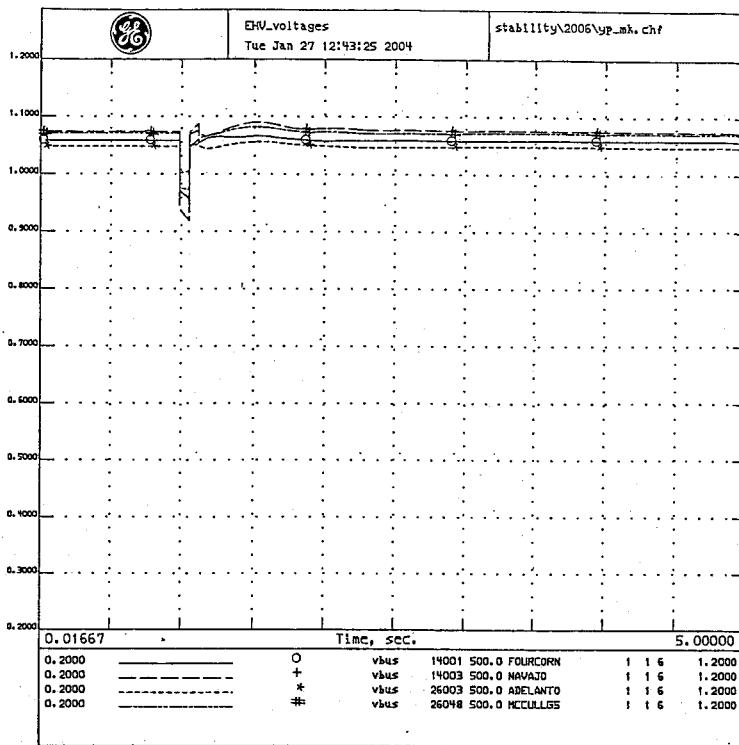
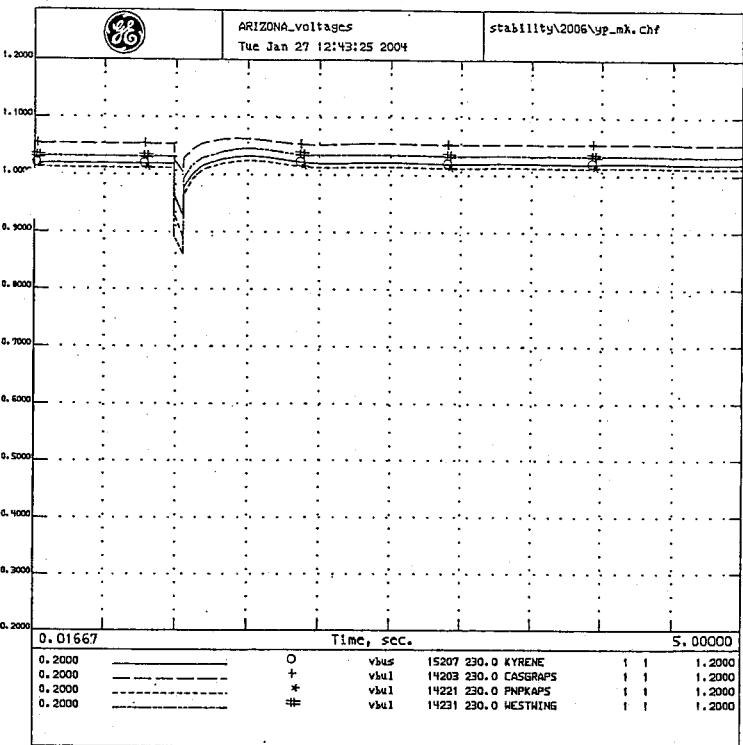
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WW\_FLT\_WW-YAV line out  
OCTOBER 28, 2003  
WWG-YAV STAB1 1/03; T=0 3P FLT WWG500;FLSH CAPS MKP-YAV/YAV-WHG,  
NAU-MKP/WHG;4C CLR FLT W/HWG-YAV;8C REIN;2006,4y4 WSCC.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
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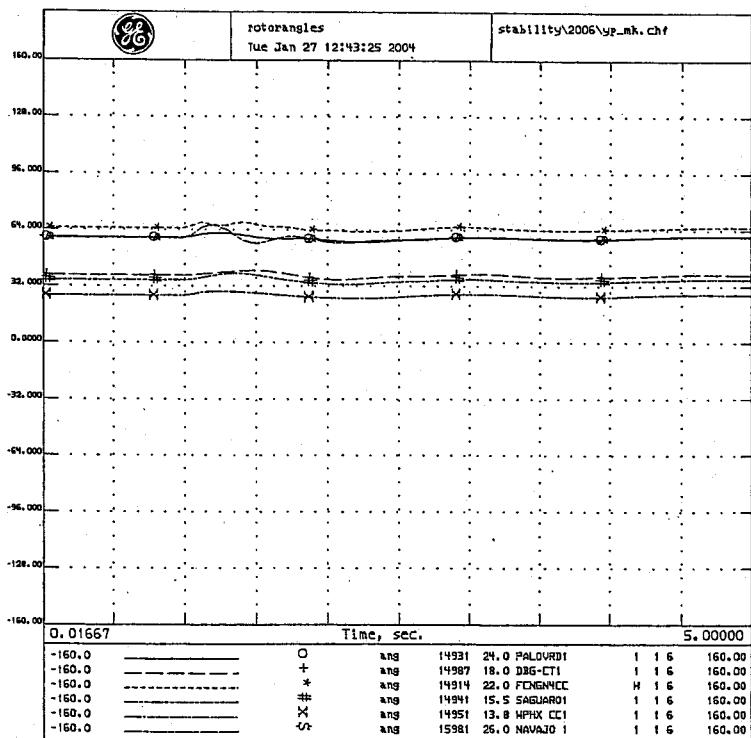


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YAV\_FLT\_Yav-Moen line out  
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YAV\_STAB; 1/03; T=0 3P FLT W/HG500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MKP/HNG;4C CLR FLT W/YAV-MNK;8C REIN;2006.d4c HSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

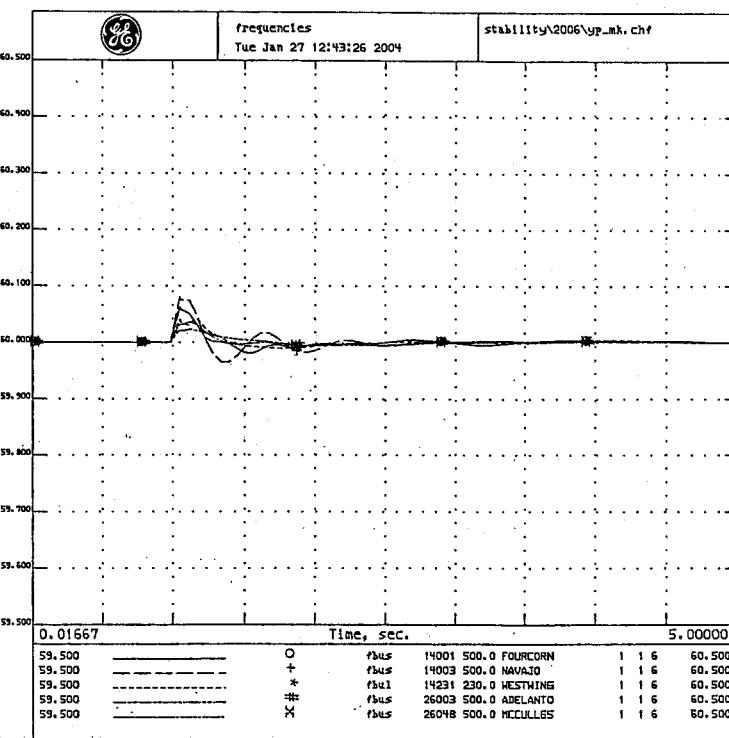
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YAV\_FLT\_Yav-Moen line out  
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NAV-MKP/HNG;4C CLR FLT W/YAV-MNK;8C REIN;2006.d4c HSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
YAV\_FLT\_Yav-Moen line out  
OCTOBER 28, 2003  
YAV\_STAB; 1/03; T=0 3P FLT W/HG500;FLSH CAPS MKP-YAV/YAV-HNG,  
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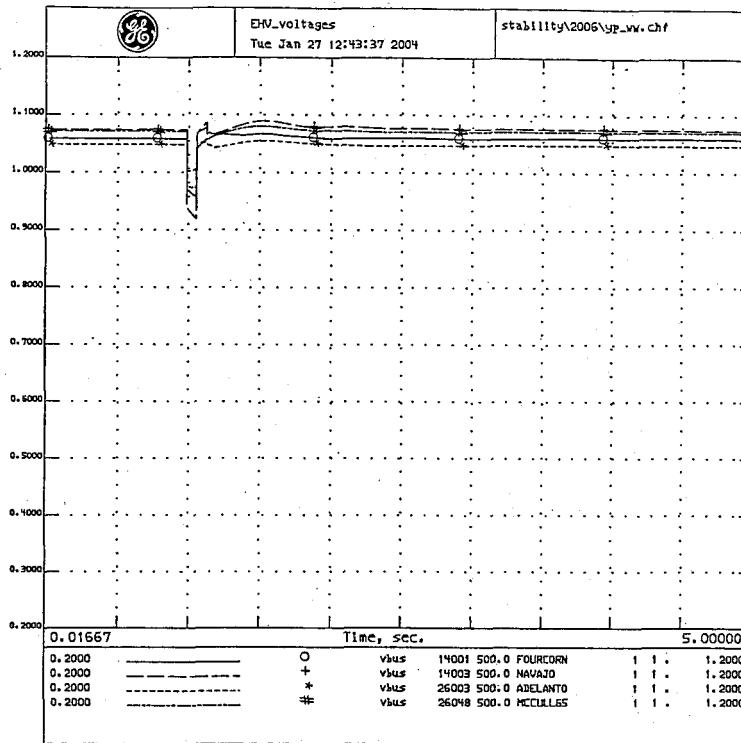
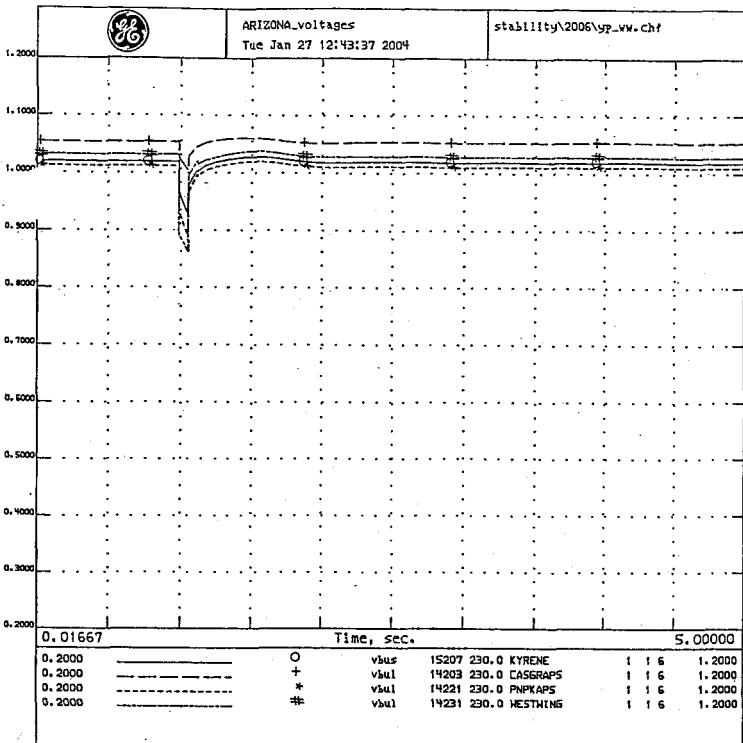
ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.



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OCTOBER 28, 2003  
YAV\_STAB; 1/03; T=0 3P FLT W/HG500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MKP/HNG;4C CLR FLT W/YAV-MNK;8C REIN;2006.d4c HSCE.bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
HOST RECENT VERSION OF THE MDF USED.

B29

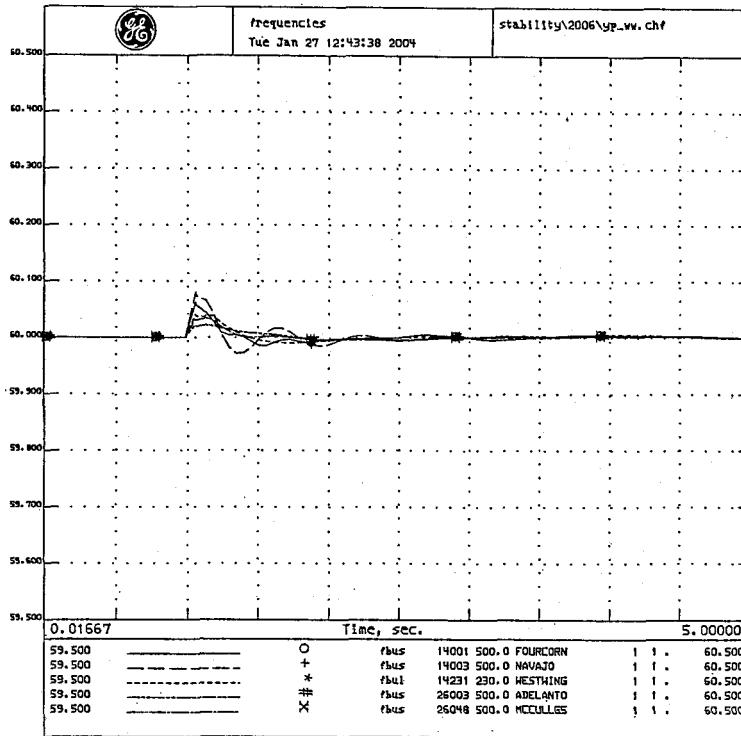
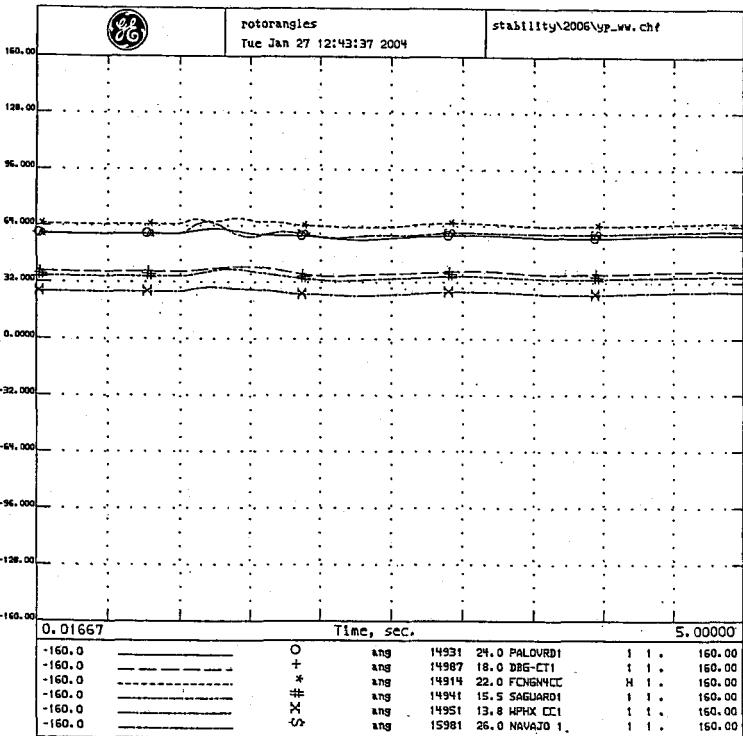


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OCTOBER 28, 2003  
YAV STAB1 1/03; T=0 3P FLT WHE500;FLSH CAPS MKP-YAV/YAV-WHG,  
NAV-MKP/WHG;HC CLR FLT W/YAV-WH;BC REIN;2006, dyd HSCC, bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

WESTERN ELECTRICITY COORDINATING COUNCIL  
YAV, FLT, Yav-WW line out  
OCTOBER 28, 2003  
YAV STAB1 1/03; T=0 3P FLT WHE500;FLSH CAPS MKP-YAV/YAV-WHG,  
NAV-MKP/WHG;HC CLR FLT W/YAV-WH;BC REIN;2006, dyd HSCC, bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.



WESTERN ELECTRICITY COORDINATING COUNCIL  
YAV, FLT, Yav-WW line out  
OCTOBER 28, 2003  
YAV STAB1 1/03; T=0 3P FLT WHE500;FLSH CAPS MKP-YAV/YAV-WHG,  
NAV-MKP/WHG;HC CLR FLT W/YAV-WH;BC REIN;2006, dyd HSCC, bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

WESTERN ELECTRICITY COORDINATING COUNCIL  
YAV, FLT, Yav-WW line out  
OCTOBER 28, 2003  
YAV STAB1 1/03; T=0 3P FLT WHE500;FLSH CAPS MKP-YAV/YAV-WHG,  
NAV-MKP/WHG;HC CLR FLT W/YAV-WH;BC REIN;2006, dyd HSCC, bat

ALL COMMENTS FROM THE TSS REVIEW ARE ADDED.  
MOST RECENT VERSION OF THE MDF USED.

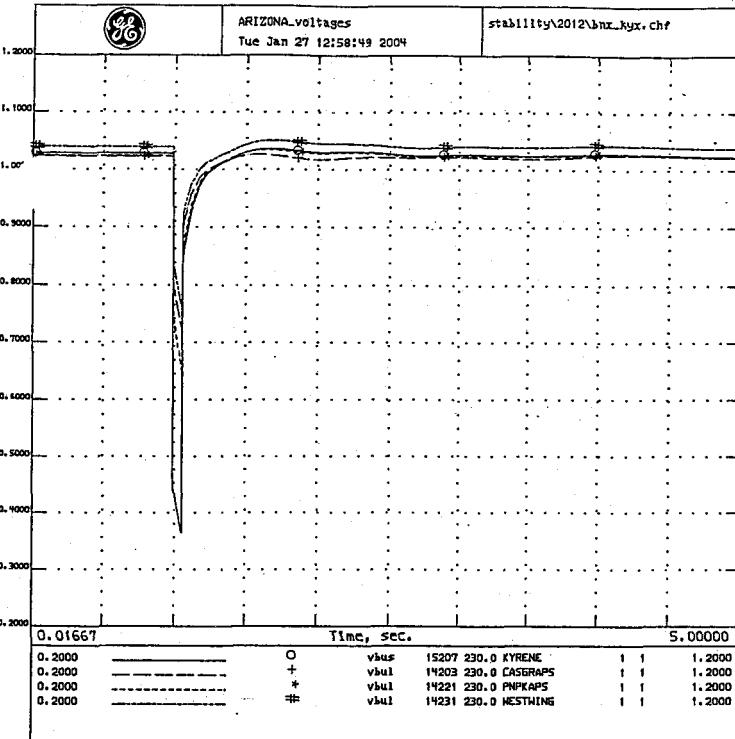
B30

## **APPENDIX C**

### **2012 Stability Plots**

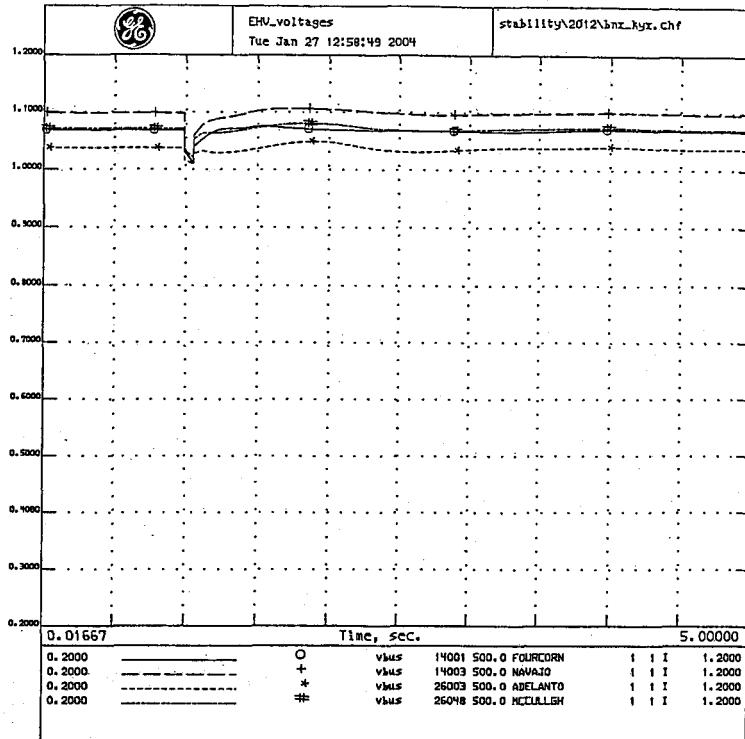
## Table of Contents

<u>Simulation</u>	<u>Page</u>
<b>Browning 500kv</b>	
Browning-Kyrene outage .....	C1
<b>Cholla 500 &amp; 345kv</b>	
Cholla-Coronado outage .....	C2
Cholla-Four Corners outage.....	C3
Cholla-Pinnacle Peak outage .....	C4
Cholla-Saguaro outage.....	C5
<b>Four Corners 500kv</b>	
Four Corners-Moenkopi outage.....	C6
<b>Jojoba 500kv</b>	
Jojoba-Hassayampa outage .....	C7
Jojoba-Kyrene outage .....	C8
<b>Kyrene 500kv</b>	
Kyrene-Jojoba outage .....	C9
<b>Moenkopi 500kv</b>	
Moenkopi-Eldorado outage .....	C10
Moenkopi-Yavapai outage .....	C11
<b>North Gila 500kv</b>	
North Gila-Hassayampa outage .....	C12
North Gila-Imperial Valley outage .....	C13
<b>Navajo 500kv</b>	
Navajo-Crystal outage.....	C14
Navajo-Moenkopi outage .....	C15
Navajo-Raceway outage .....	C16
<b>Perkins 500kv</b>	
Perkins-Mead outage.....	C17
<b>Palo Verde 500kv</b>	
Palo Verde-Devers outage.....	C18
Palo Verde-Jojoba outage .....	C19
Palo Verde-North Gila outage .....	C20
Palo Verde-Rudd outage .....	C21
Palo Verde-Westwing outage.....	C22
<b>Pinnacle Peak 345kv</b>	
Pinnacle Peak-Cholla outage .....	C23
<b>Rudd 500kv</b>	
Rudd-Palo Verde outage .....	C24
<b>Raceway 500kv</b>	
Raceway-Navajo outage .....	C25
<b>Saguaro 500kv</b>	
Saguaro-Cholla outage .....	C26
<b>Westwing 500kv</b>	
Westwing-Palo Verde outage.....	C27
Westwing-Raceway outage .....	C28
Westwing-Yavapai outage .....	C29
<b>Yavapai 500kv</b>	
Yavapai-Moenkopi outage .....	C30
Yavapai-Westwing outage .....	C31



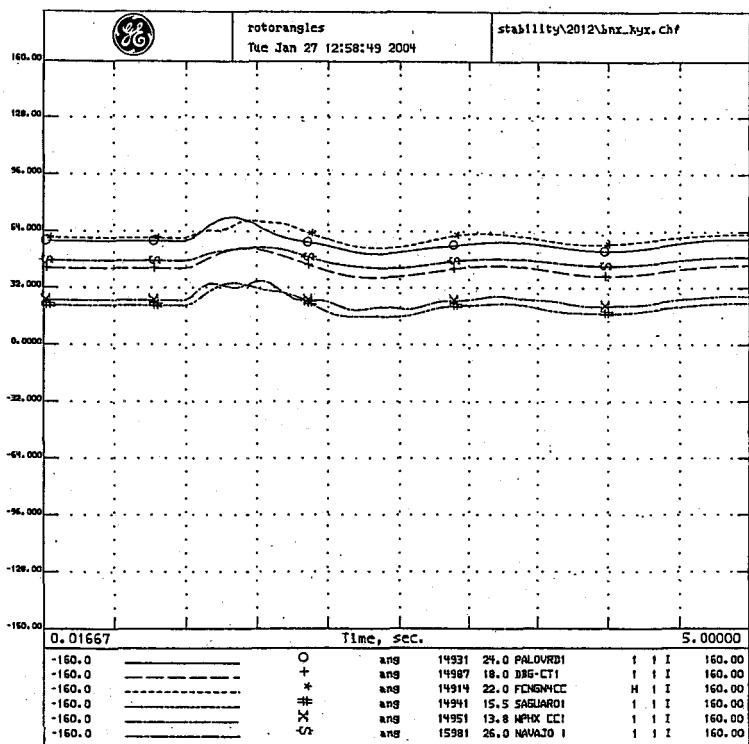
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
BRWN-KYR STAB +1; 01/03; T=0 3P FLT KYRS00;  
4C CLR FLT W/BRWN-KYR/2012.4y4(HSICL.bpt)

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
CONTAINS THE NEW GOVERNOR MODELING RECEIVED IN RESPONSE TO THE  
NOVEMBER 7, 2002 DATA REQUEST.



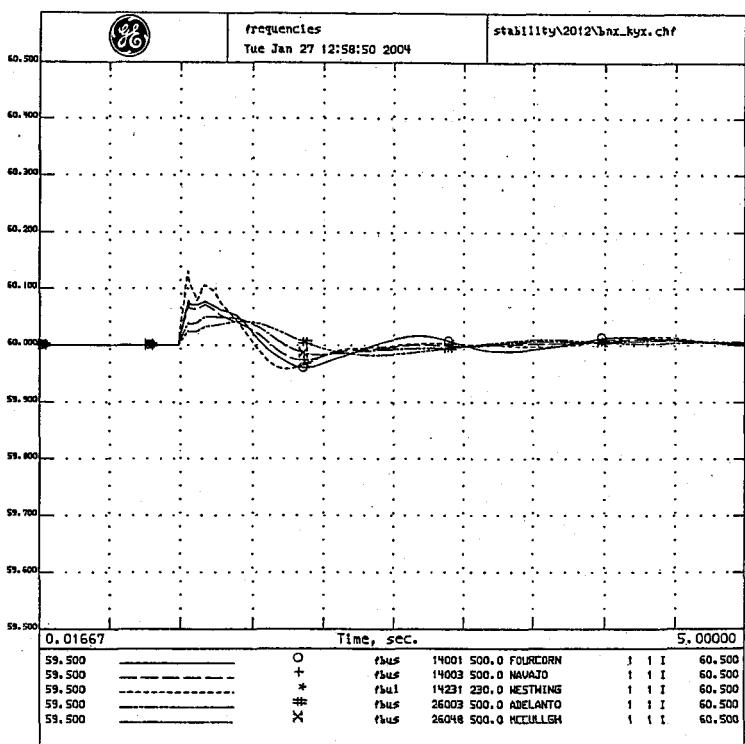
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
BRWN-KYR STAB +1; 01/03; T=0 3P FLT KYRS00;  
4C CLR FLT W/BRWN-KYR/2012.4y4(HSICL.bpt)

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
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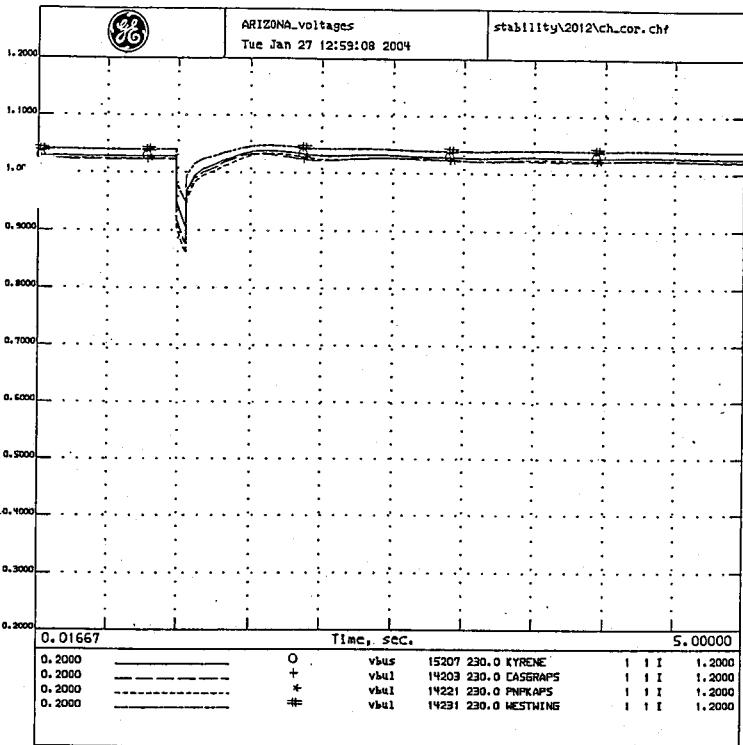
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HSIA APPROVED BASE CASE  
MAY 19, 2003  
BRWN-KYR STAB +1; 01/03; T=0 3P FLT KYRS00;  
4C CLR FLT W/BRWN-KYR/2012.4y4(HSICL.bpt)

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
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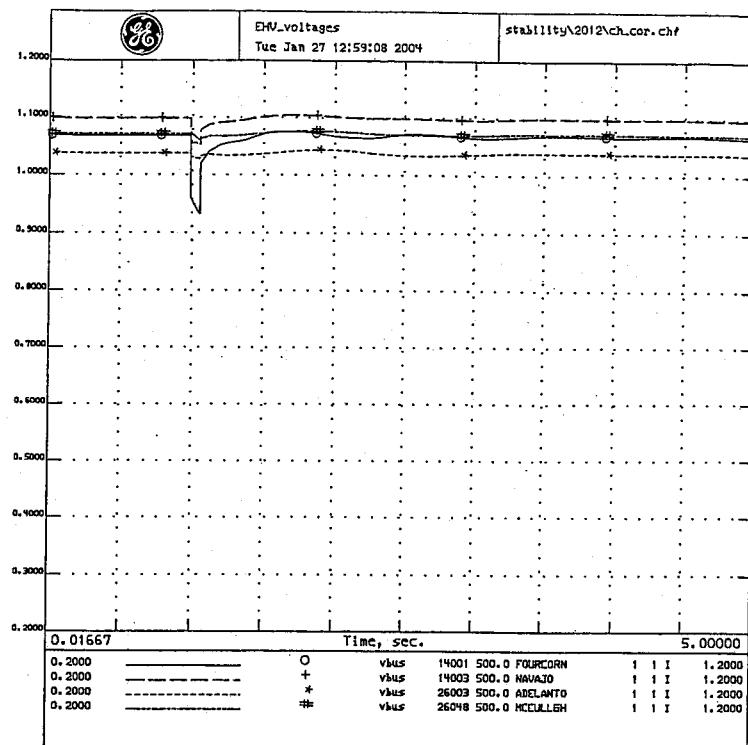
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
BRWN-KYR STAB +1; 01/03; T=0 3P FLT KYRS00;  
4C CLR FLT W/BRWN-KYR/2012.4y4(HSICL.bpt)

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
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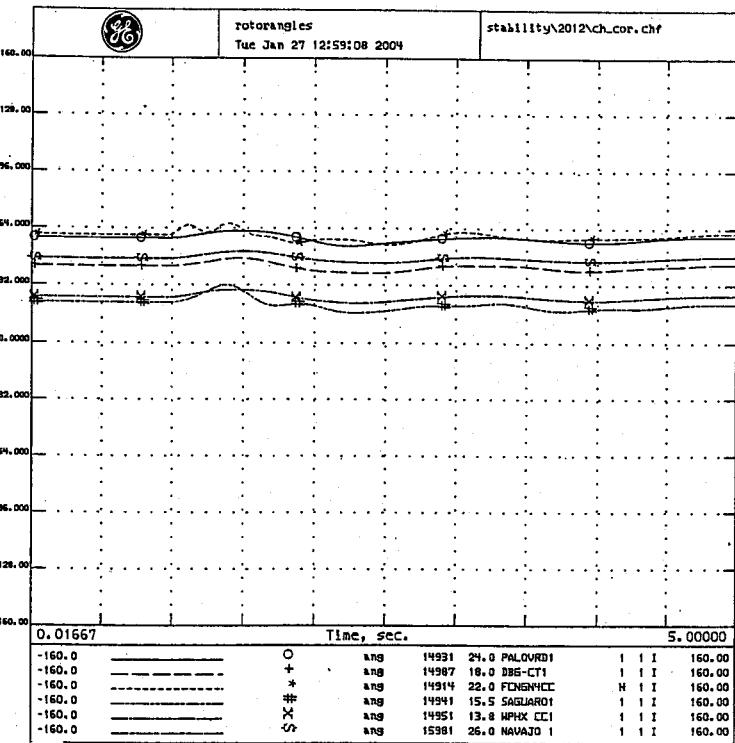
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2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
CHO-COR STAB: 1/03; T=0 3P FLT CH0500;4C CLR FLT  
W/CHO-COR\2012.d4d\HSCC.bpt

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
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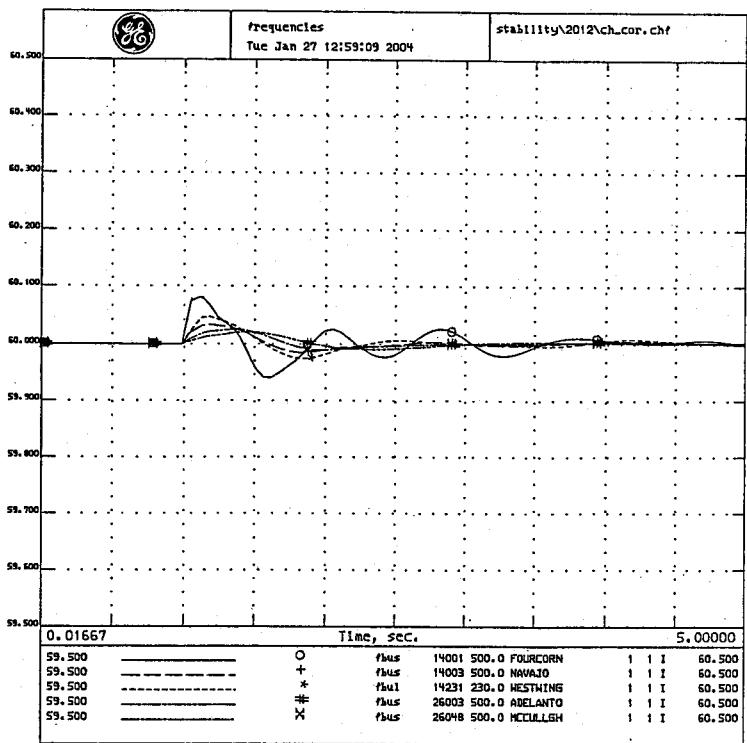
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2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
CHO-COR STAB: 1/03; T=0 3P FLT CH0500;4C CLR FLT  
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ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
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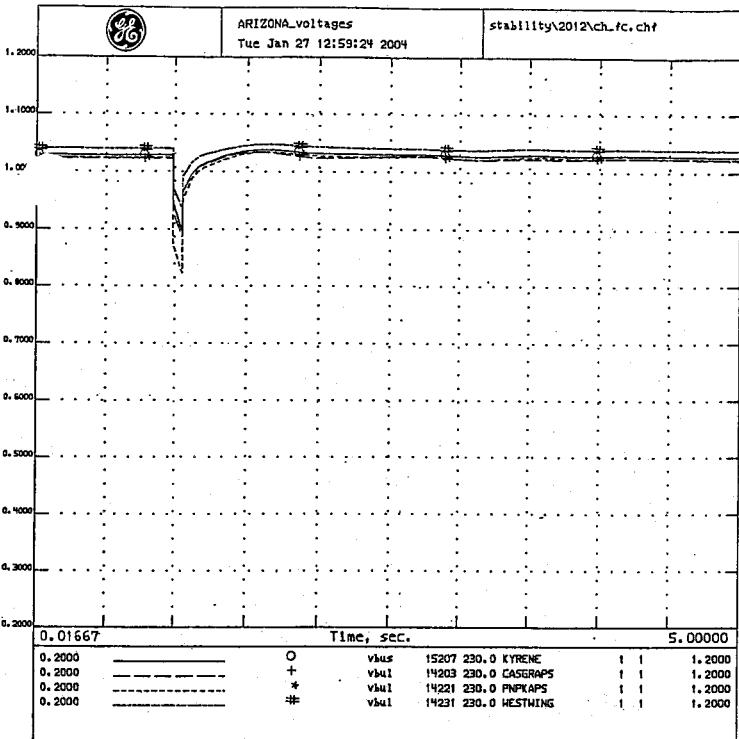
ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
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NOVEMBER 7, 2002 DATA REQUEST.



CHOLLA 500KV FLT CH-COR LINE OUT  
2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
CHO-COR STAB: 1/03; T=0 3P FLT CH0500;4C CLR FLT  
W/CHO-COR\2012.d4d\HSCC.bpt

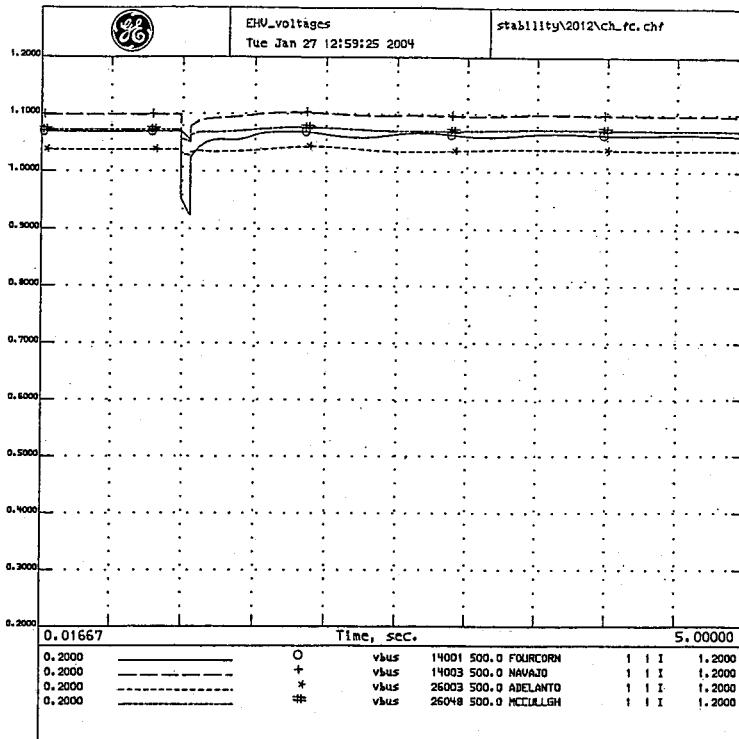
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NOVEMBER 7, 2002 DATA REQUEST.

C2



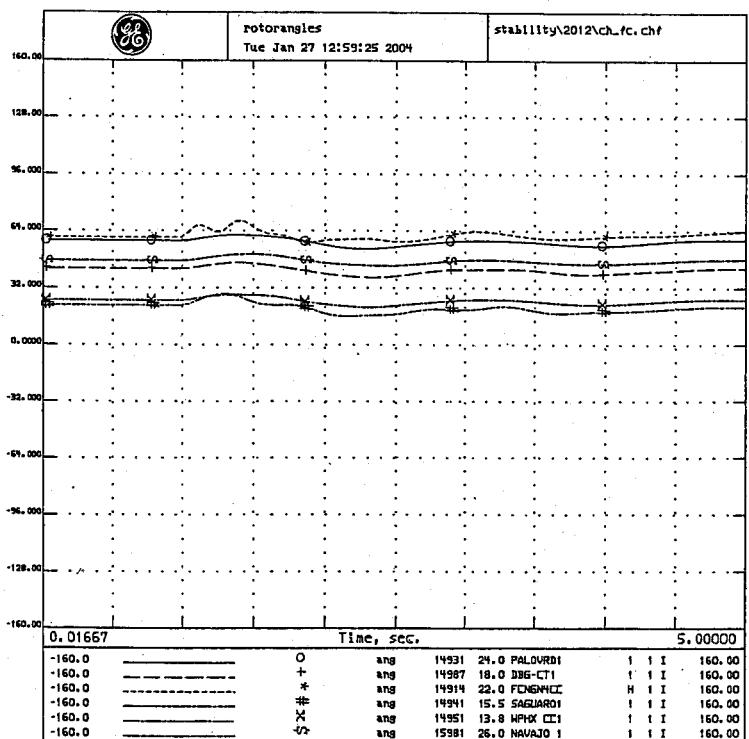
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2012 HSLA APPROVED BASE CASE  
MAY 19, 2003  
CHO-FC #1 STAB; 01/03; T=0 3P FLT CH0345;FLSH FCN-CHO CAPS;  
4C CLR FLT W/CHO-FC #1;2012.4y4;HSCC.bpt

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
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NOVEMBER 7, 2002 DATA REQUEST.



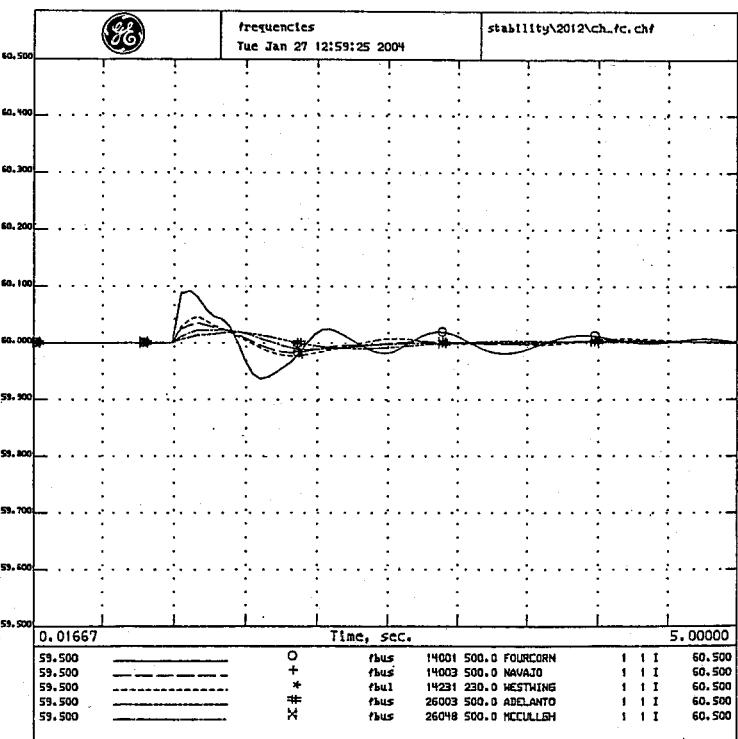
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2012 HSLA APPROVED BASE CASE  
MAY 19, 2003  
CHO-FC #1 STAB; 01/03; T=0 3P FLT CH0345;FLSH FCN-CHO CAPS;  
4C CLR FLT W/CHO-FC #1;2012.4y4;HSCC.bpt

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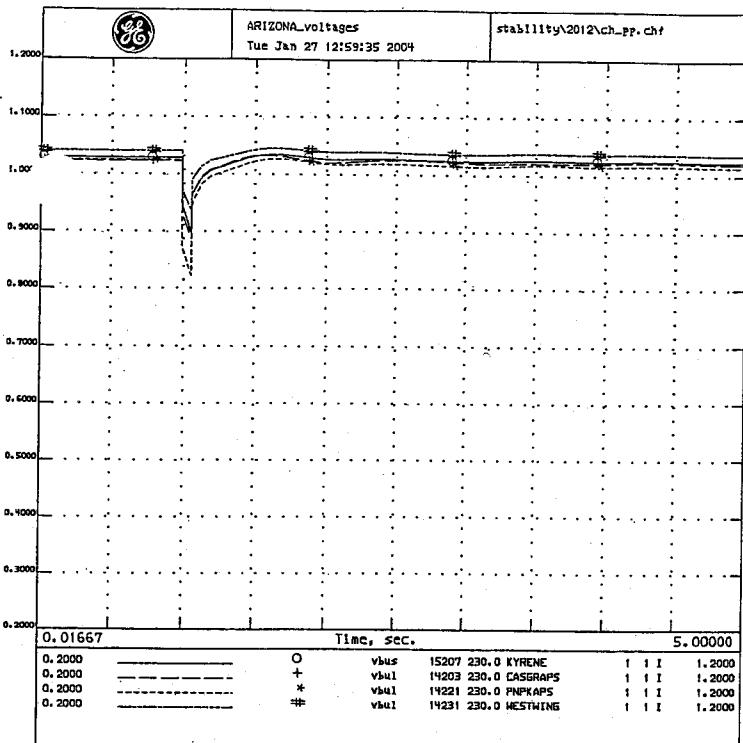
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4 HSLA APPROVED BASE CASE  
MAY 19, 2003  
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4C CLR FLT W/CHO-FC #1;2012.4y4;HSCC.bpt

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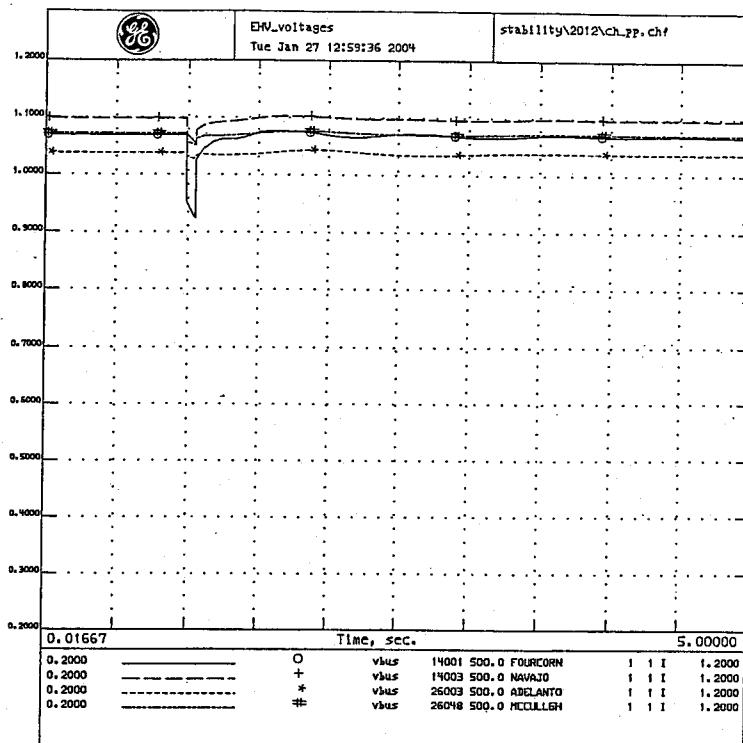
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2012 HSLA APPROVED BASE CASE  
MAY 19, 2003  
CHO-FC #1 STAB; 01/03; T=0 3P FLT CH0345;FLSH FCN-CHO CAPS;  
4C CLR FLT W/CHO-FC #1;2012.4y4;HSCC.bpt

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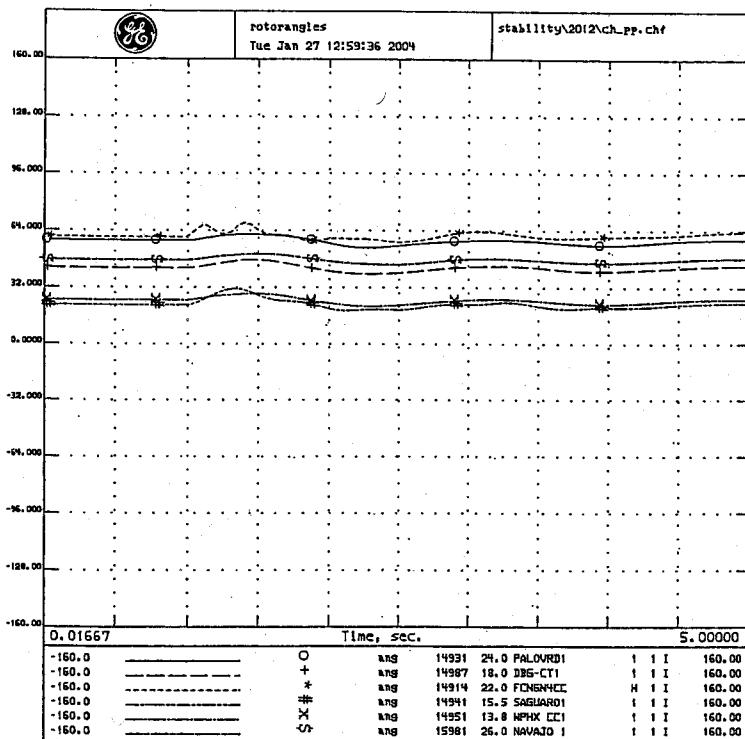
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MAY 19, 2003  
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4C CLR FLT W/CHO-PPK +1;BC REIN CAPS;2012.4y4;NSCC.bpt

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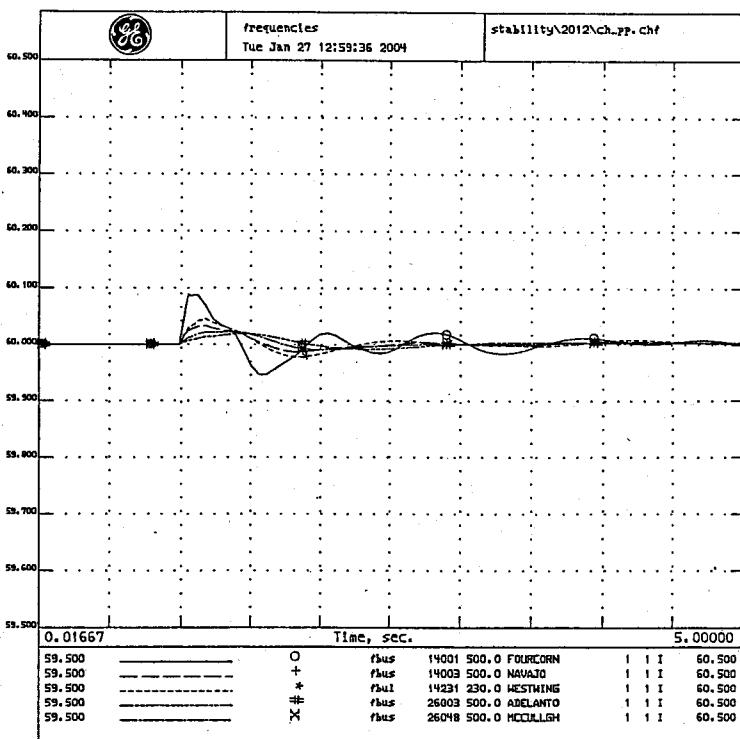
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MAY 19, 2003  
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4C CLR FLT W/CHO-PPK +1;BC REIN CAPS;2012.4y4;NSCC.bpt

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LA FLT CH-PPK LINE OUT!  
2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
CHO-PPK +1 STAB; 01/03; T=0 3P FLT CHO345;FLSH FCN-CHO CAPS;  
4C CLR FLT W/CHO-PPK +1;BC REIN CAPS;2012.4y4;NSCC.bpt

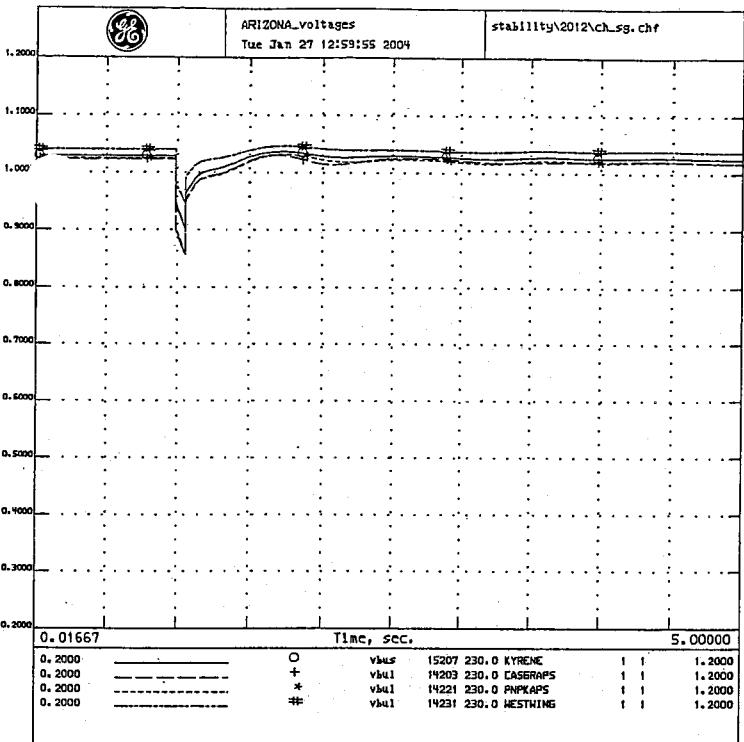
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CHOLLA FLT CH-PPK LINE OUT!  
2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
CHO-PPK +1 STAB; 01/03; T=0 3P FLT CHO345;FLSH FCN-CHO CAPS;  
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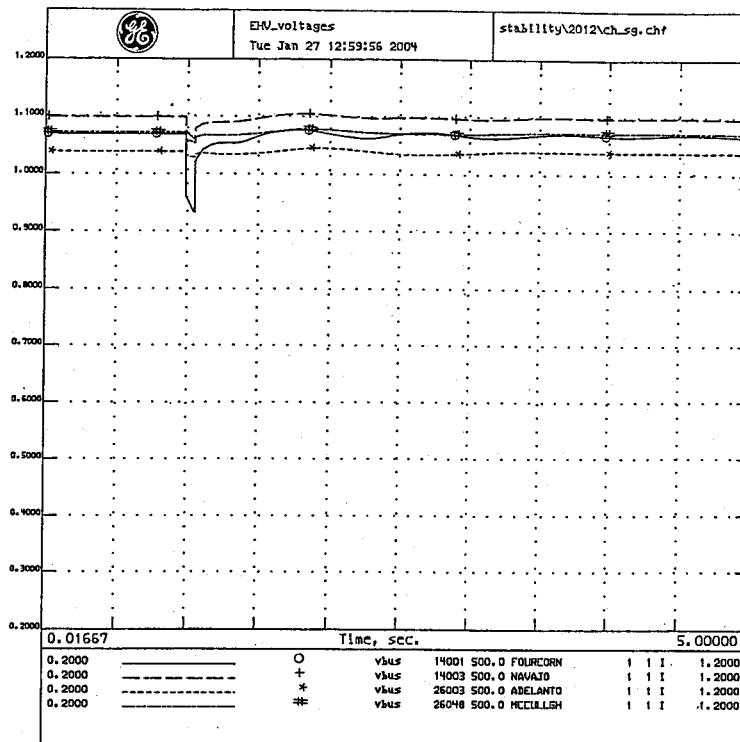
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NOVEMBER 7, 2002 DATA REQUEST.

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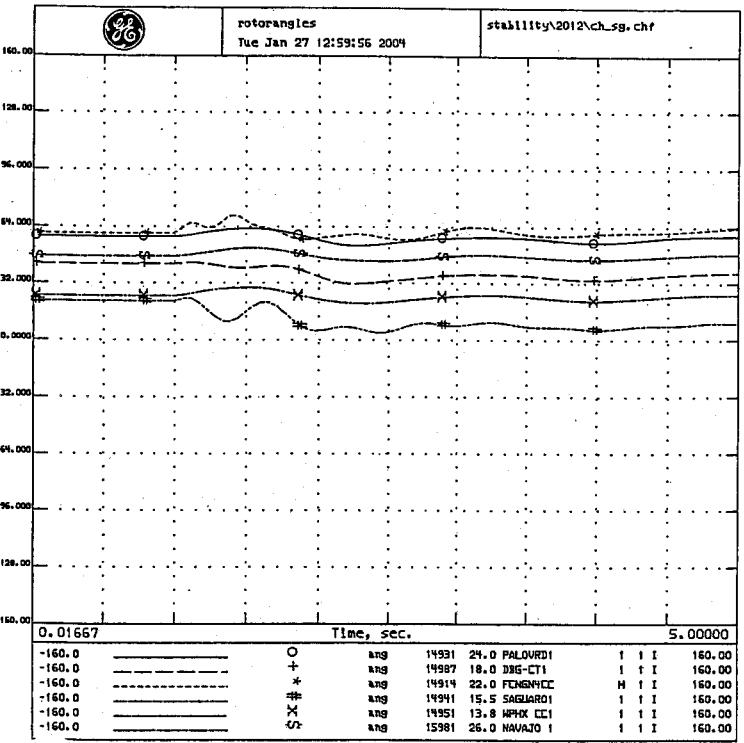
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
CHO-SAG STAB: 1/03; T=0 3P FLT CHO500;4C CLR FLT  
W/CHO-SAG|2012\_d44|NSCC.bpt

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
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NOVEMBER 7, 2002 DATA REQUEST.



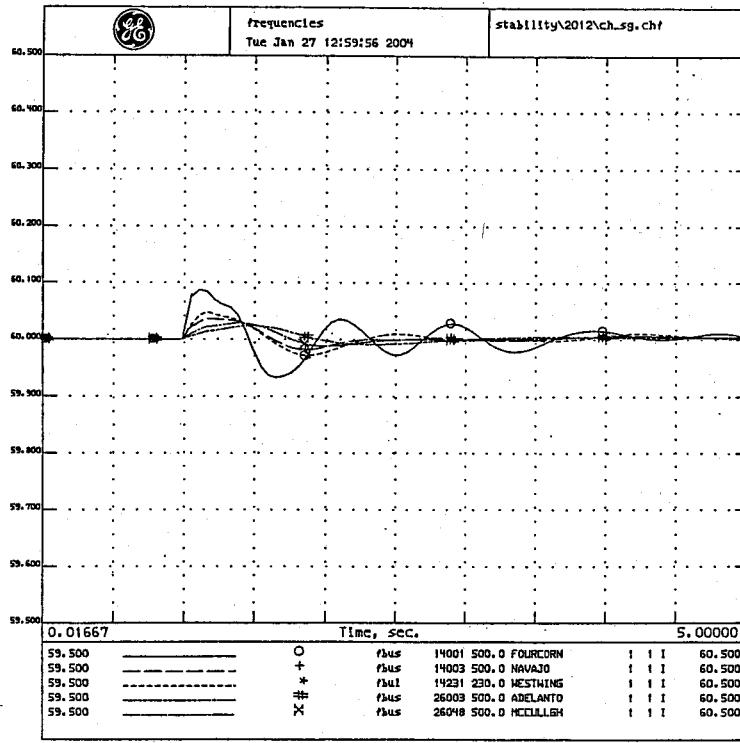
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
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W/CHO-SAG|2012\_d44|NSCC.bpt

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NOVEMBER 7, 2002 DATA REQUEST.



A 500KV FLT CH-SAG LINE OUT  
HSIA APPROVED BASE CASE  
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CHO-SAG STAB: 1/03; T=0 3P FLT CHO500;4C CLR FLT  
W/CHO-SAG|2012\_d44|NSCC.bpt

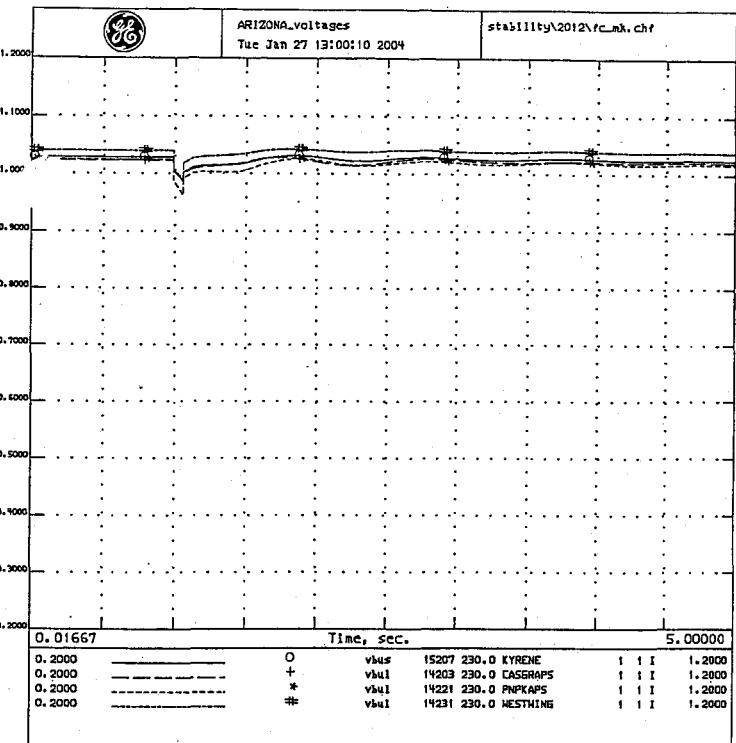
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CHOLLA 500KV FLT CH-SAG LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
CHO-SAG STAB: 1/03; T=0 3P FLT CHO500;4C CLR FLT  
W/CHO-SAG|2012\_d44|NSCC.bpt

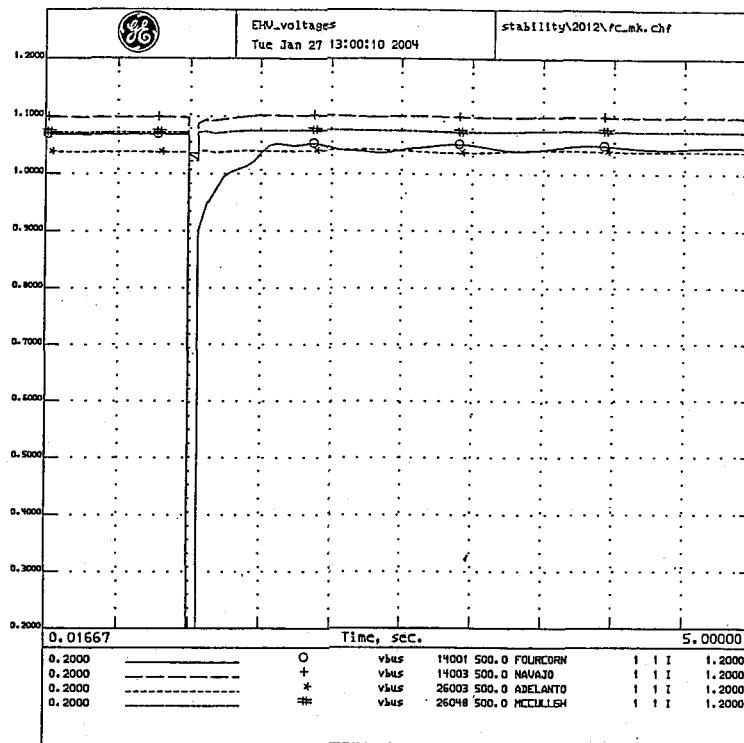
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NOVEMBER 7, 2002 DATA REQUEST.

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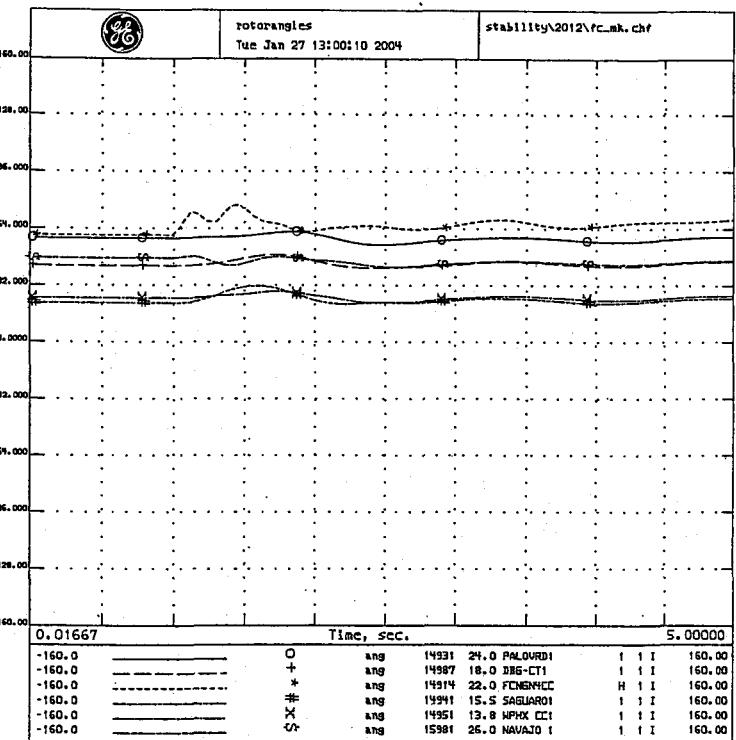
FCN FLT500 FCN-MNK out  
2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
FOURCORN-HOENKOPF STAB; 1/03; T=0 3P FLT FCN500|10X FLT DMPING|FLSH  
CAPS FCN-MKP|NAV-MKP|HC CLR FLT W/FCN-MKP|8C REIN CAPS;2012.4y4\HSCC.bpt

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
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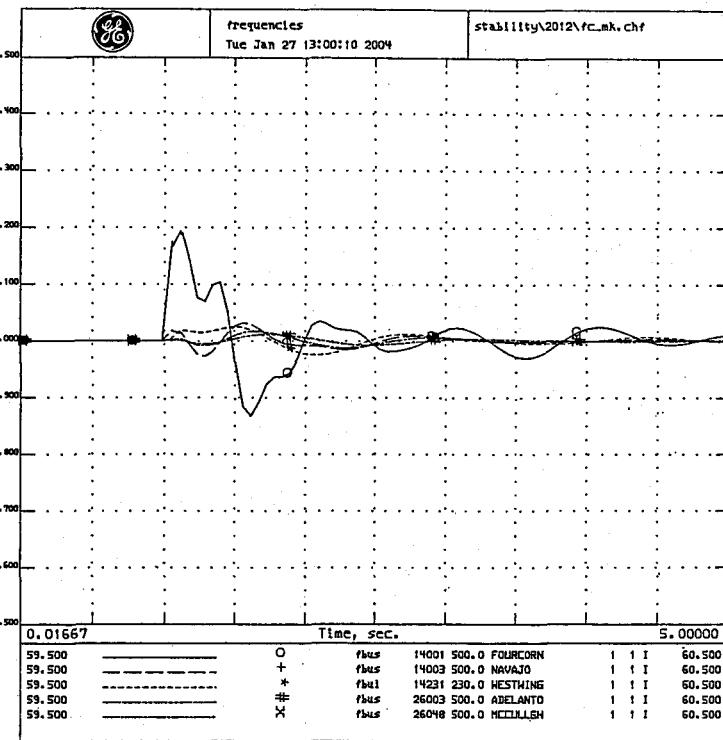
FCN FLT500 FCN-MNK out  
2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
FOURCORN-HOENKOPF STAB; 1/03; T=0 3P FLT FCN500|10X FLT DMPING|FLSH  
CAPS FCN-MKP|NAV-MKP|HC CLR FLT W/FCN-MKP|8C REIN CAPS;2012.4y4\HSCC.bpt

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FLT500 FCN-MNK out  
HS1A APPROVED BASE CASE  
MAY 19, 2003  
FOURCORN-HOENKOPF STAB; 1/03; T=0 3P FLT FCN500|10X FLT DMPING|FLSH  
CAPS FCN-MKP|NAV-MKP|HC CLR FLT W/FCN-MKP|8C REIN CAPS;2012.4y4\HSCC.bpt

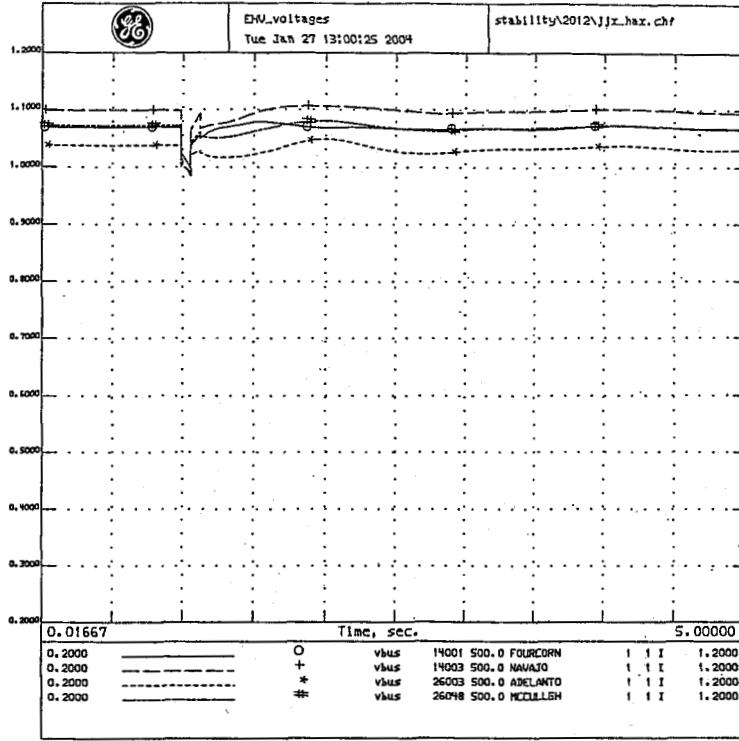
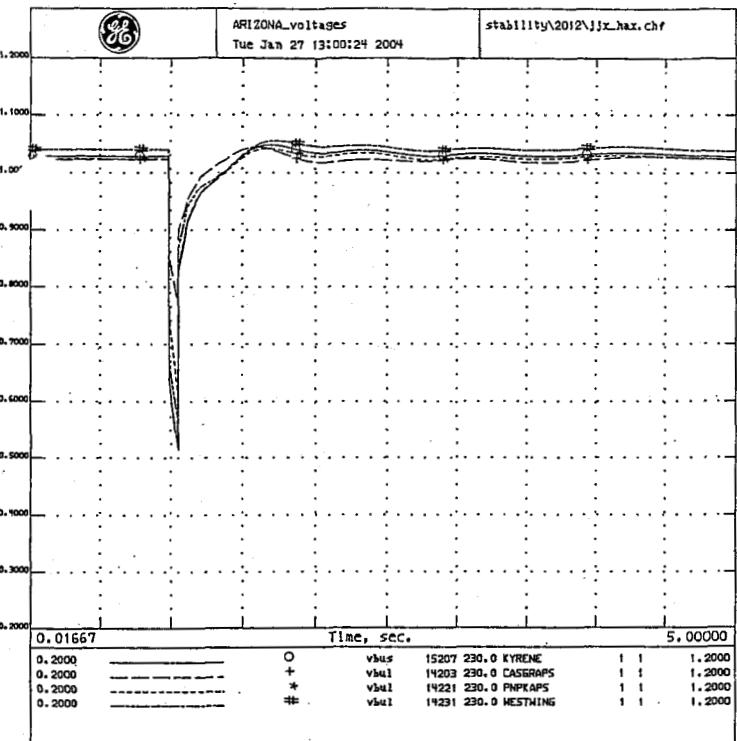
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FCN FLT500 FCN-MNK out  
2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
FOURCORN-HOENKOPF STAB; 1/03; T=0 3P FLT FCN500|10X FLT DMPING|FLSH  
CAPS FCN-MKP|NAV-MKP|HC CLR FLT W/FCN-MKP|8C REIN CAPS;2012.4y4\HSCC.bpt

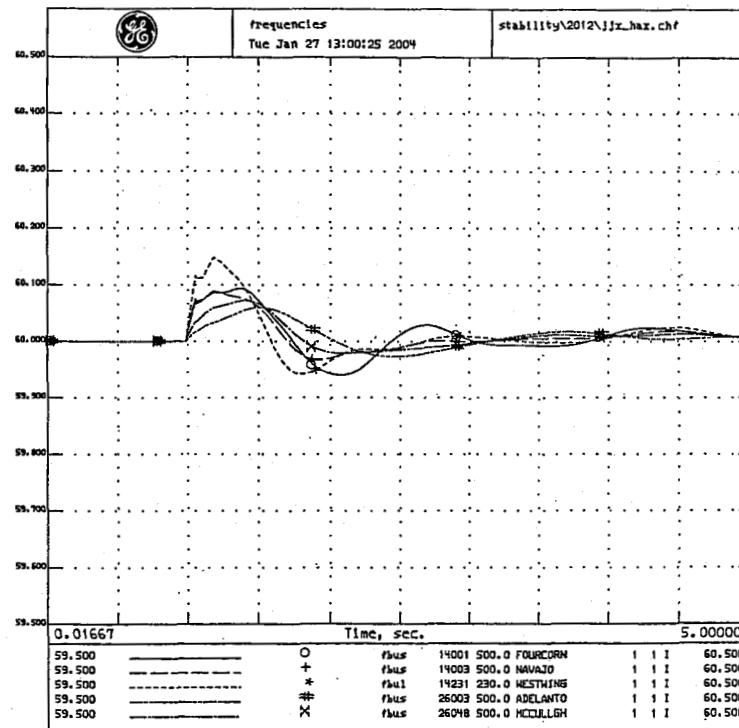
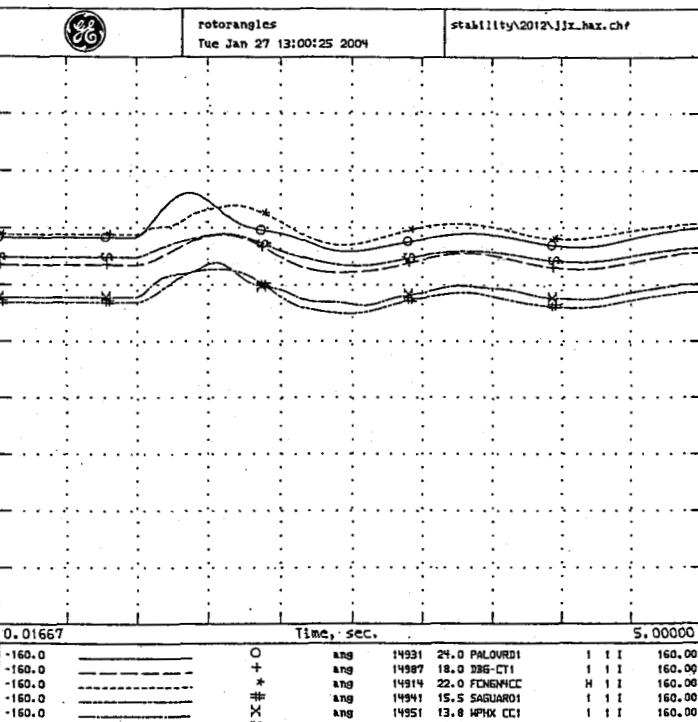
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NOVEMBER 7, 2002 DATA REQUEST.

C6



JOJOBA FLT JOJOBA-HASSY LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
HAS-JJ STAB #1 01/031 T=0 3P FLT JJ500|10X FLT IMPING|FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG|NC CLR FLT W/HAS-JJ|8C REIN|2012.4y4|HSCC.bpt

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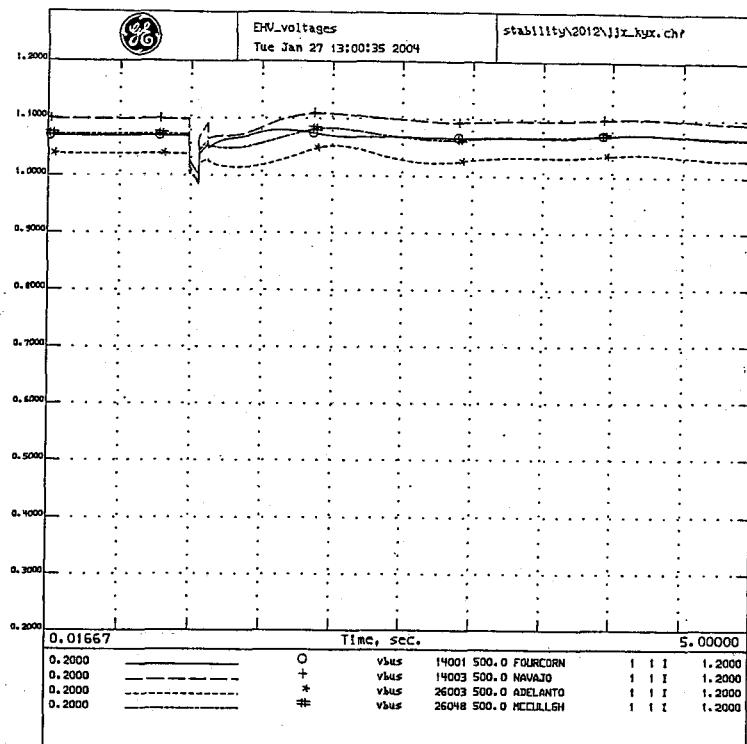
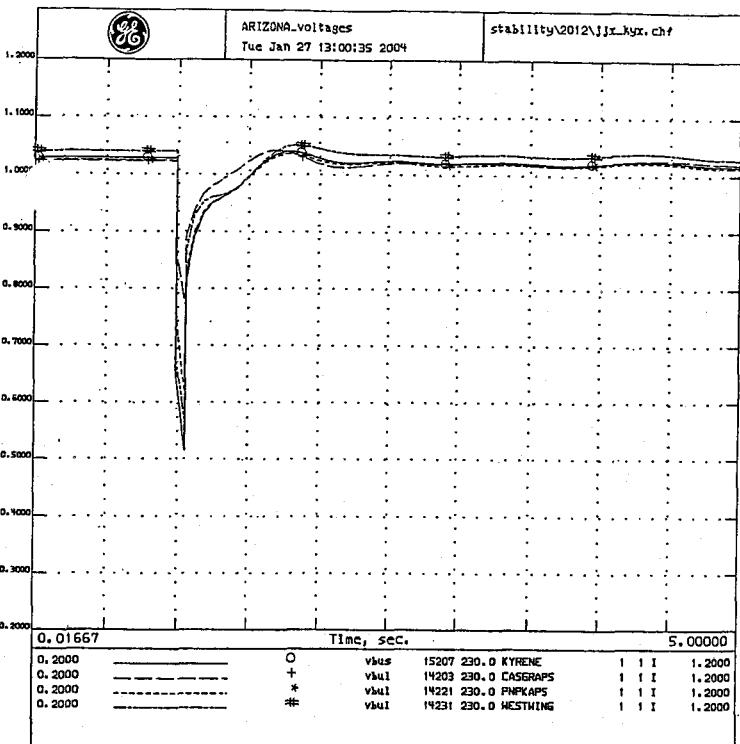
JOFLT JOJOBA-HASSY LINE OUT  
HSIA APPROVED BASE CASE  
MAY 19, 2003  
HAS-JJ STAB #1 01/031 T=0 3P FLT JJ500|10X FLT IMPING|FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG|NC CLR FLT W/HAS-JJ|8C REIN|2012.4y4|HSCC.bpt

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JOJOBA FLT JOJOBA-HASSY LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
HAS-JJ STAB #1 01/031 T=0 3P FLT JJ500|10X FLT IMPING|FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG|NC CLR FLT W/HAS-JJ|8C REIN|2012.4y4|HSCC.bpt

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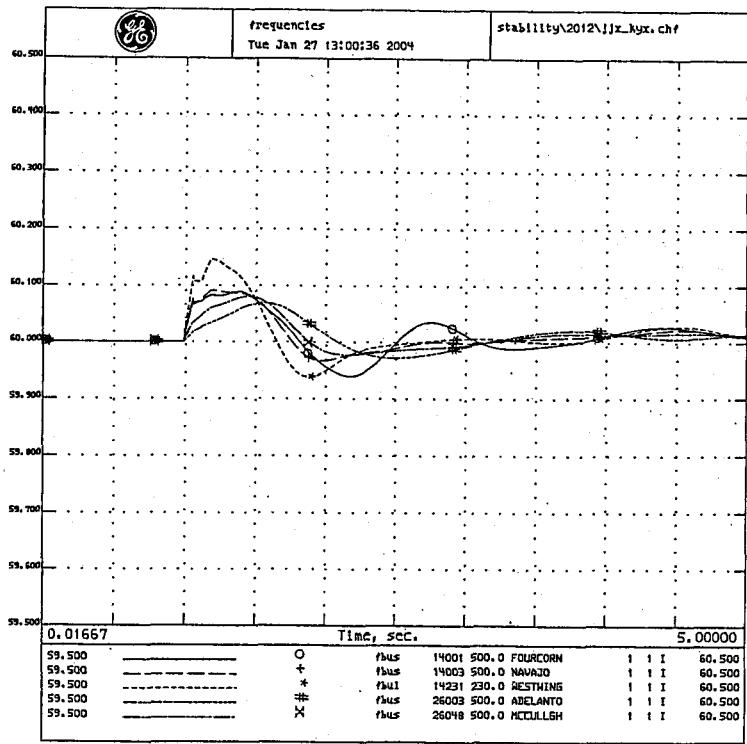
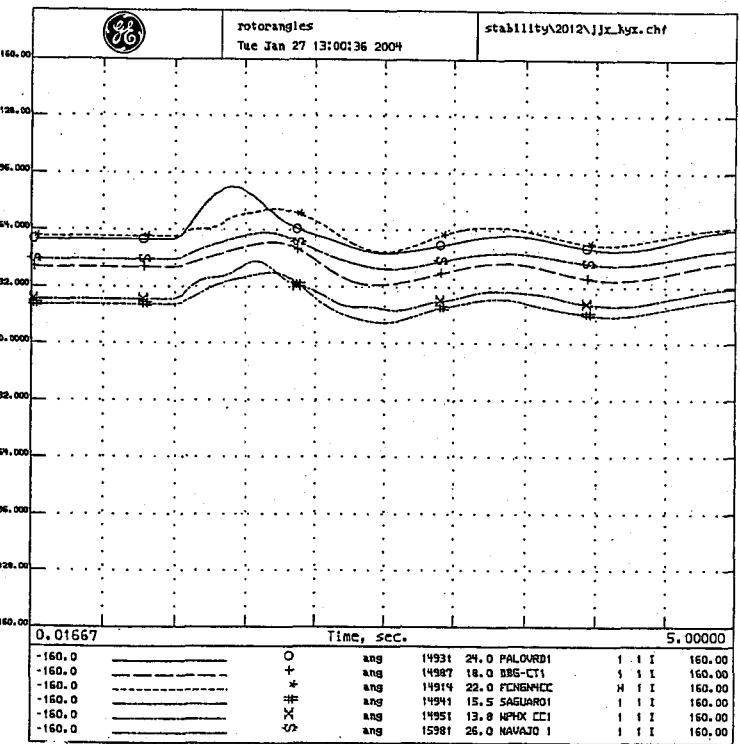


JOJOBA FLT JOJOBA-KYR LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
JJ-KYR STAB +1; 01/03; T=0 3P FLT JJ500;10X FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/JJ-KYR;BC REIN;2012.4y4;NSCC.bpt

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JOJOBA FLT JOJOBA-KYR LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
JJ-KYR STAB +1; 01/03; T=0 3P FLT JJ500;10X FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/JJ-KYR;BC REIN;2012.4y4;NSCC.bpt

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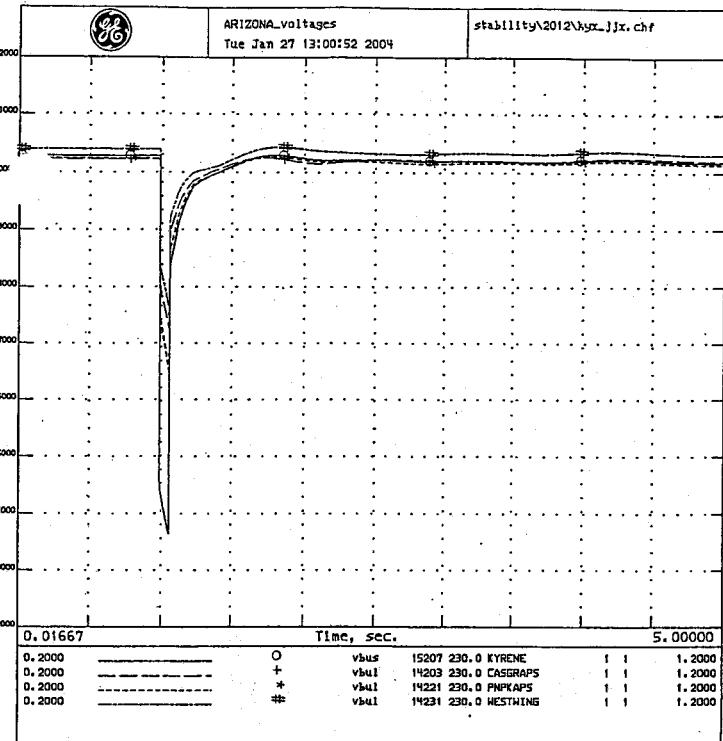


JOJOBA FLT JOJOBA-KYR LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
JJ-KYR STAB +1; 01/03; T=0 3P FLT JJ500;10X FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/JJ-KYR;BC REIN;2012.4y4;NSCC.bpt

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JOJOBA FLT JOJOBA-KYR LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
JJ-KYR STAB +1; 01/03; T=0 3P FLT JJ500;10X FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG;4C CLR FLT W/JJ-KYR;BC REIN;2012.4y4;NSCC.bpt

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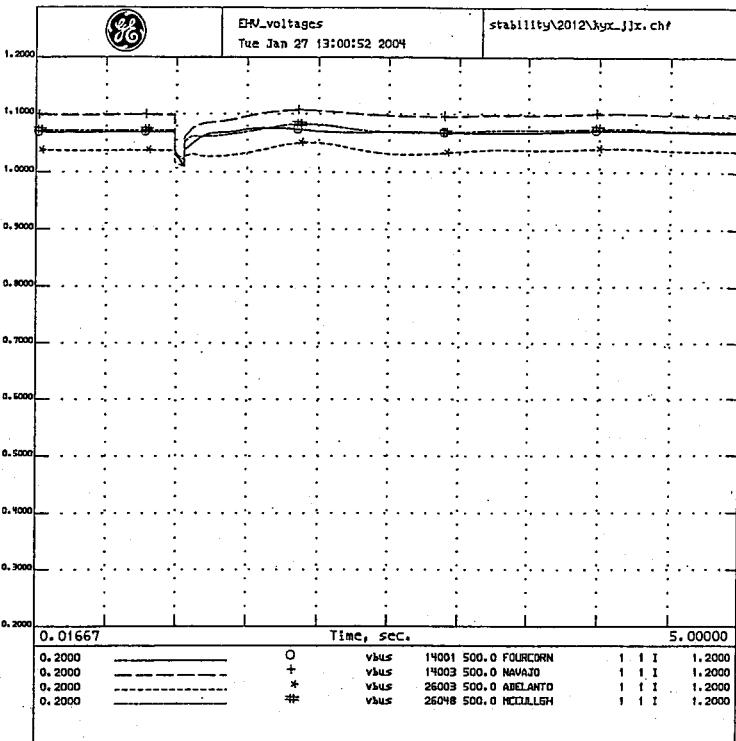
2012 HS1A APPROVED BASE CASE

MAY 19, 2003

JJ-KYR STAB +1; 01/03; T=0 3P FLT KYR500;

HC CLR FLT W/JJ-KYR|2012.4y4|HSCC.bpt

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KYRENE FLT KYR-JOJOBIA LINE OUT

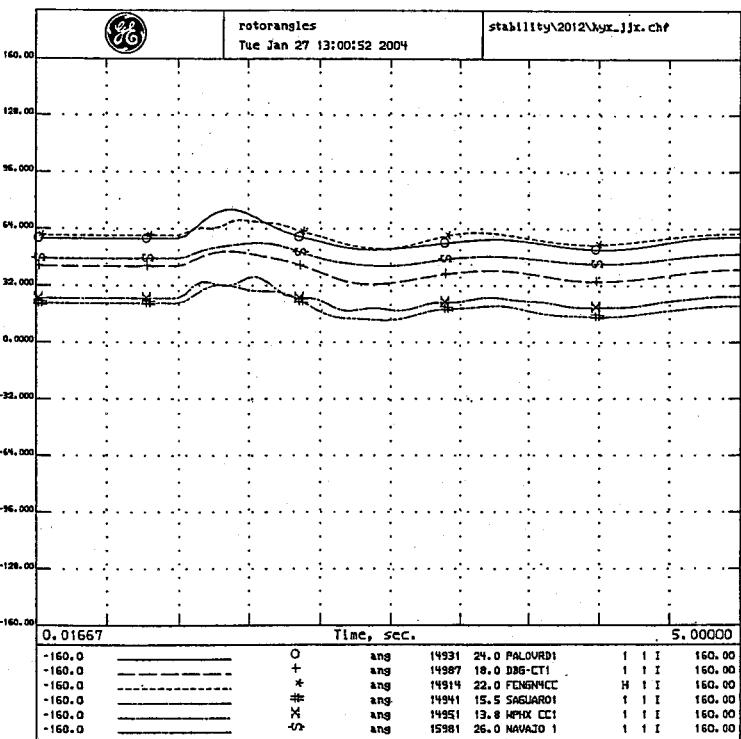
2012 HS1A APPROVED BASE CASE

MAY 19, 2003

JJ-KYR STAB +1; 01/03; T=0 3P FLT KYR500;

HC CLR FLT W/JJ-KYR|2012.4y4|HSCC.bpt

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NOVEMBER 7, 2002 DATA REQUEST.



NE FLT KYR-JOJOBIA LINE OUT

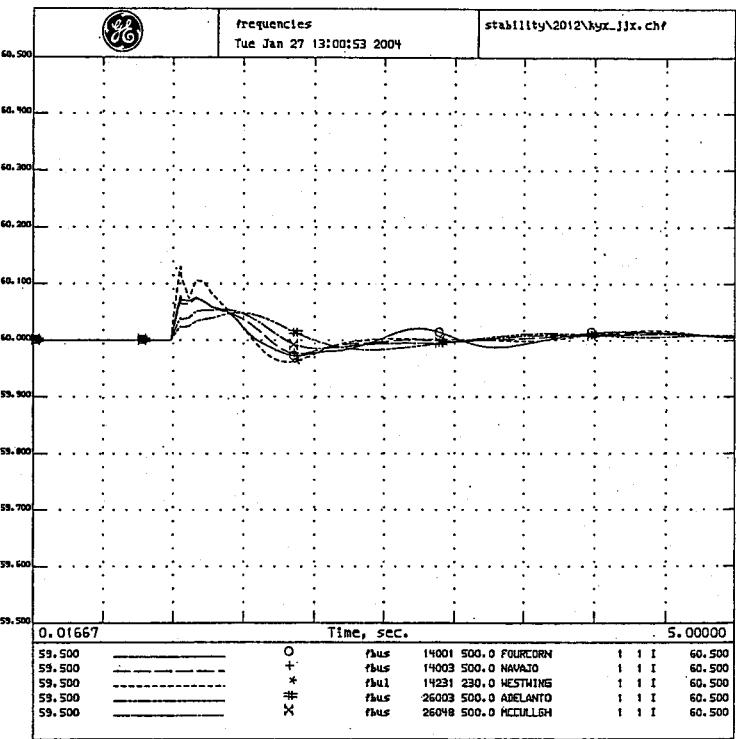
2012 HS1A APPROVED BASE CASE

MAY 19, 2003

JJ-KYR STAB +1; 01/03; T=0 3P FLT KYR500;

HC CLR FLT W/JJ-KYR|2012.4y4|HSCC.bpt

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KYRENE FLT KYR-JOJOBIA LINE OUT

2012 HS1A APPROVED BASE CASE

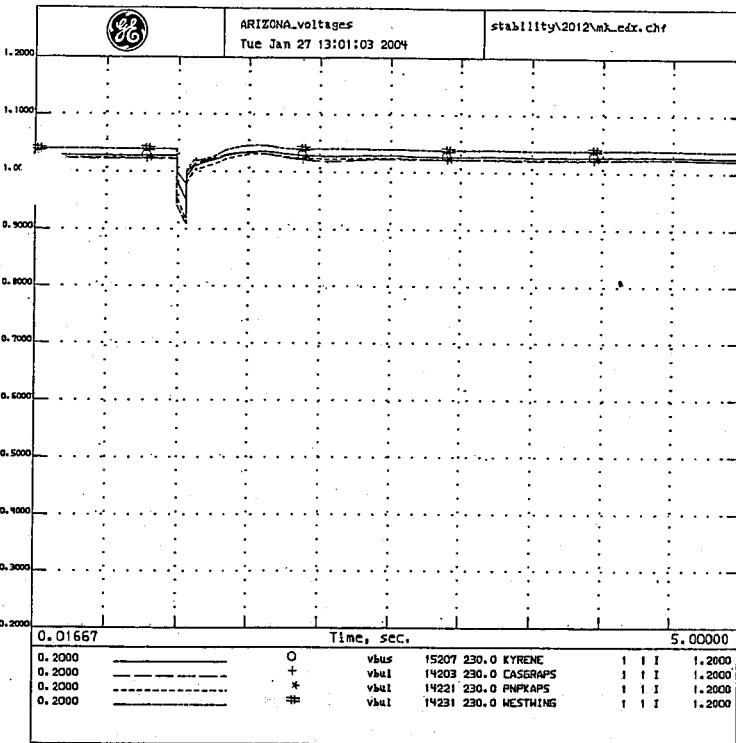
MAY 19, 2003

JJ-KYR STAB +1; 01/03; T=0 3P FLT KYR500;

HC CLR FLT W/JJ-KYR|2012.4y4|HSCC.bpt

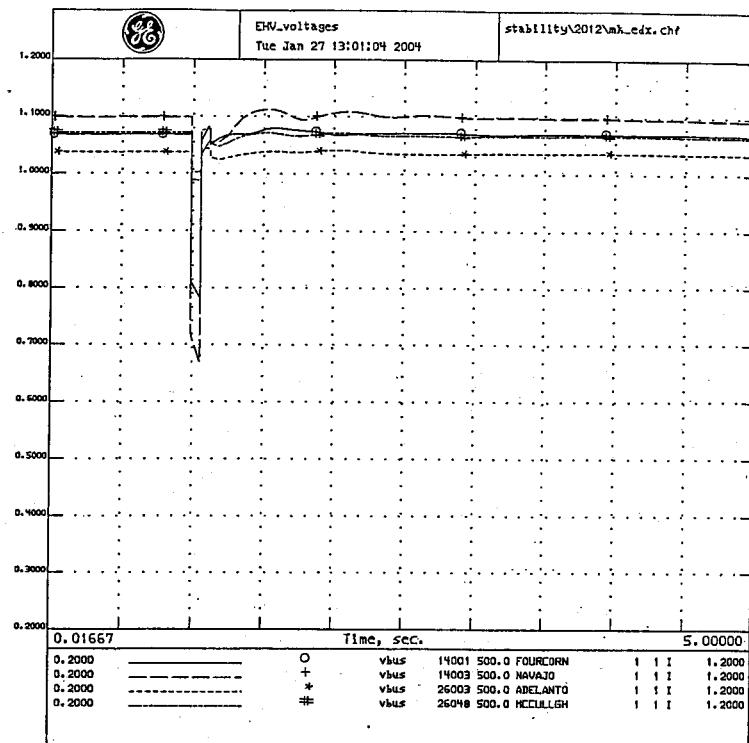
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NOVEMBER 7, 2002 DATA REQUEST.

C9



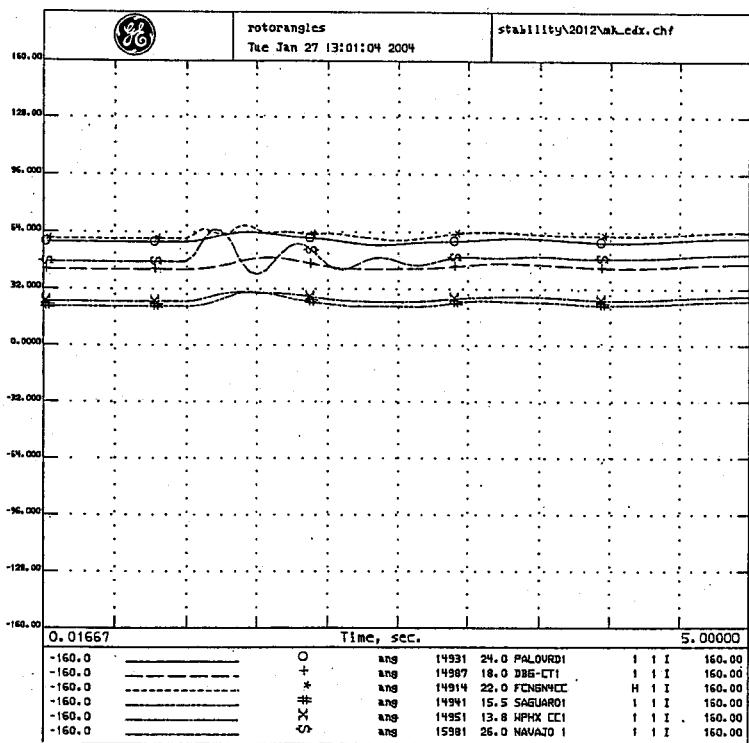
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MKP FLT. MKP-ELD line out  
MAY 19, 2003  
MKP-ELD STAB: 1/03; T=0 3P FLT MKPS00;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT W/MKP-ELD;BC REIN;2012.dyd;WSCC.bat

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
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NOVEMBER 7, 2002 DATA REQUEST.



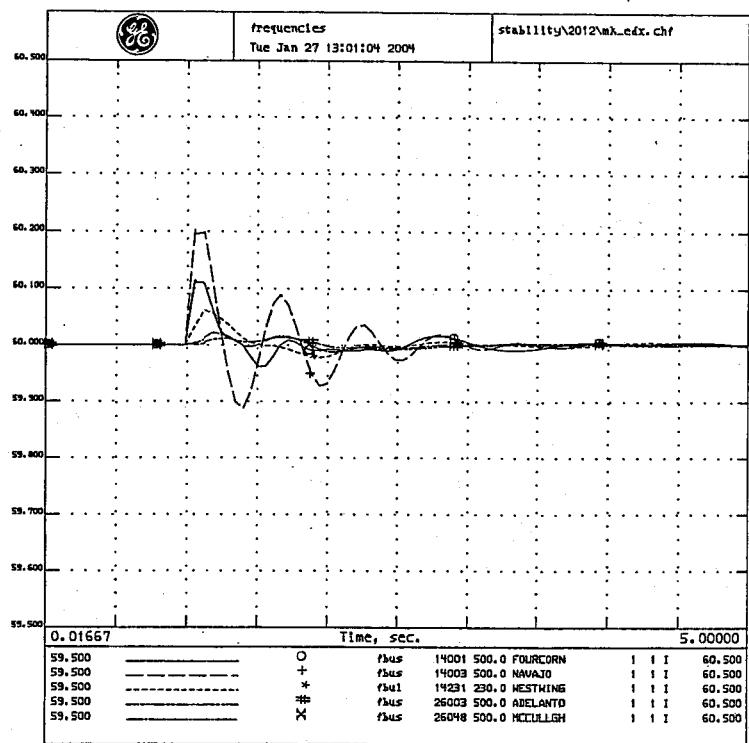
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MKP FLT. MKP-ELD line out  
MAY 19, 2003  
MKP-ELD STAB: 1/03; T=0 3P FLT MKPS00;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT W/MKP-ELD;BC REIN;2012.dyd;WSCC.bat

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WESTERN ELECTRICITY COORDINATING COUNCIL  
FLT. MKP-ELD line out  
MAY 19, 2003  
MKP-ELD STAB: 1/03; T=0 3P FLT MKPS00;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT W/MKP-ELD;BC REIN;2012.dyd;WSCC.bat

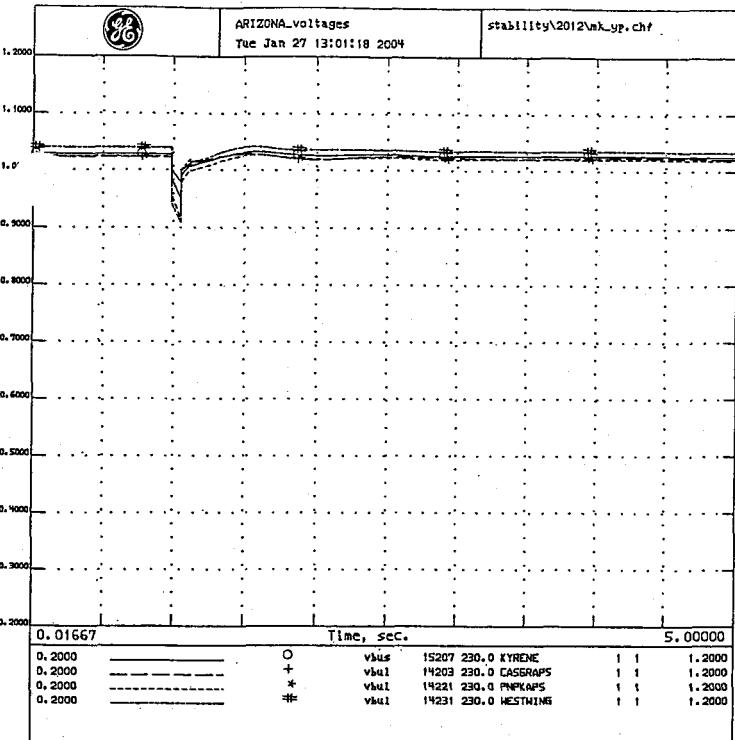
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WESTERN ELECTRICITY COORDINATING COUNCIL  
MKP FLT. MKP-ELD line out  
MAY 19, 2003  
MKP-ELD STAB: 1/03; T=0 3P FLT MKPS00;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT W/MKP-ELD;BC REIN;2012.dyd;WSCC.bat

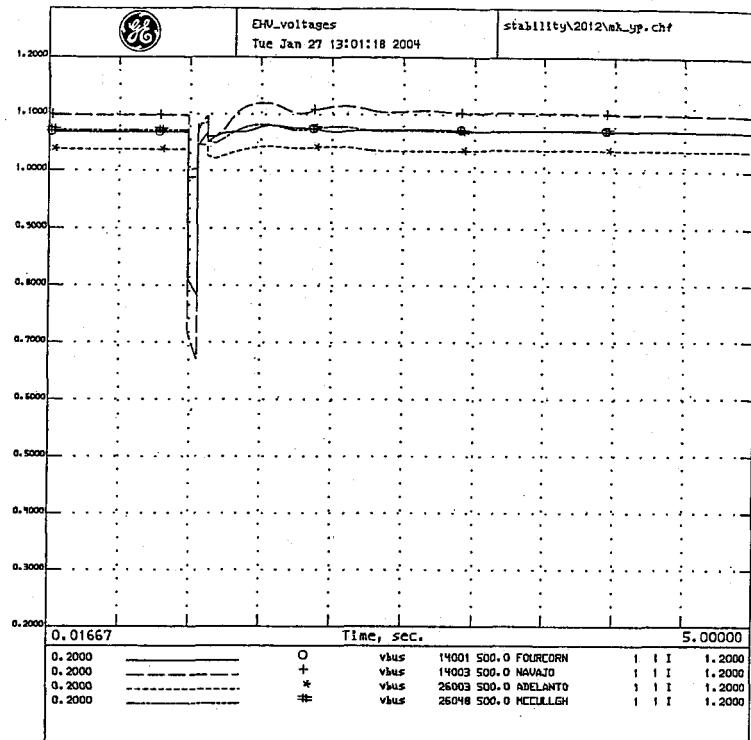
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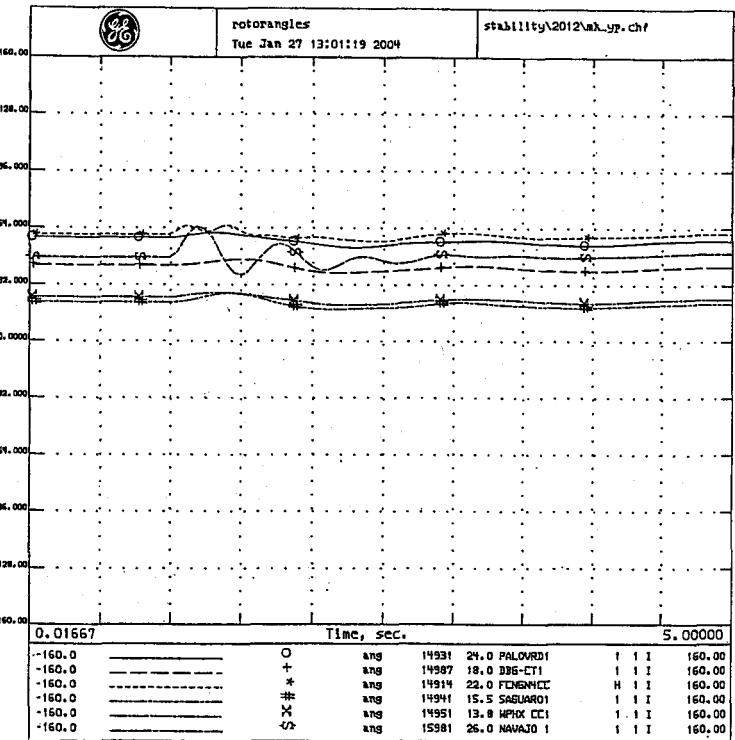
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
MKP-YAV STAB1 1/031 T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;HC CLR FLT W/MKP-YAV;BC REIN;2012.4y4;NSCC.bat

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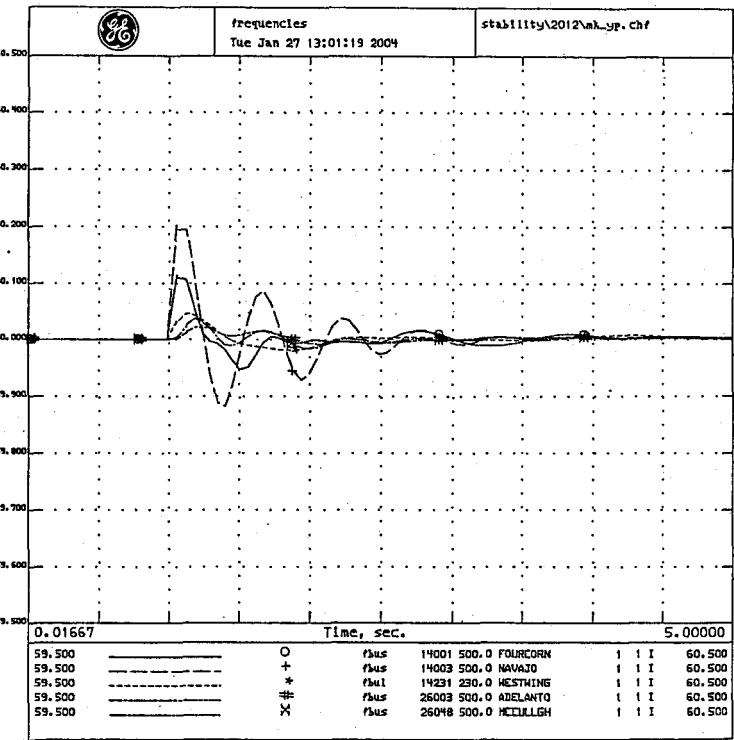
MKP, FLT MKP-YAV line out  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
MKP-YAV STAB1 1/031 T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;HC CLR FLT W/MKP-YAV;BC REIN;2012.4y4;NSCC.bat

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FLT MKP-YAV line out  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
MKP-YAV STAB1 1/031 T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;HC CLR FLT W/MKP-YAV;BC REIN;2012.4y4;NSCC.bat

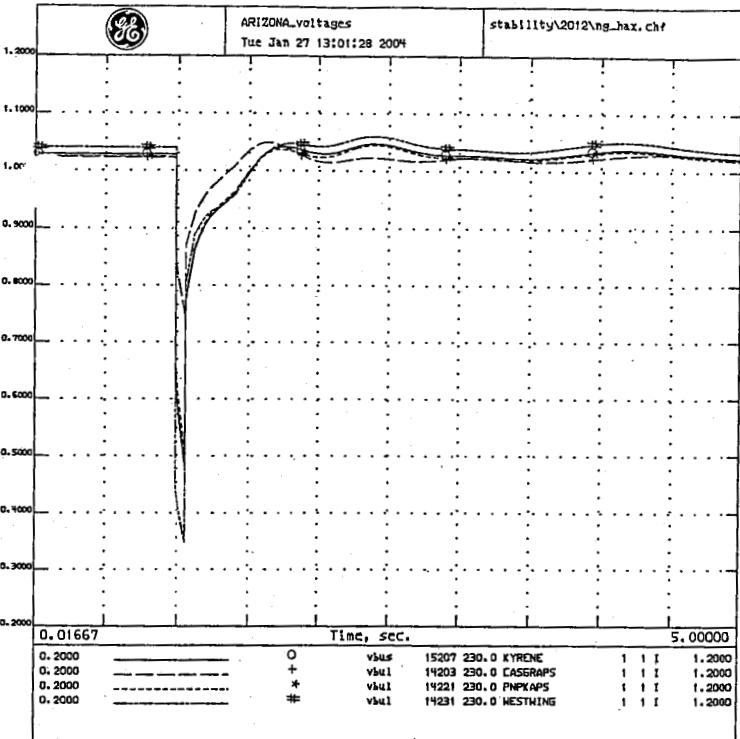
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MKP, FLT MKP-YAV line out  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
MKP-YAV STAB1 1/031 T=0 3P FLT MKP500;FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MCC/MKP,MKP-ELD;HC CLR FLT W/MKP-YAV;BC REIN;2012.4y4;NSCC.bat

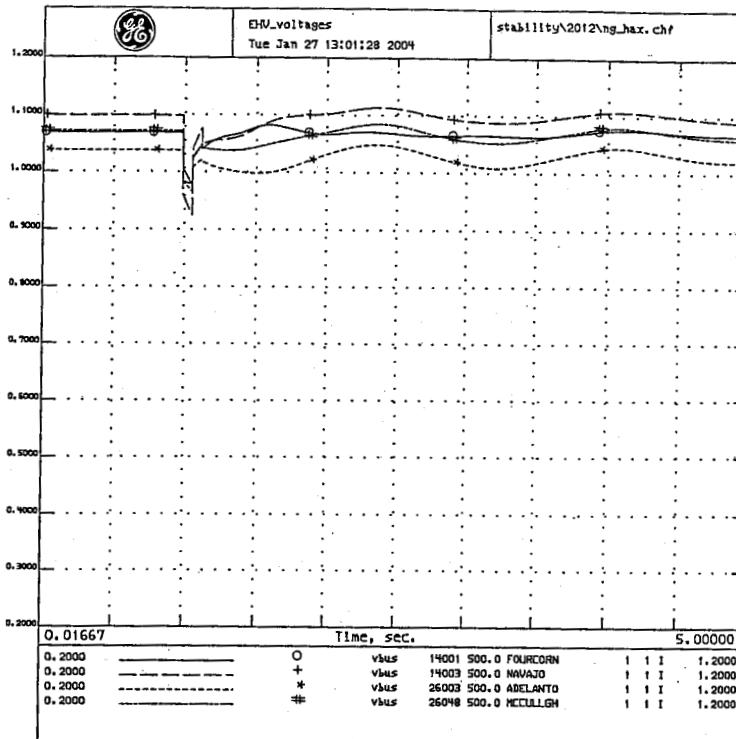
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C11



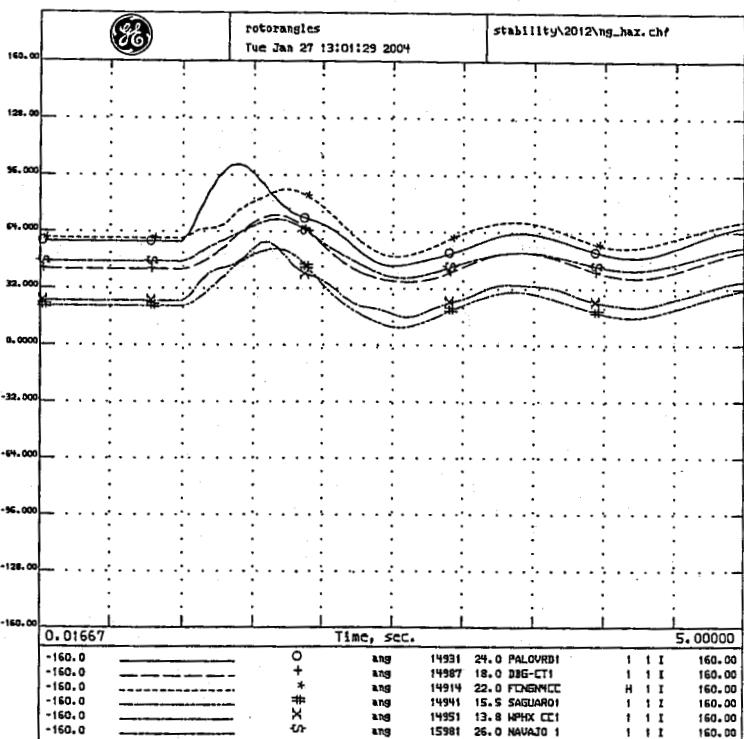
N. GILA FLT N. GILA-HASSY LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
N. GILA STAB, 3 PH FLT N. GILA 500KV  
FLASH CAPS, 1/4 CYC CLR FLT\HASSAYMPA-NG OUT\1/8 CYC REIN CAPS

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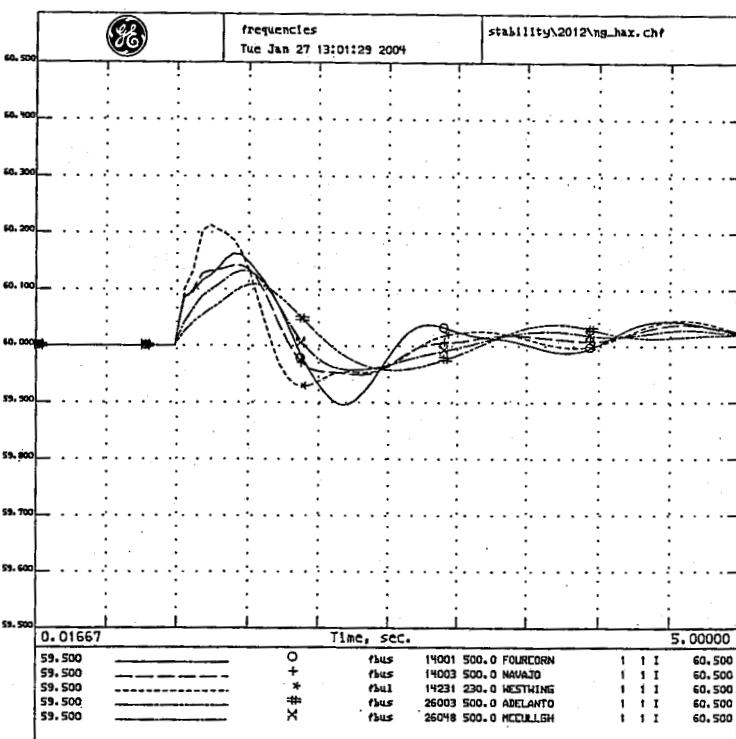
N. GILA FLT N. GILA-HASSY LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
N. GILA STAB, 3 PH FLT N. GILA 500KV  
FLASH CAPS, 1/4 CYC CLR FLT\HASSAYMPA-NG OUT\1/8 CYC REIN CAPS

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A FLT N. GILA-HASSY LINE OUT  
HSIA APPROVED BASE CASE  
MAY 19, 2003  
N. GILA STAB, 3 PH FLT N. GILA 500KV  
FLASH CAPS, 1/4 CYC CLR FLT\HASSAYMPA-NG OUT\1/8 CYC REIN CAPS

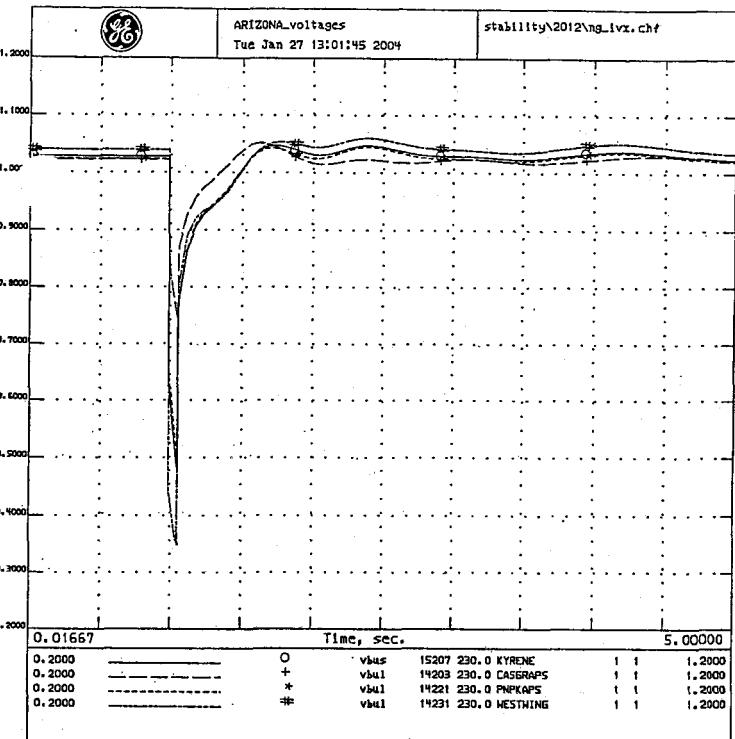
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N. GILA FLT N. GILA-HASSY LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
N. GILA STAB, 3 PH FLT N. GILA 500KV  
FLASH CAPS, 1/4 CYC CLR FLT\HASSAYMPA-NG OUT\1/8 CYC REIN CAPS

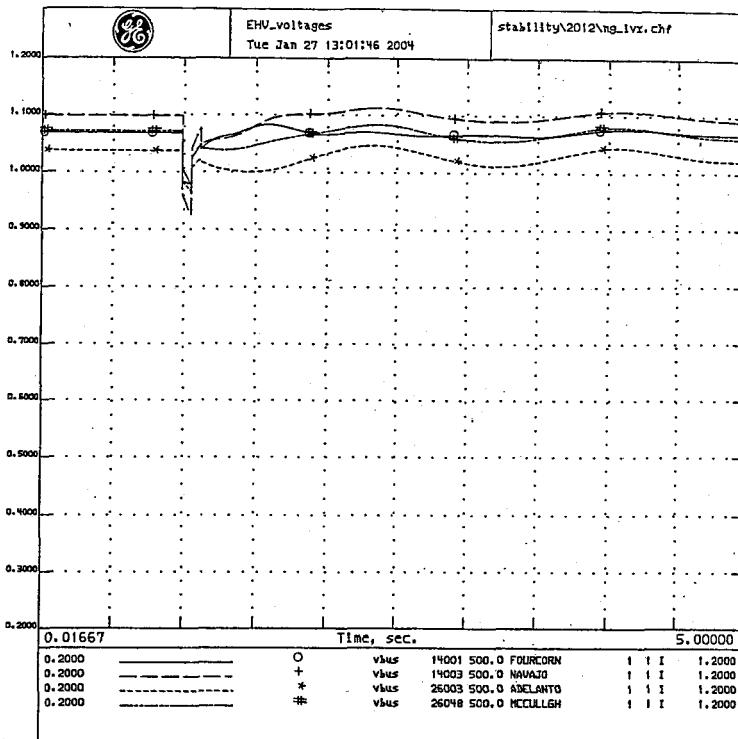
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C12



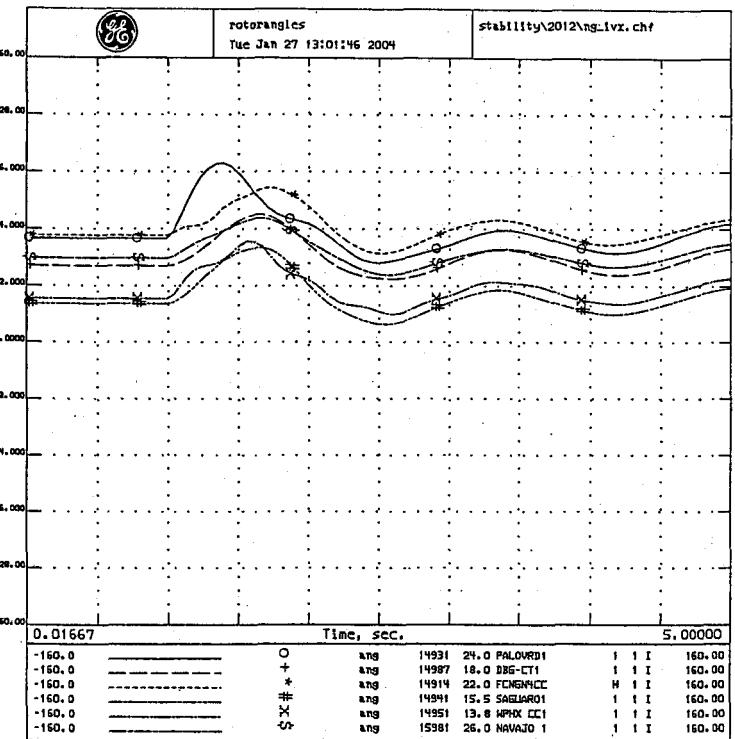
N. GILA FLT N. GILA-IMP. V LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
N. GILA STAB,3 PH FLT N. GILA 500KV  
FLASH CAPS,W/4 CYC CLR FLT;IMPV-NG OUT;4/8 CYC REIN CAPS

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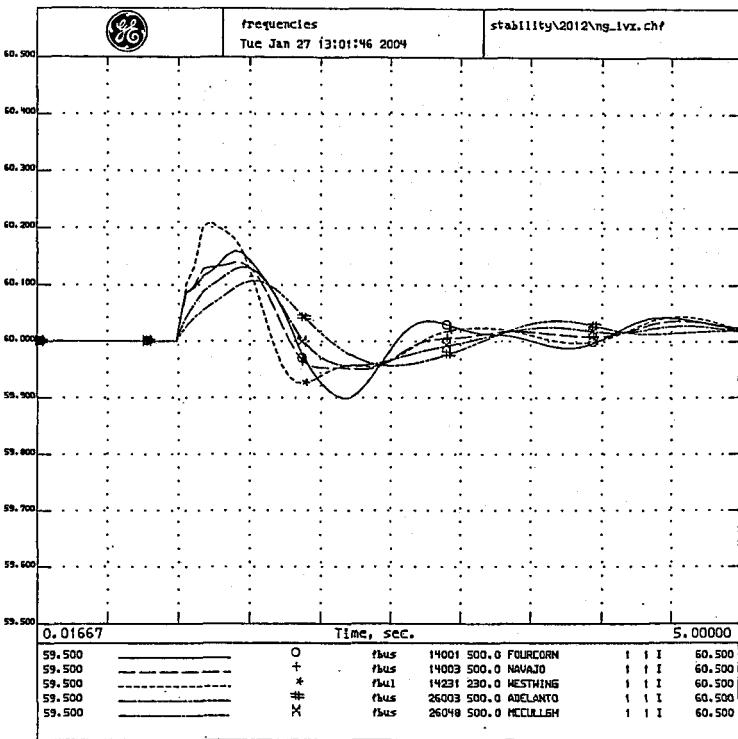
N. GILA FLT N. GILA-IMP. V LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
N. GILA STAB,3 PH FLT N. GILA 500KV  
FLASH CAPS,W/4 CYC CLR FLT;IMPV-NG OUT;4/8 CYC REIN CAPS

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A FLT N. GILA-IMP. V LINE OUT  
HSIA APPROVED BASE CASE  
MAY 19, 2003  
N. GILA STAB,3 PH FLT N. GILA 500KV  
FLASH CAPS,W/4 CYC CLR FLT;IMPV-NG OUT;4/8 CYC REIN CAPS

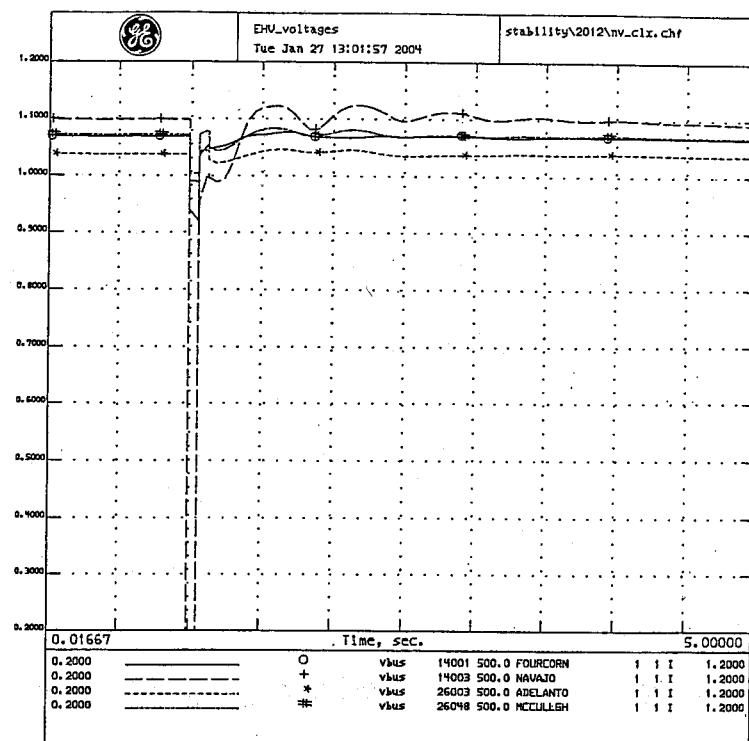
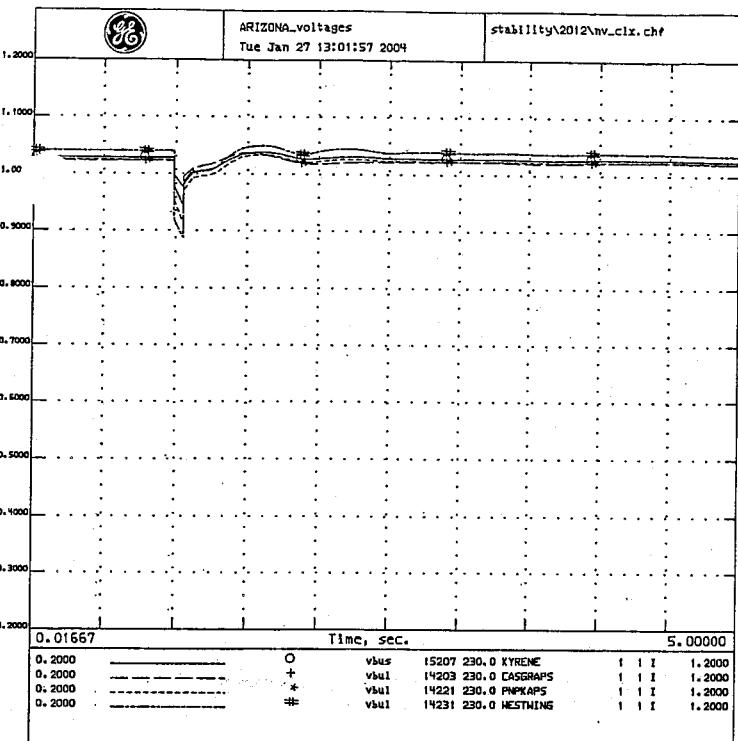
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
N. GILA STAB,3 PH FLT N. GILA 500KV  
FLASH CAPS,W/4 CYC CLR FLT;IMPV-NG OUT;4/8 CYC REIN CAPS

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C13

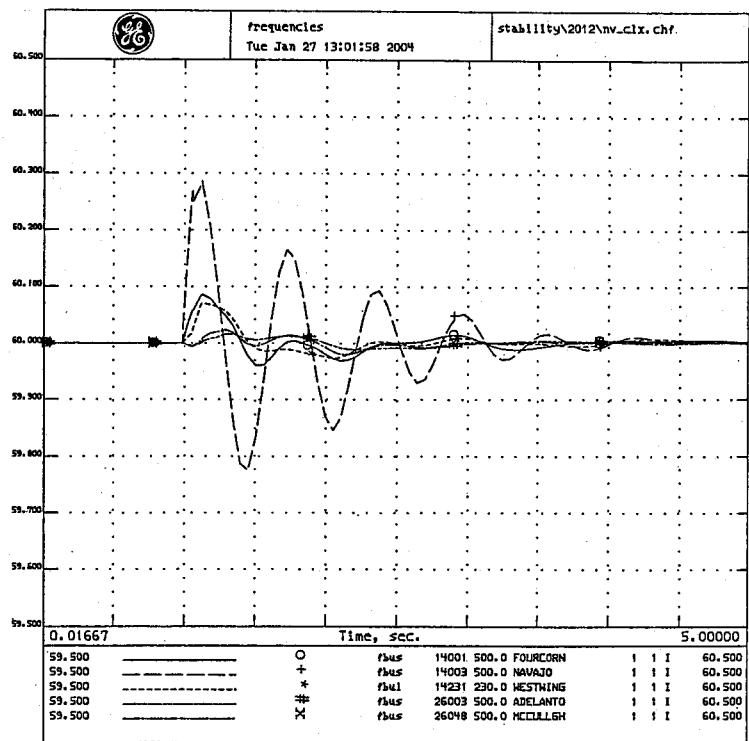
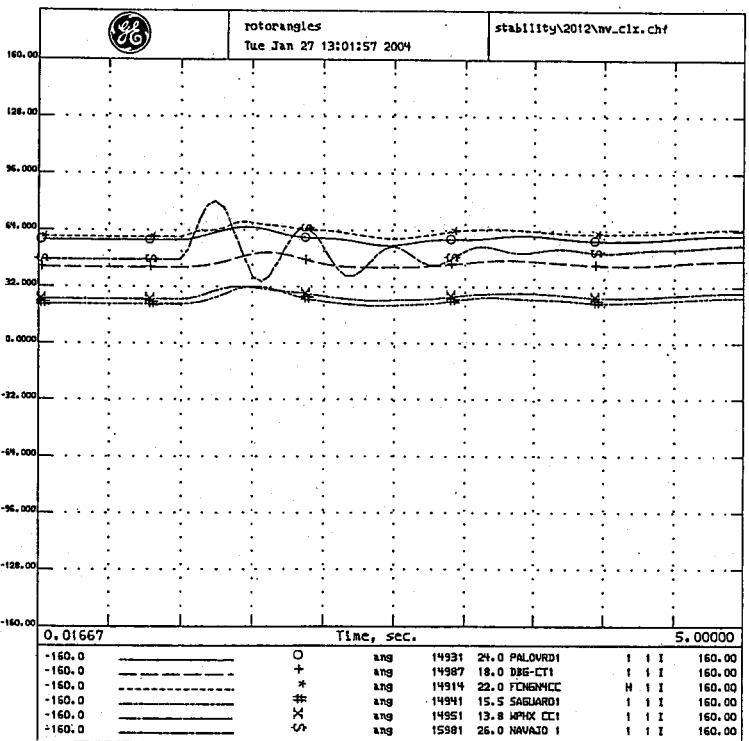


WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV\_FLT\_Nav-Crystal line out  
MAY 19, 2003  
NAV-CRYS STAB1 1/03; T=0 3P FLT NAV500; 6% FLT DMPING;FLSH CAPS  
NAV-MCC/MKP,MKP-ELD\4C CLR FLT W/NAV-CRYS\8C REIN\2012.4y4\WSCC.bat

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WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV\_FLT\_Nav-Crystal line out  
MAY 19, 2003  
NAV-CRYS STAB1 1/03; T=0 3P FLT NAV500; 6% FLT DMPING;FLSH CAPS  
NAV-MCC/MKP,MKP-ELD\4C CLR FLT W/NAV-CRYS\8C REIN\2012.4y4\WSCC.bat

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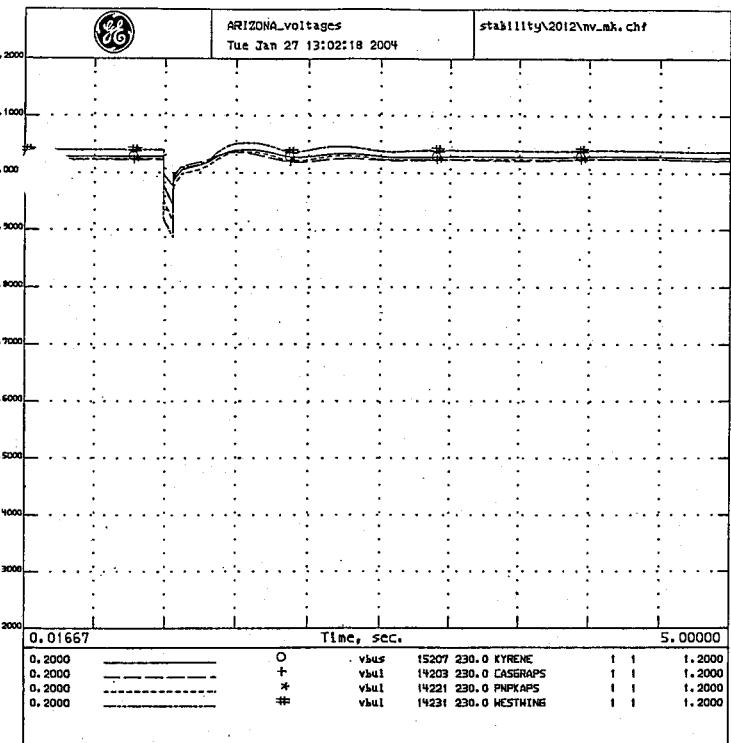
WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV\_FLT\_Nav-Crystal line out  
MAY 19, 2003  
NAV-CRYS STAB1 1/03; T=0 3P FLT NAV500; 6% FLT DMPING;FLSH CAPS  
NAV-MCC/MKP,MKP-ELD\4C CLR FLT W/NAV-CRYS\8C REIN\2012.4y4\WSCC.bat

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NAV\_FLT\_Nav-Crystal line out  
MAY 19, 2003  
NAV-CRYS STAB1 1/03; T=0 3P FLT NAV500; 6% FLT DMPING;FLSH CAPS  
NAV-MCC/MKP,MKP-ELD\4C CLR FLT W/NAV-CRYS\8C REIN\2012.4y4\WSCC.bat

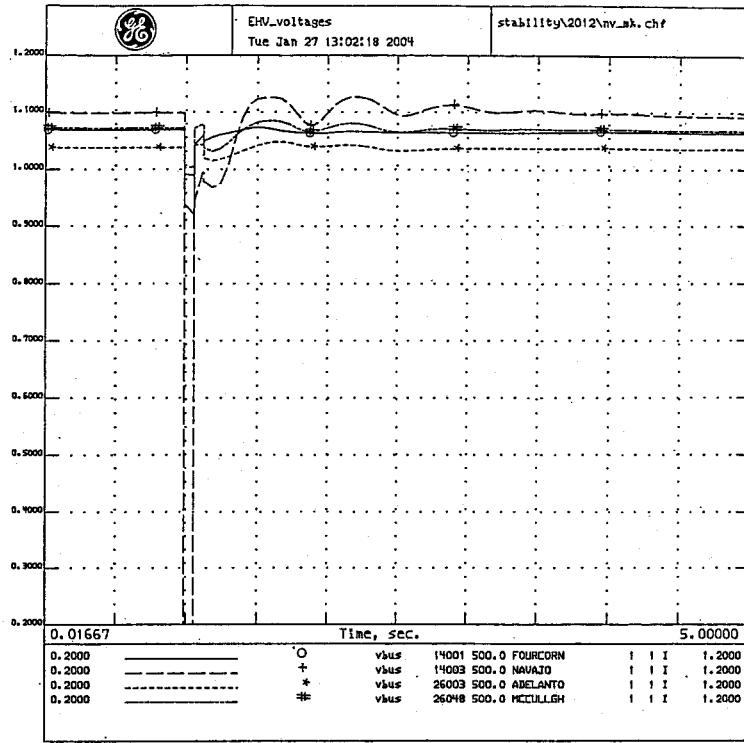
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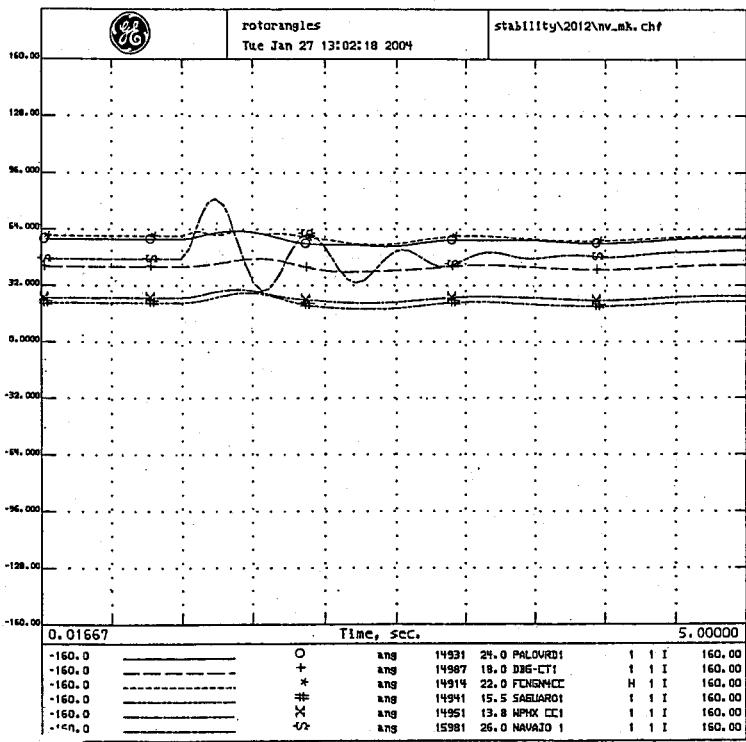
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NAV. FLT. Navjo-Mhn. line out  
MAY 19, 2003  
NAV-MKP STAB; 1/03; T=0 3P FLT NAV500; 6X FLT IMPINGEFLSH CAPS  
NAV-HCC/MKP,MKP-ELD;4C CLR FLT W/NAV-MKP;8C REIN;2012.4y4;WSCC.bat

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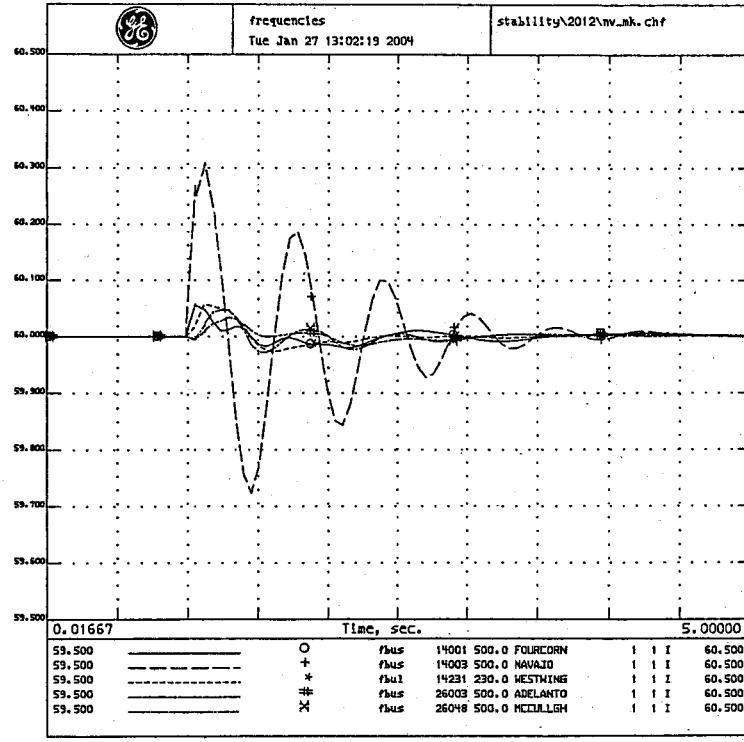
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NAV. FLT. Navjo-Mhn. line out  
MAY 19, 2003  
NAV-MKP STAB; 1/03; T=0 3P FLT NAV500; 6X FLT IMPINGEFLSH CAPS  
NAV-HCC/MKP,MKP-ELD;4C CLR FLT W/NAV-MKP;8C REIN;2012.4y4;WSCC.bat

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WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV. FLT. Navjo-Mhn. line out  
MAY 19, 2003  
NAV-MKP STAB; 1/03; T=0 3P FLT NAV500; 6X FLT IMPINGEFLSH CAPS  
NAV-HCC/MKP,MKP-ELD;4C CLR FLT W/NAV-MKP;8C REIN;2012.4y4;WSCC.bat

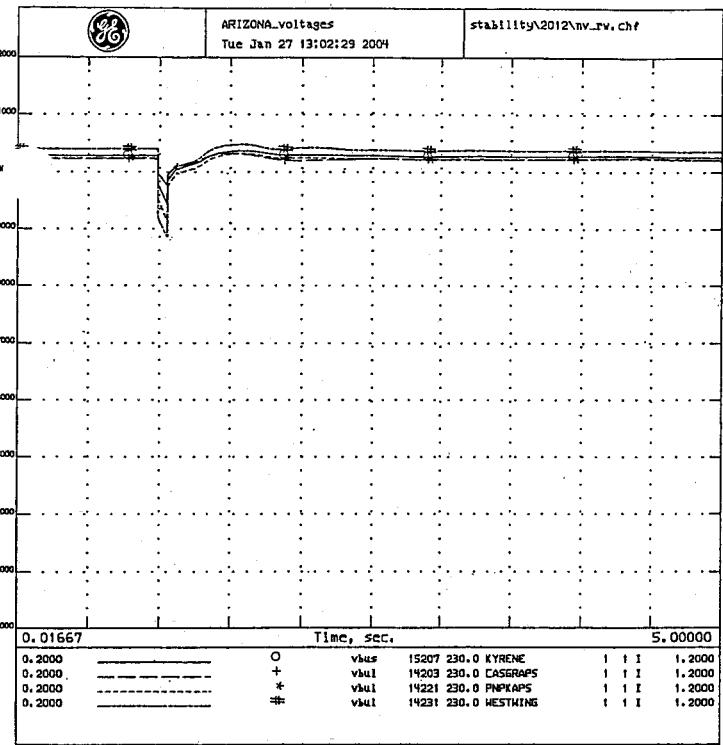
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WESTERN ELECTRICITY COORDINATING COUNCIL  
NAV. FLT. Navjo-Mhn. line out  
MAY 19, 2003  
NAV-MKP STAB; 1/03; T=0 3P FLT NAV500; 6X FLT IMPINGEFLSH CAPS  
NAV-HCC/MKP,MKP-ELD;4C CLR FLT W/NAV-MKP;8C REIN;2012.4y4;WSCC.bat

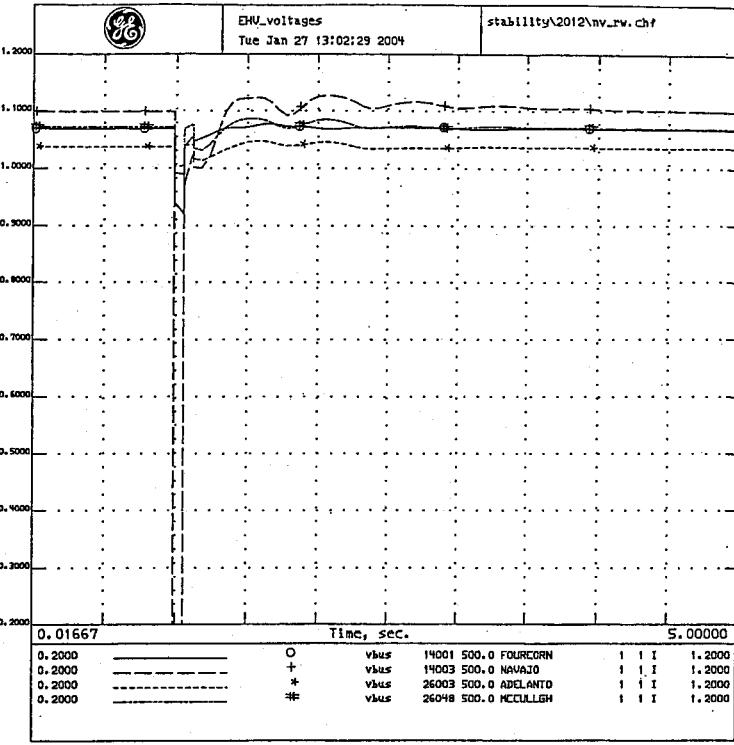
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C15



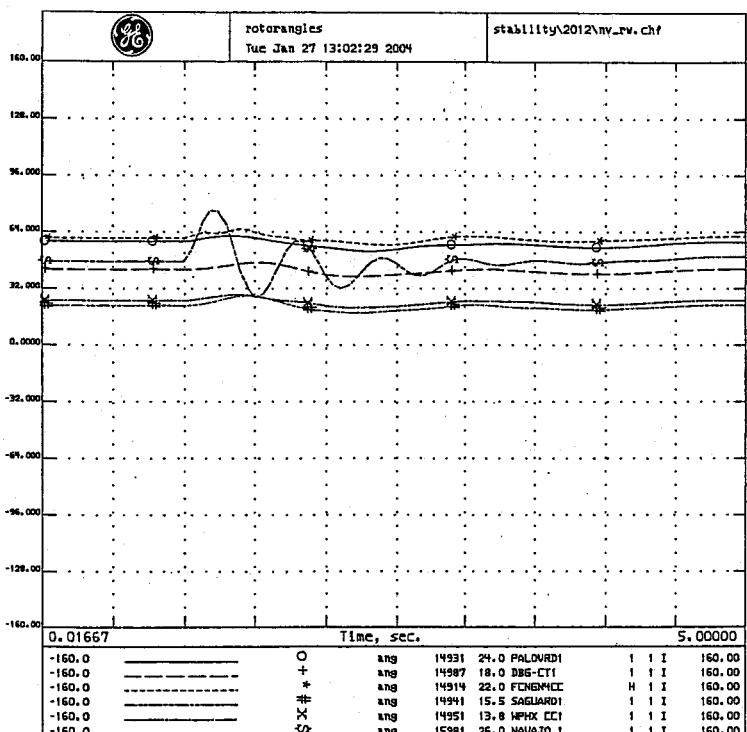
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
NAV-RHY STAB1 1/03; T=0 3P FLT NAV500; 6% FLT DMPNG;FLSH CAPS  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT W/NAV-RHY;BC REIN|2012.d44\HSCL.bat

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
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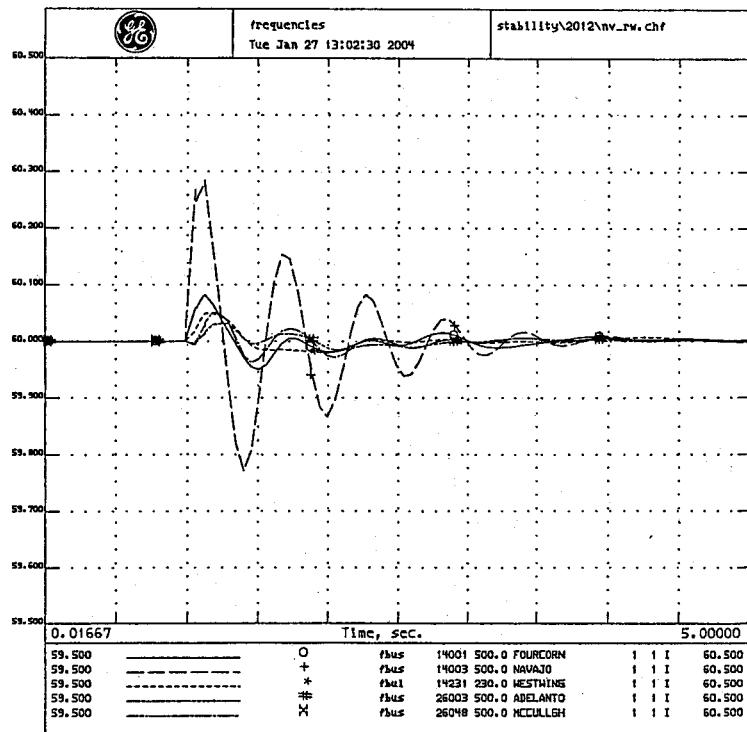
NAV FLT NAV-RM LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
NAV-RHY STAB1 1/03; T=0 3P FLT NAV500; 6% FLT DMPNG;FLSH CAPS  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT W/NAV-RHY;BC REIN|2012.d44\HSCL.bat

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NOVEMBER 7, 2002 DATA REQUEST.



FLT NAV-RM LINE OUT  
.2 HSIA APPROVED BASE CASE  
MAY 19, 2003  
NAV-RHY STAB1 1/03; T=0 3P FLT NAV500; 6% FLT DMPNG;FLSH CAPS  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT W/NAV-RHY;BC REIN|2012.d44\HSCL.bat

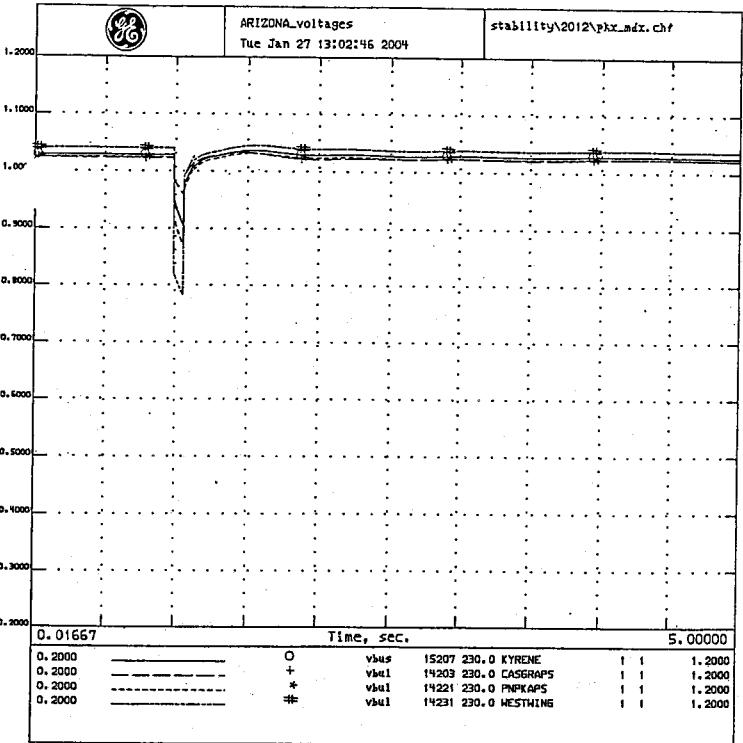
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NAV FLT NAV-RM LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
NAV-RHY STAB1 1/03; T=0 3P FLT NAV500; 6% FLT DMPNG;FLSH CAPS  
NAV-MCC/MKP,MKP-ELD;4C CLR FLT W/NAV-RHY;BC REIN|2012.d44\HSCL.bat

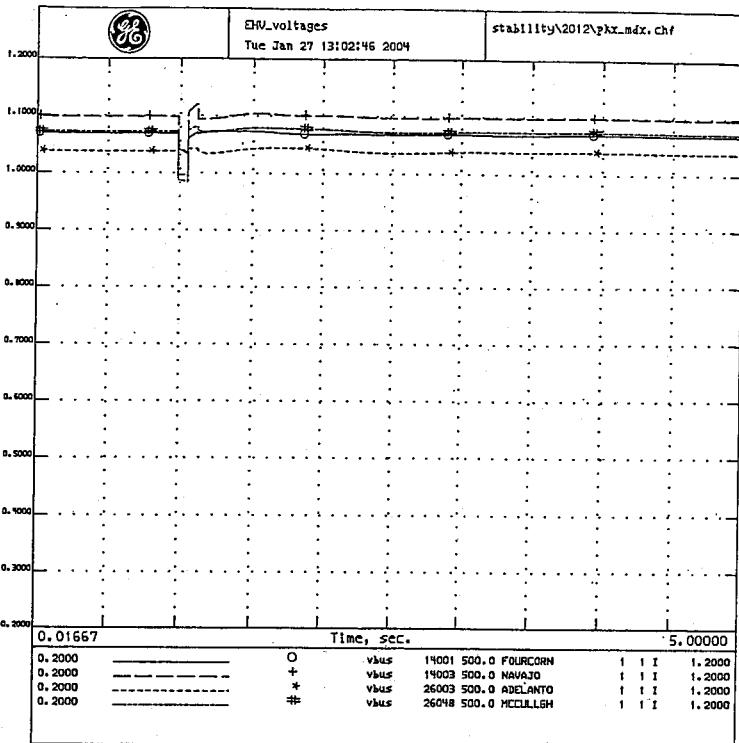
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NOVEMBER 7, 2002 DATA REQUEST.

C16



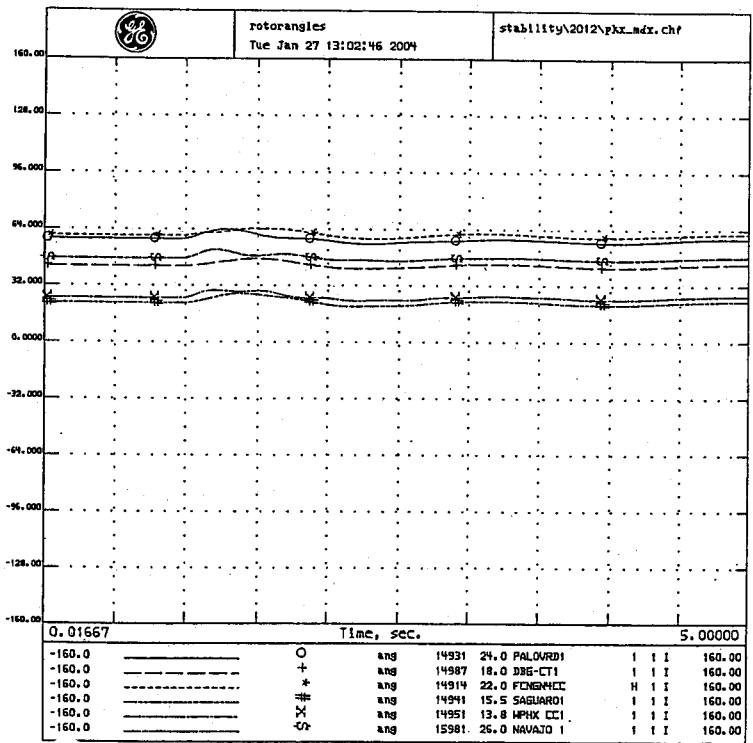
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
PERK-MEAD STAB: 01/03; T=0 3P FLT PERKS001FLSH CAPS MHP-YAU/YAU-HNG,  
NAV-MHP/HNG;4C CLR FLT W/PERK-MEAD;8C REIN;2012.4y4HSCL.bat

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
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NOVEMBER 7, 2002 DATA REQUEST.



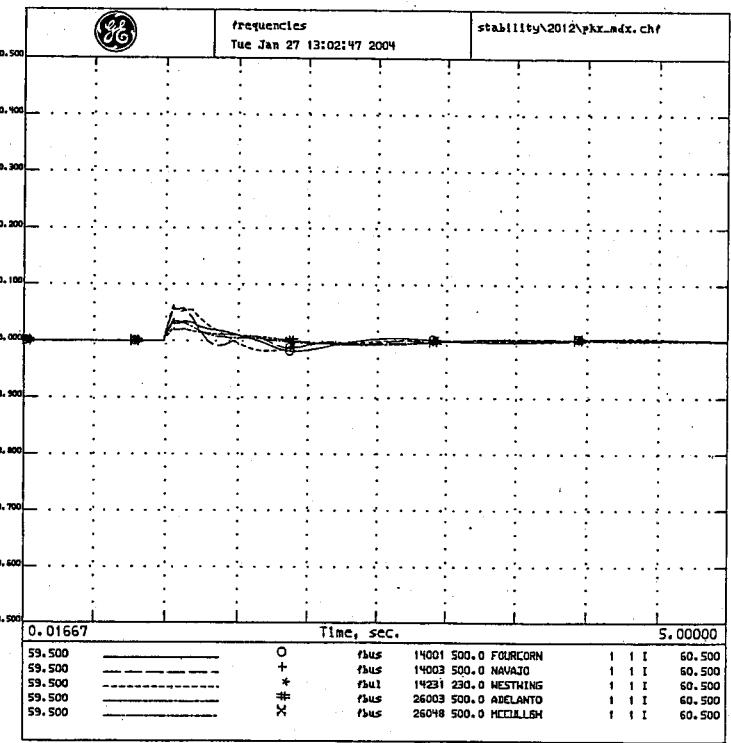
PERKINS FLT PERKINS-MEAD LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
PERK-MEAD STAB: 01/03; T=0 3P FLT PERKS001FLSH CAPS MHP-YAU/YAU-HNG,  
NAV-MHP/HNG;4C CLR FLT W/PERK-MEAD;8C REIN;2012.4y4HSCL.bat

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NOVEMBER 7, 2002 DATA REQUEST.



NS FLT PERKINS-MEAD LINE OUT  
HSIA APPROVED BASE CASE  
MAY 19, 2003  
PERK-MEAD STAB: 01/03; T=0 3P FLT PERKS001FLSH CAPS MHP-YAU/YAU-HNG,  
NAV-MHP/HNG;4C CLR FLT W/PERK-MEAD;8C REIN;2012.4y4HSCL.bat

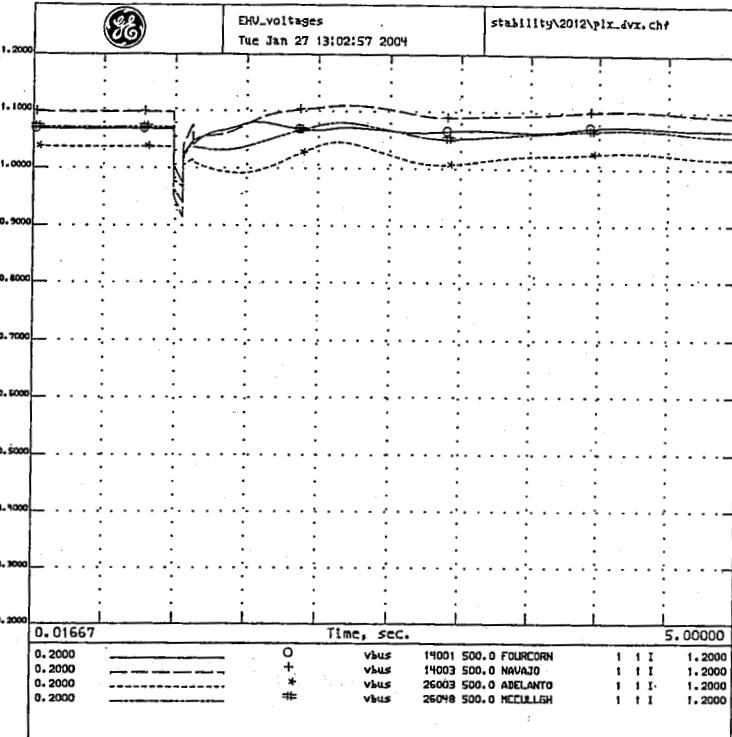
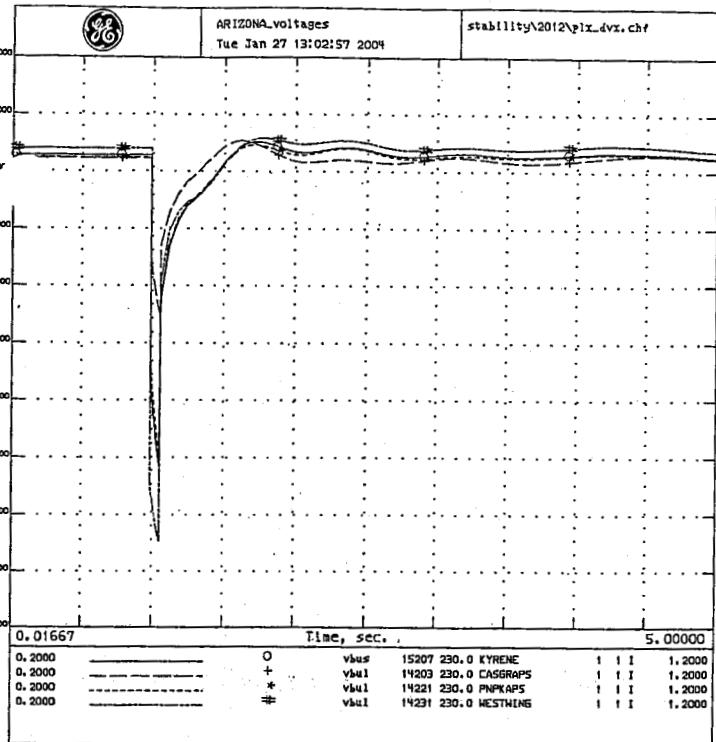
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PERKINS FLT PERKINS-MEAD LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
PERK-MEAD STAB: 01/03; T=0 3P FLT PERKS001FLSH CAPS MHP-YAU/YAU-HNG,  
NAV-MHP/HNG;4C CLR FLT W/PERK-MEAD;8C REIN;2012.4y4HSCL.bat

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NOVEMBER 7, 2002 DATA REQUEST.

C17



WESTERN ELECTRICITY COORDINATING COUNCIL

PV FLT. /&PV - Devers line out

MAY 19, 2003

PV-DEV STAB1 1/03; T=0 3P FLT PUS00;10% FLT IMPING;FLSH CAPS  
NAU-HKP/HKP-YAV,PV-DV/NG14C CLR FLT /&PV-DEVBC REIN\2012.4y4\NSCC.bat

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HOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
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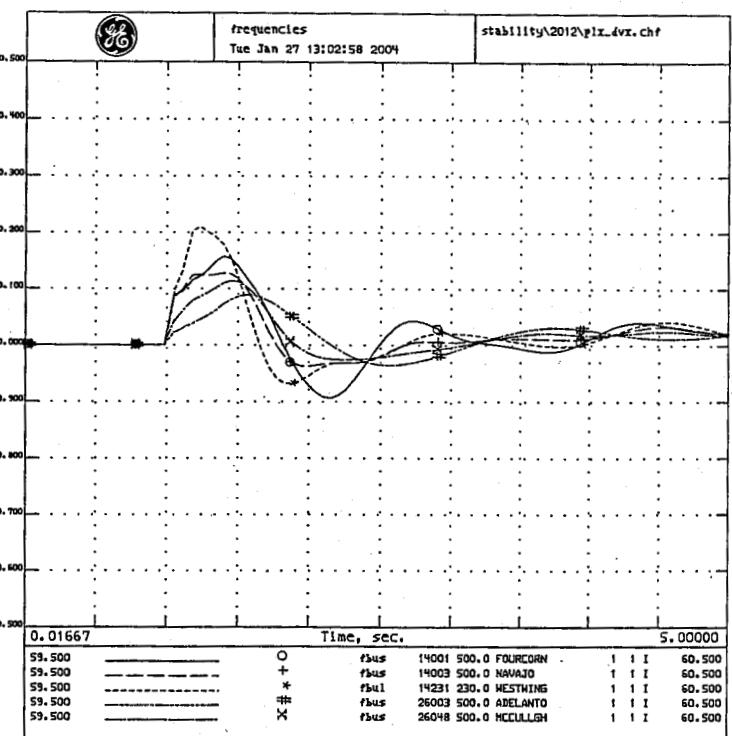
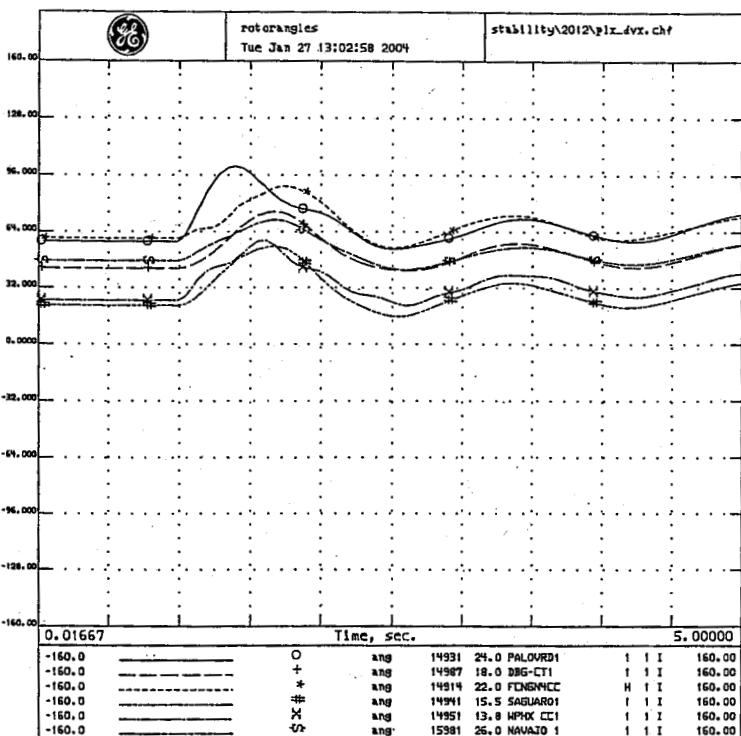
WESTERN ELECTRICITY COORDINATING COUNCIL

PV FLT. /&PV - Devers line out

MAY 19, 2003

PV-DEV STAB1 1/03; T=0 3P FLT PUS00;10% FLT IMPING;FLSH CAPS  
NAU-HKP/HKP-YAV,PV-DV/NG14C CLR FLT /&PV-DEVBC REIN\2012.4y4\NSCC.bat

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WESTERN ELECTRICITY COORDINATING COUNCIL

PV FLT. /&PV - Devers line out

MAY 19, 2003

PV-DEV STAB1 1/03; T=0 3P FLT PUS00;10% FLT IMPING;FLSH CAPS  
NAU-HKP/HKP-YAV,PV-DV/NG14C CLR FLT /&PV-DEVBC REIN\2012.4y4\NSCC.bat

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WESTERN ELECTRICITY COORDINATING COUNCIL

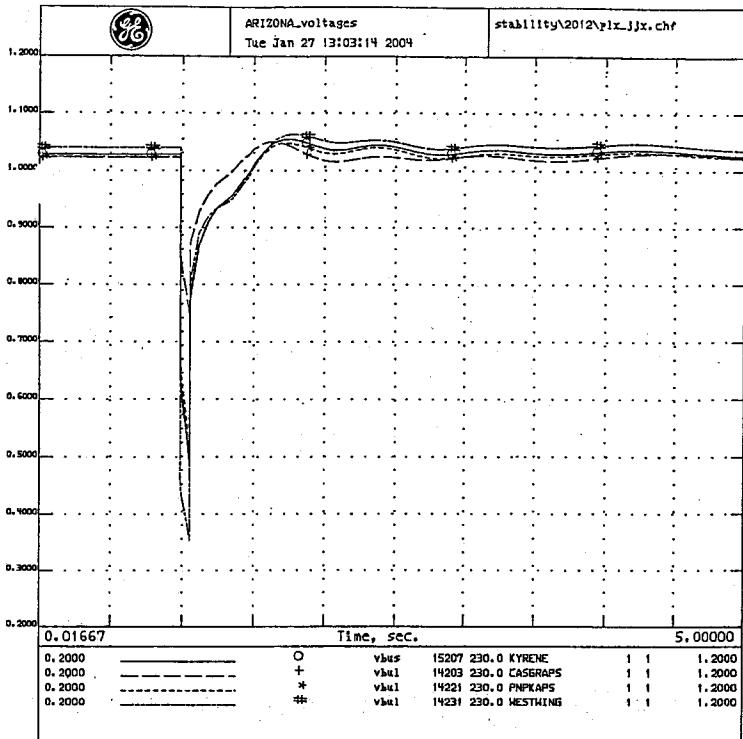
PV FLT. /&PV - Devers line out

MAY 19, 2003

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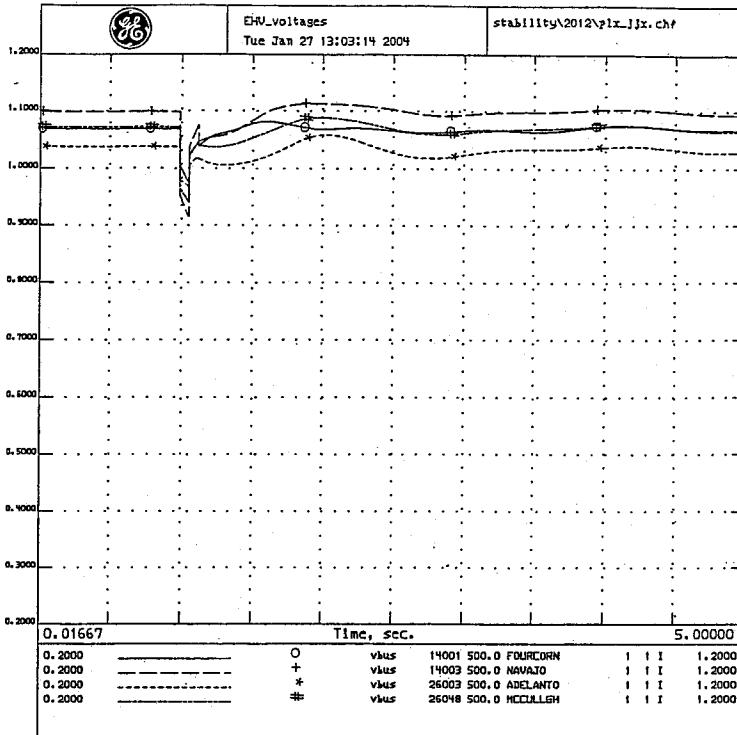
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C18



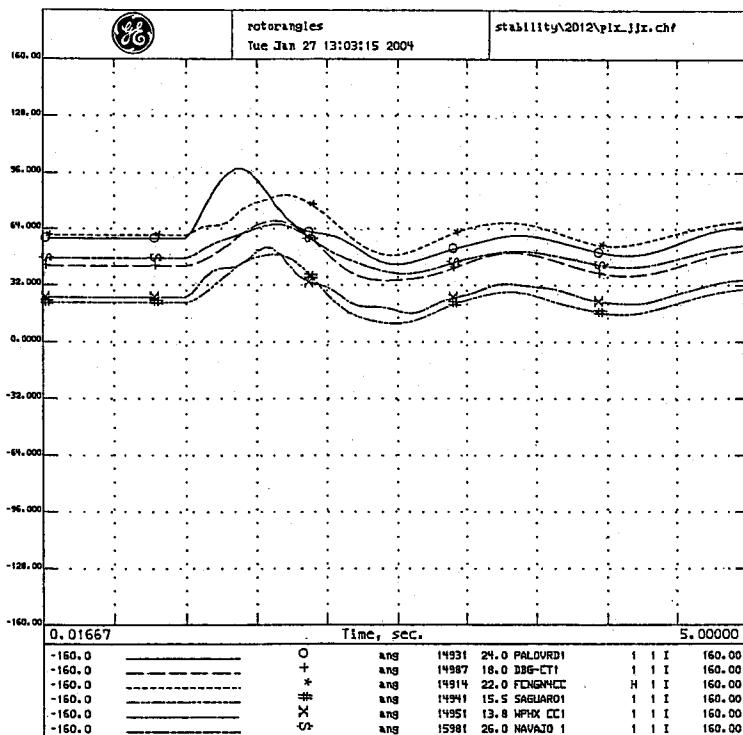
PALO VERDE FLT HASSY-JOJOBA LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
HAS-JJ STAB +1 01/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG/4C CLR FLT W/HAS-JJ;BC REIN|2012.4y4;NSCC.bpt

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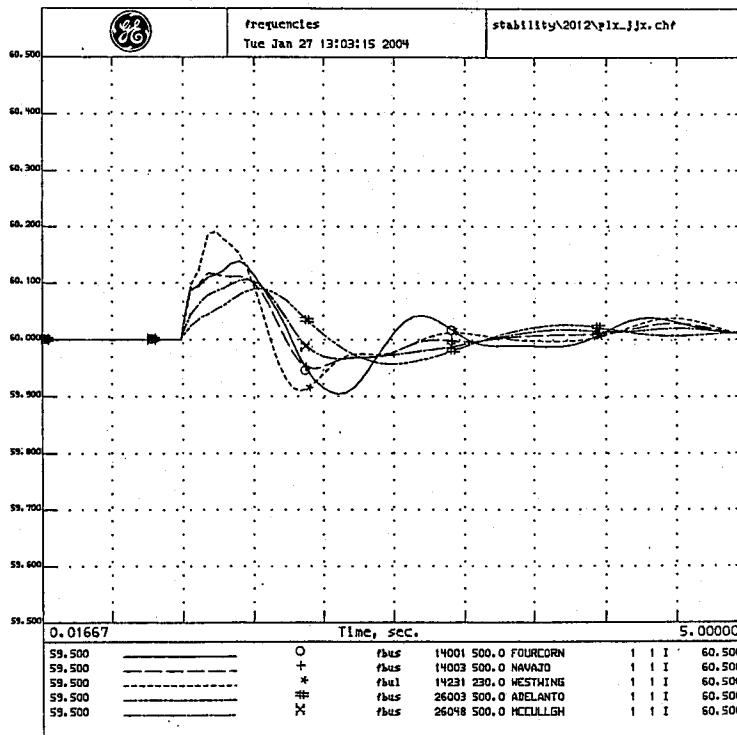
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
HAS-JJ STAB +1 01/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG/4C CLR FLT W/HAS-JJ;BC REIN|2012.4y4;NSCC.bpt

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VERDE FLT HASSY-JOJOBA LINE OUT  
HSIA APPROVED BASE CASE  
MAY 19, 2003  
HAS-JJ STAB +1 01/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG/4C CLR FLT W/HAS-JJ;BC REIN|2012.4y4;NSCC.bpt

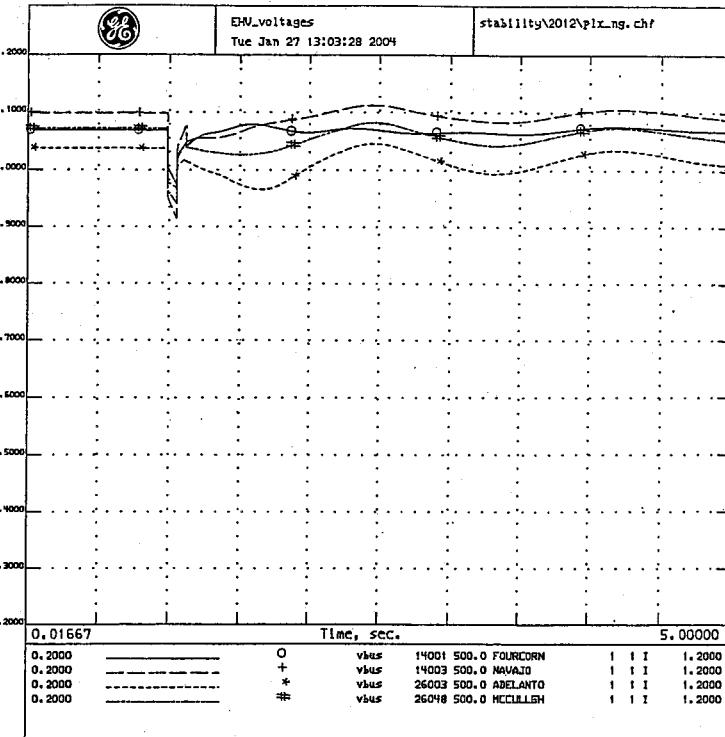
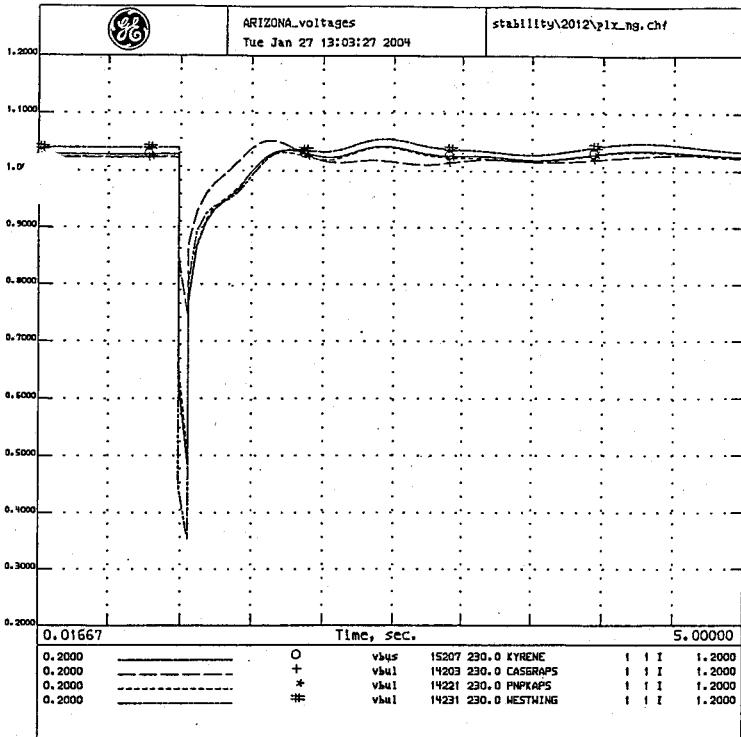
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PALO VERDE FLT HASSY-JOJOBA LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
HAS-JJ STAB +1 01/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-DV/NG/4C CLR FLT W/HAS-JJ;BC REIN|2012.4y4;NSCC.bpt

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C19

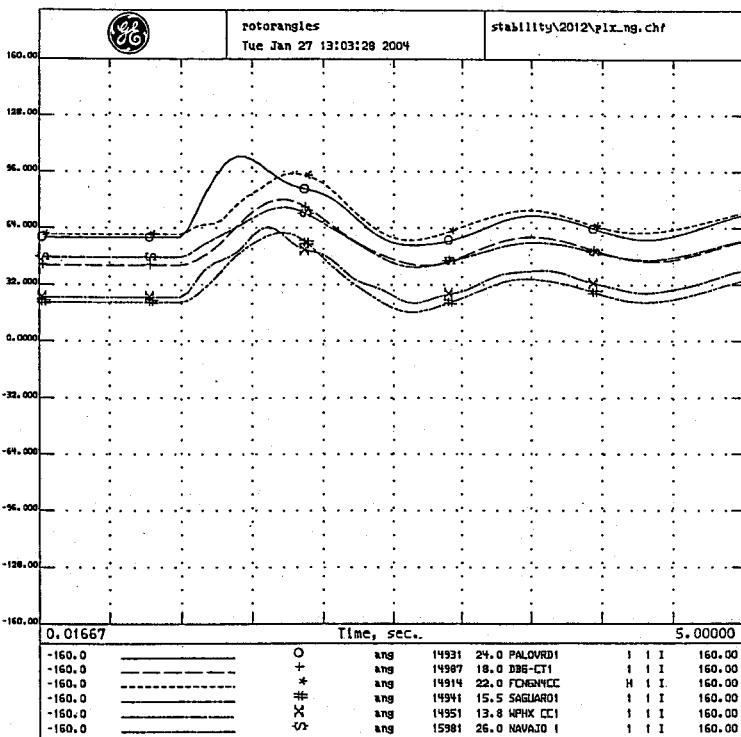


WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. w/HASSY-N.GILA line out  
MAY 19, 2003  
PV-NGILA STAB: 1/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-NG;BC REIN|2012.d4|WSCC.bat

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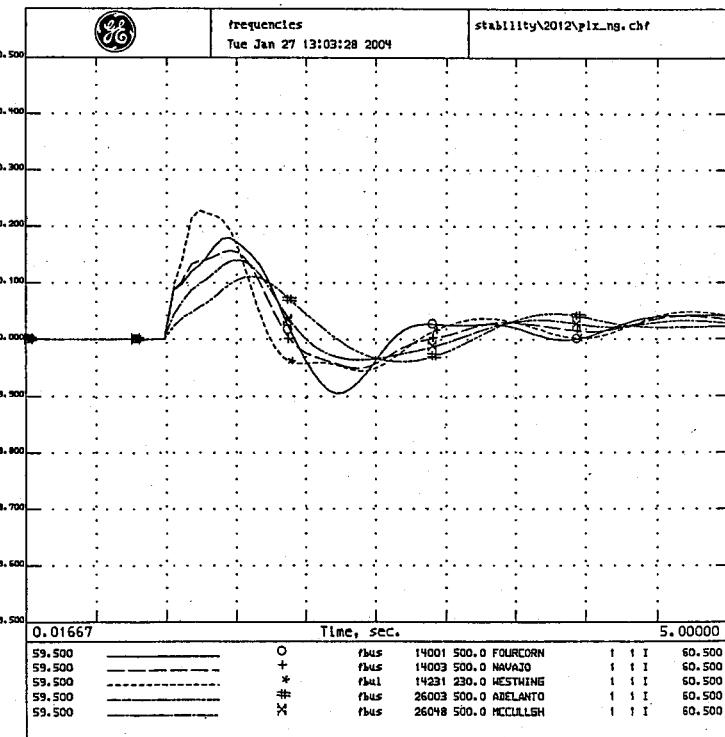
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PV FLT. w/HASSY-N.GILA line out  
MAY 19, 2003  
PV-NGILA STAB: 1/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-NG;BC REIN|2012.d4|WSCC.bat

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WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. w/HASSY-N.GILA line out  
MAY 19, 2003  
PV-NGILA STAB: 1/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
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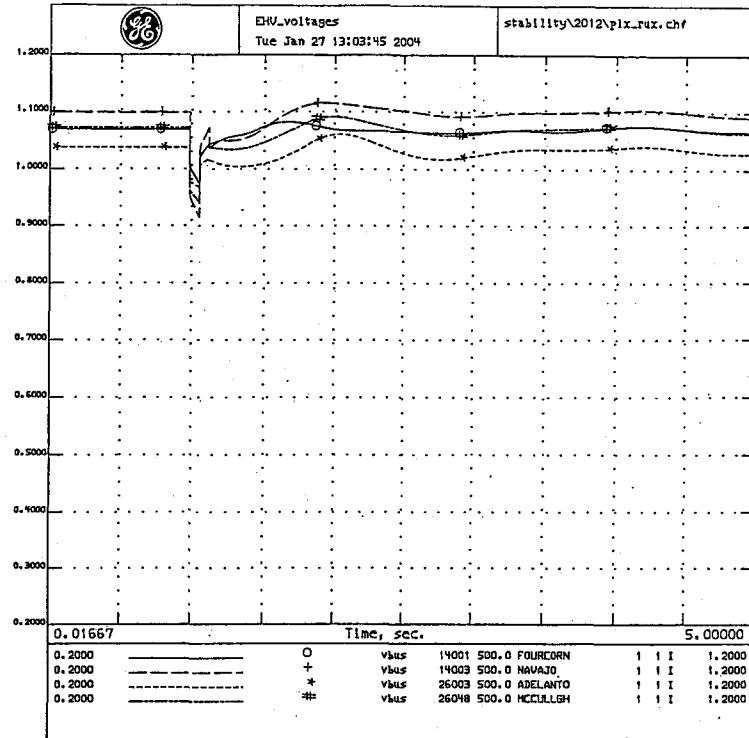
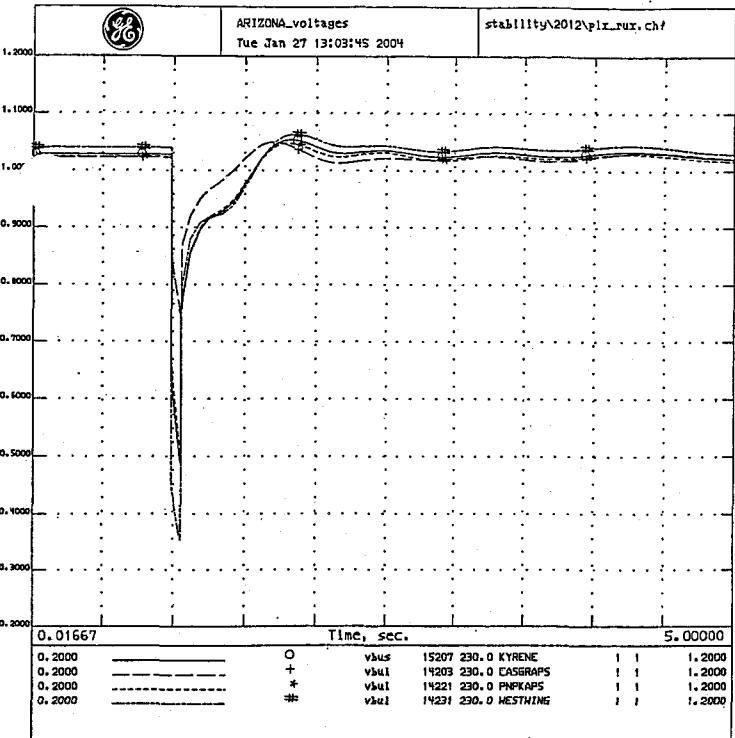
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WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT. w/HASSY-N.GILA line out  
MAY 19, 2003  
PV-NGILA STAB: 1/03; T=0 3P FLT PV500;10% FLT IMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-NG;BC REIN|2012.d4|WSCC.bat

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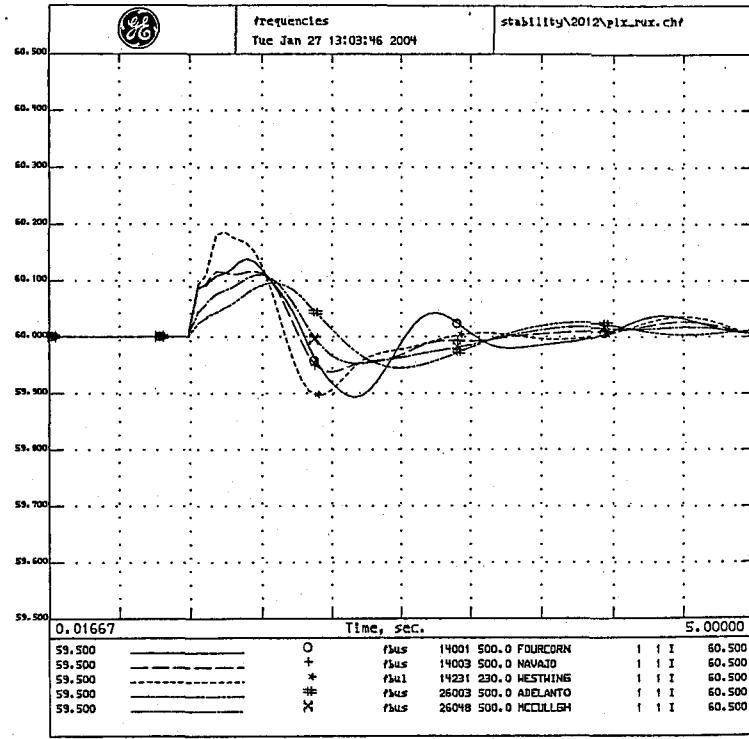
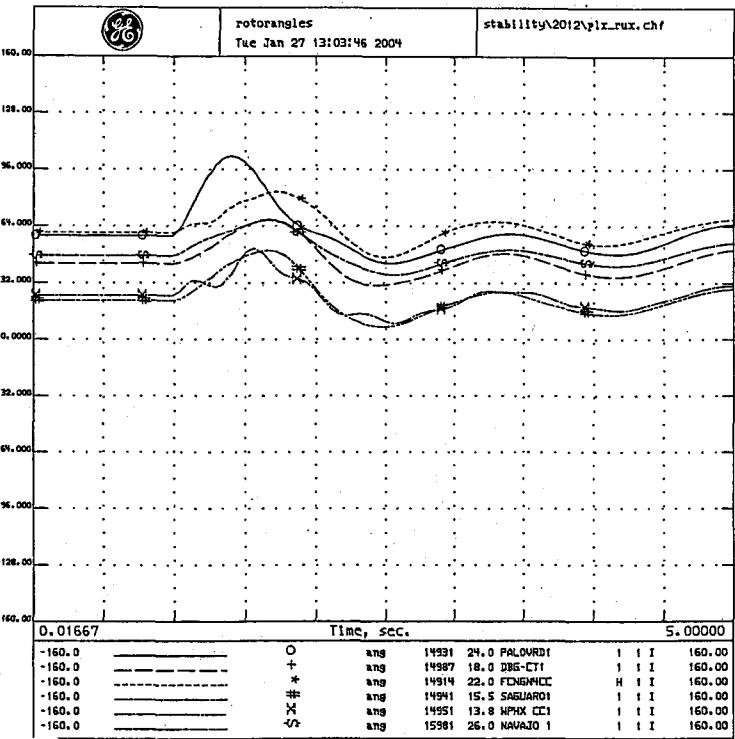


PALO VERDE FLT PU-RUDD LINE OUT  
2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
PV-RUDD STAB #1 01/03; T=0 3P FLT PV500;10% FLT DMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-JV/NG/4C CLR FLT W/PV-RD;BC REIN|2012.4y4|HSCC.bpt

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2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
PV-RUDD STAB #1 01/03; T=0 3P FLT PV500;10% FLT DMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-JV/NG/4C CLR FLT W/PV-RD;BC REIN|2012.4y4|HSCC.bpt

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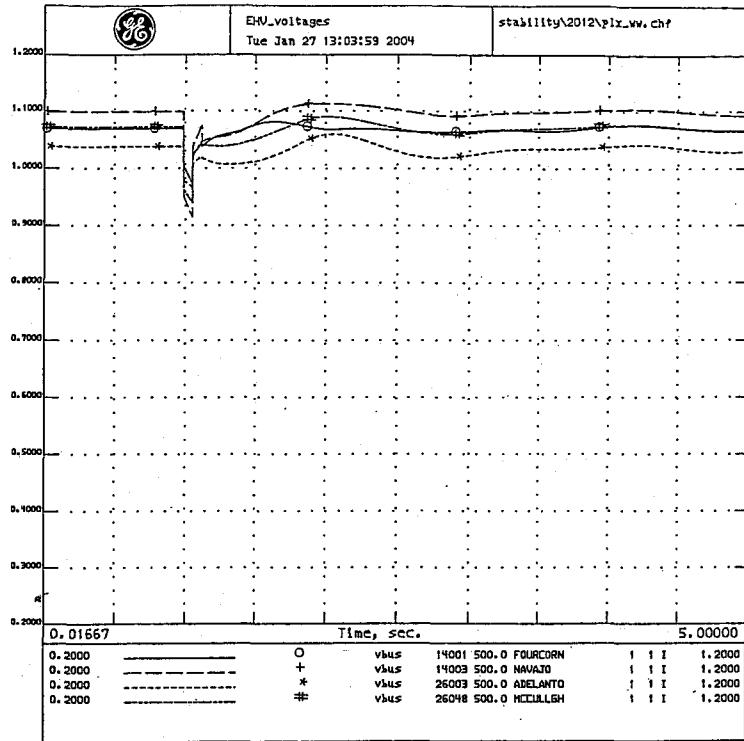
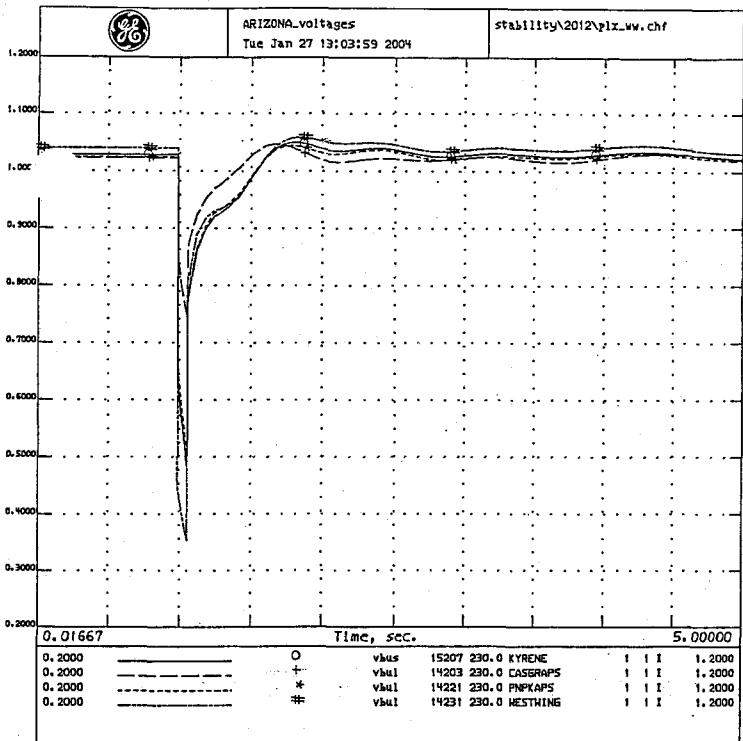
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2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
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PALO VERDE FLT PU-RUDD LINE OUT  
2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
PV-RUDD STAB #1 01/03; T=0 3P FLT PV500;10% FLT DMPING;FLSH CAPS  
NAV-HKP/HKP-YAV,PV-JV/NG/4C CLR FLT W/PV-RD;BC REIN|2012.4y4|HSCC.bpt

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C21

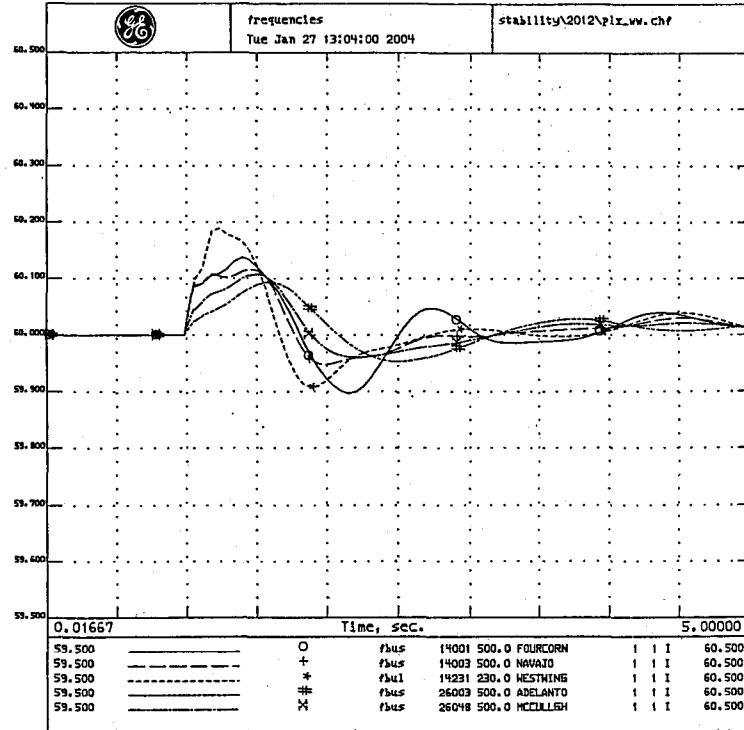
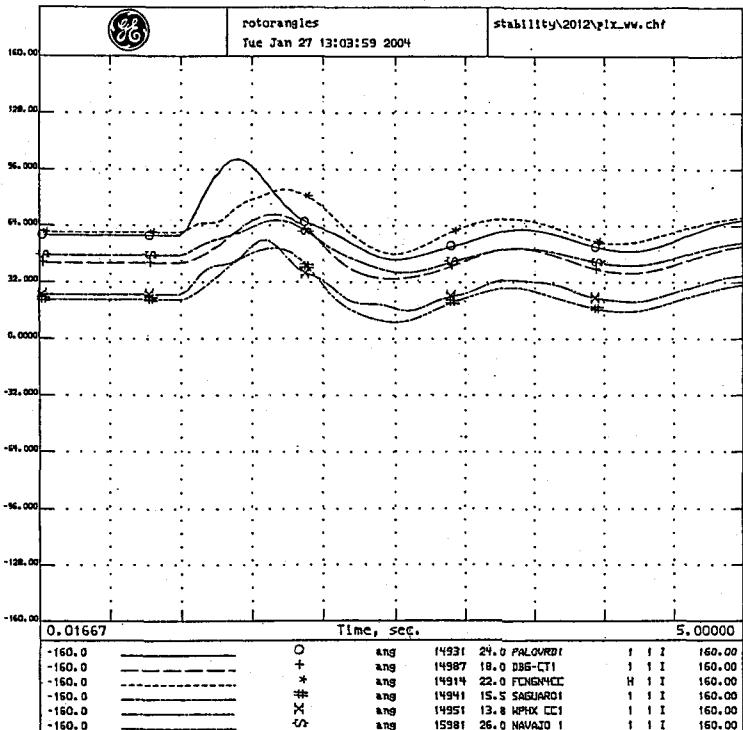


WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT w/PV-WH line out  
MAY 19, 2003  
PV-HWG STAB1 1/03; T=0 3P FLT PV500;10X FLT DMPNG;FLSH CAPS  
NAU-HKP/HKP-YAV,PV-DV/NG14C CLR FLT W/PV-WH;BC REIN\2012.dg4\WSCC.bat

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PV FLT w/PV-WH line out  
MAY 19, 2003  
PV-HWG STAB1 1/03; T=0 3P FLT PV500;10X FLT DMPNG;FLSH CAPS  
NAU-HKP/HKP-YAV,PV-DV/NG14C CLR FLT W/PV-WH;BC REIN\2012.dg4\WSCC.bat

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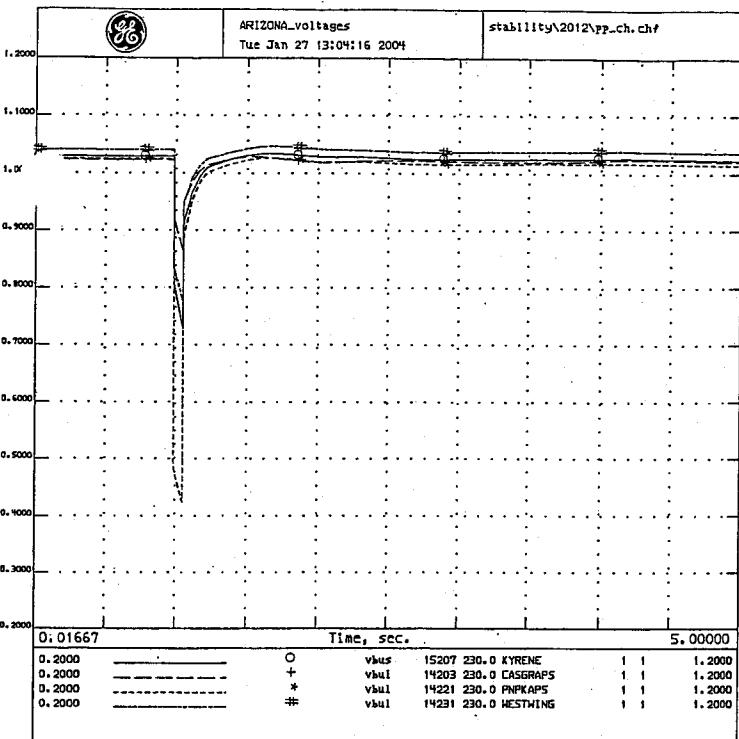
WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT w/PV-WH line out  
MAY 19, 2003  
PV-HWG STAB1 1/03; T=0 3P FLT PV500;10X FLT DMPNG;FLSH CAPS  
NAU-HKP/HKP-YAV,PV-DV/NG14C CLR FLT W/PV-WH;BC REIN\2012.dg4\WSCC.bat

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WESTERN ELECTRICITY COORDINATING COUNCIL  
PV FLT w/PV-WH line out  
MAY 19, 2003  
PV-HWG STAB1 1/03; T=0 3P FLT PV500;10X FLT DMPNG;FLSH CAPS  
NAU-HKP/HKP-YAV,PV-DV/NG14C CLR FLT W/PV-WH;BC REIN\2012.dg4\WSCC.bat

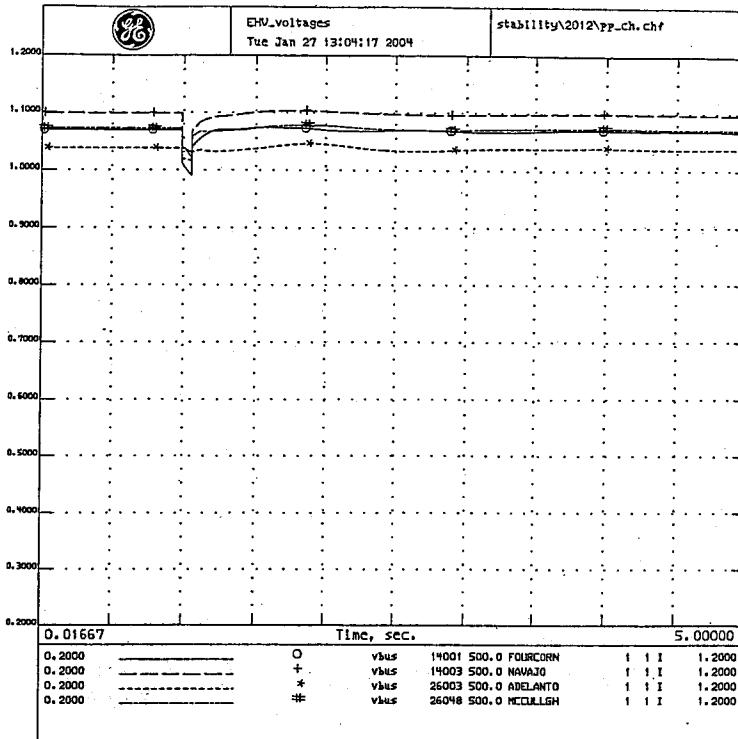
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C22



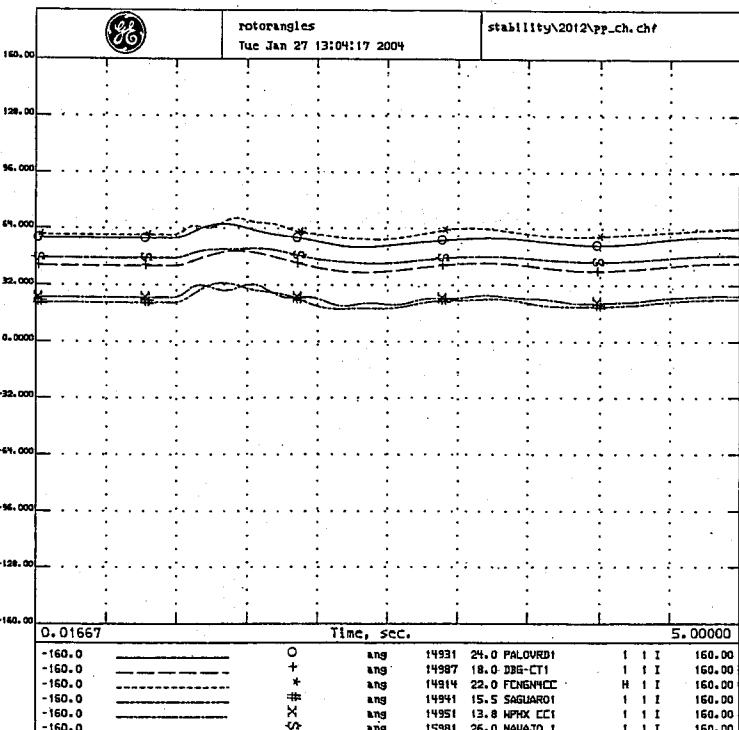
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
PP-CH STAB +1; 01/03; T=0 3P FLT PP345;  
4C CLR FLT W/PP-CH 2012. dyd\HSCC.bpt

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NOVEMBER 7, 2002 DATA REQUEST.



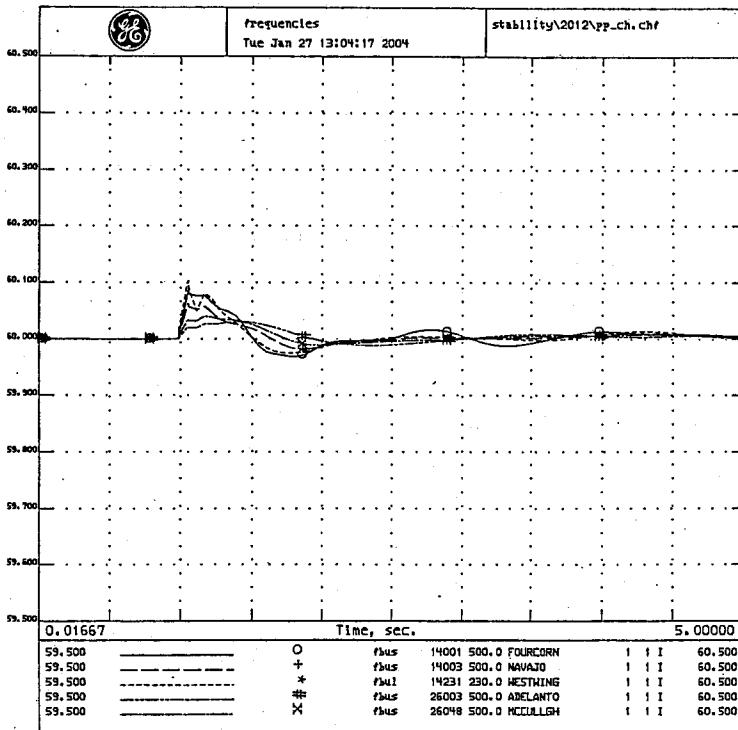
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
PP-CH STAB +1; 01/03; T=0 3P FLT PP345;  
4C CLR FLT W/PP-CH 2012. dyd\HSCC.bpt

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
CONTAINS THE NEW GOVERNOR MODELING RECEIVED IN RESPONSE TO THE  
NOVEMBER 7, 2002 DATA REQUEST.



X 345KV FLT PP-CH LINE OUT  
.12 HSIA APPROVED BASE CASE  
MAY 19, 2003  
PP-CH STAB +1; 01/03; T=0 3P FLT PP345;  
4C CLR FLT W/PP-CH 2012. dyd\HSCC.bpt

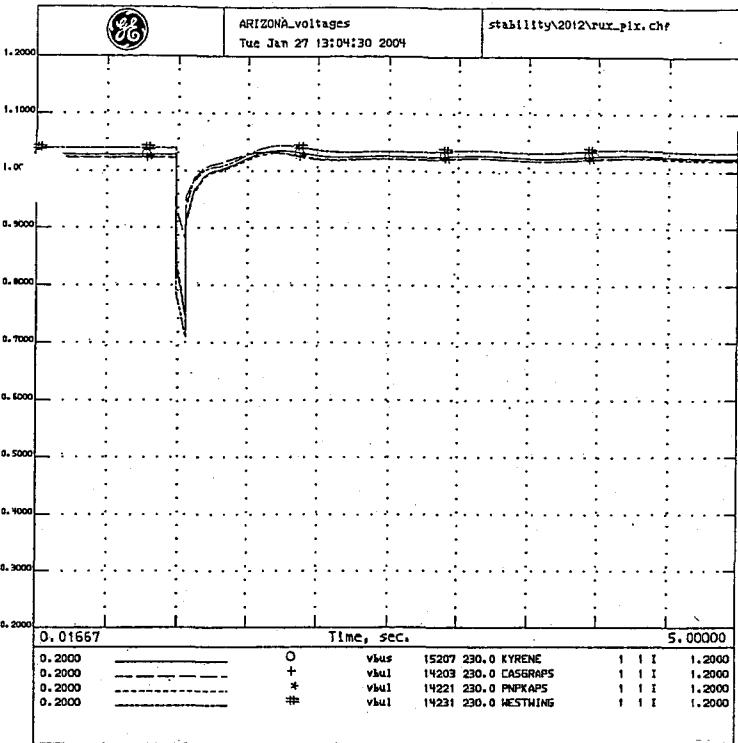
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PNPK 345KV FLT PP-CH LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
PP-CH STAB +1; 01/03; T=0 3P FLT PP345;  
4C CLR FLT W/PP-CH 2012. dyd\HSCC.bpt

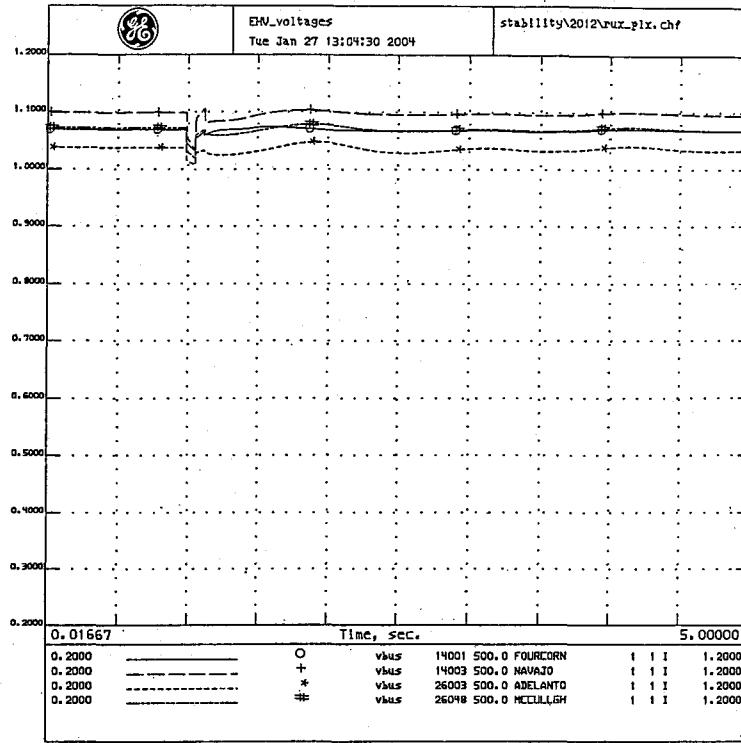
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NOVEMBER 7, 2002 DATA REQUEST.

C23



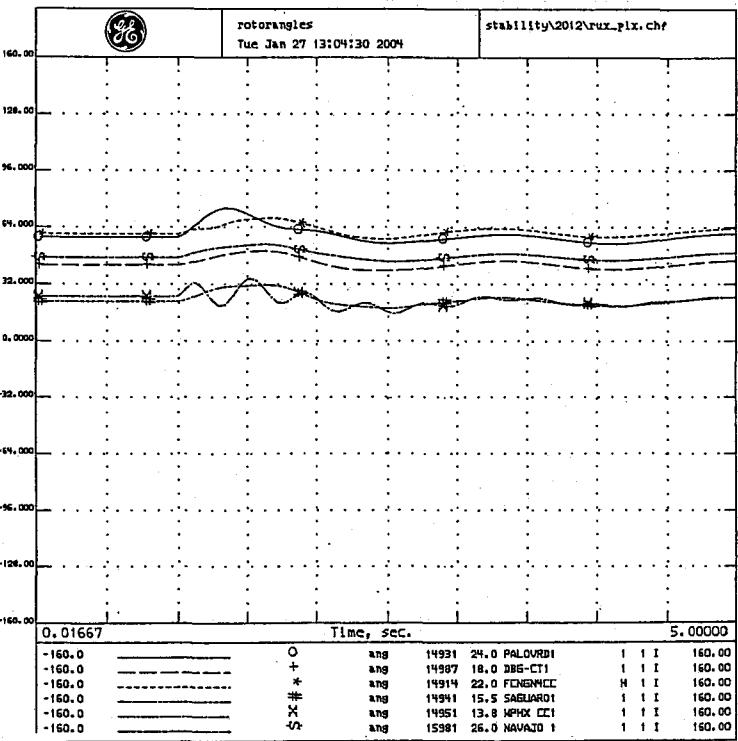
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2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT RUDD500;10% FLT DMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-RUDD;8C REIN[2012, 4y4]NSCC.bpt

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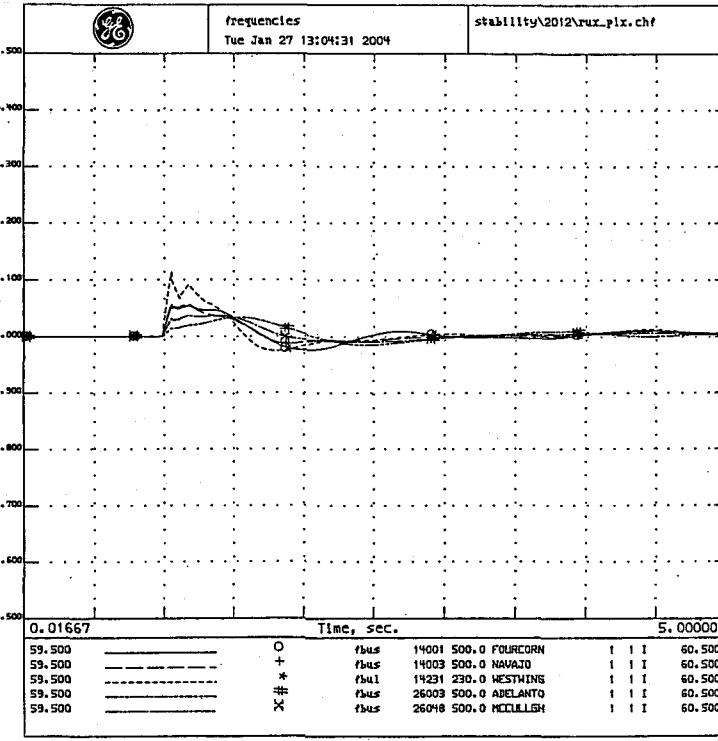
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2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT RUDD500;10% FLT DMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-RUDD;8C REIN[2012, 4y4]NSCC.bpt

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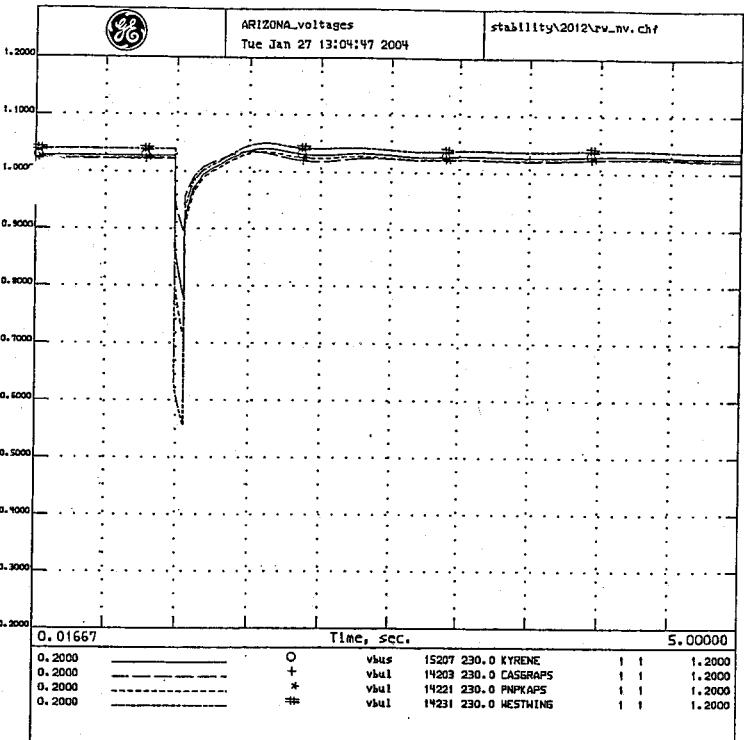
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2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
PV-RUDD STAB +1; 01/03; T=0 3P FLT RUDD500;10% FLT DMPING;FLSH CAPS  
NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-RUDD;8C REIN[2012, 4y4]NSCC.bpt

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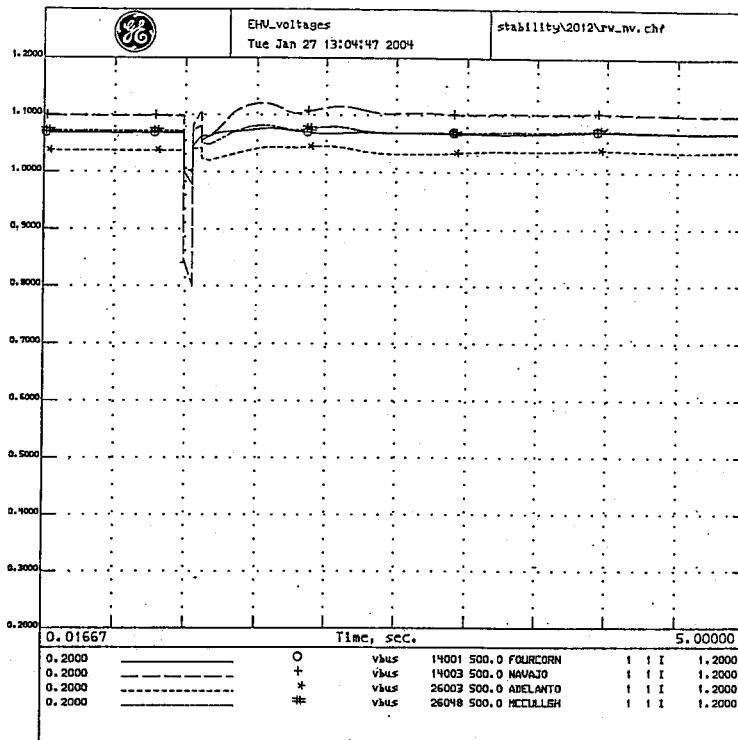
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2012 HS1A APPROVED BASE CASE  
MAY 19, 2003  
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NAV-MKP/MKP-YAV,PV-DV/NG/4C CLR FLT W/PV-RUDD;8C REIN[2012, 4y4]NSCC.bpt

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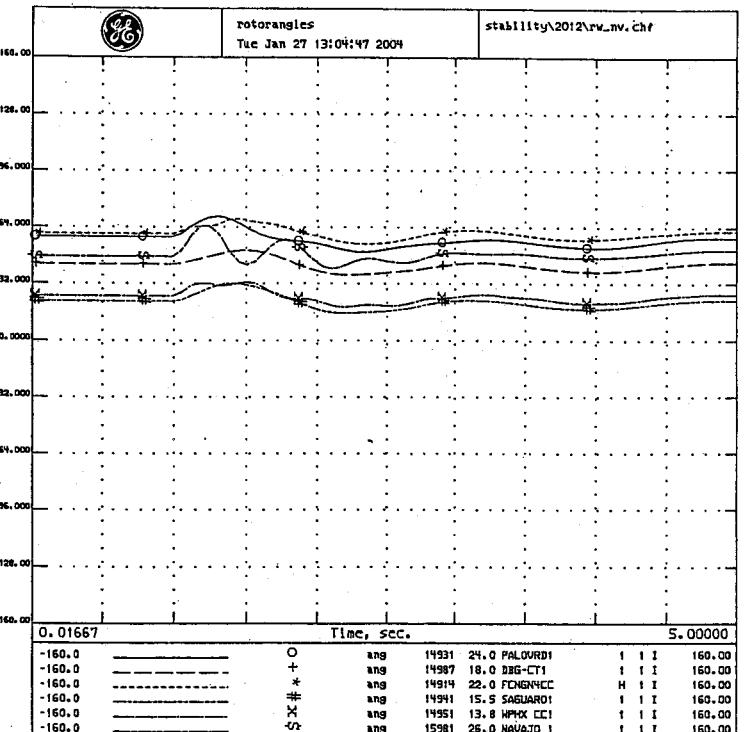
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
RHY-NAV STAB: 1/03; T=0 3P FLT RHY500; 6% FLT DIMPING; FLSH CAPS  
NAV-MCC/MKP, MKP-ELD)4C CLR FLT W/RHY-NAV\BC REIN\2012.dyd\HSCC.bat

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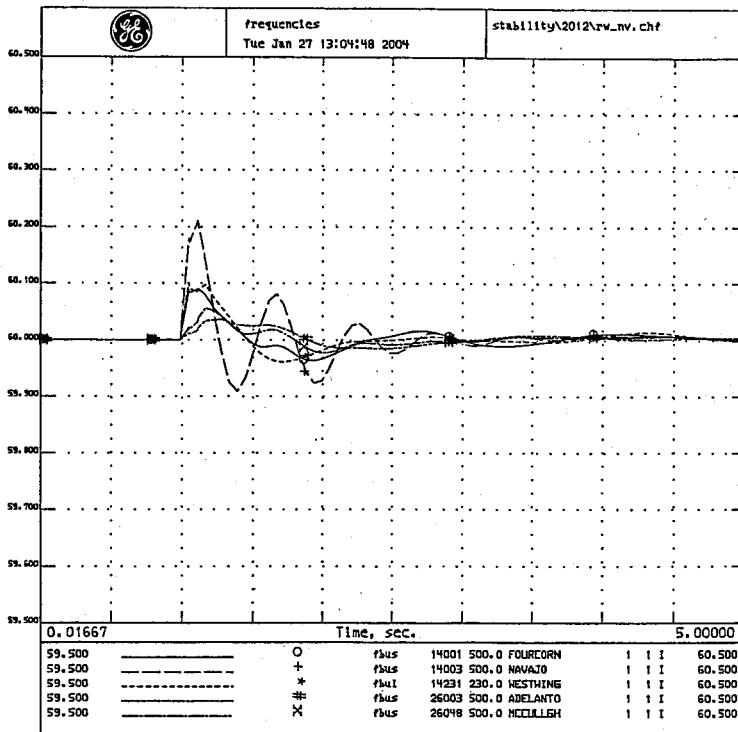
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
RHY-NAV STAB: 1/03; T=0 3P FLT RHY500; 6% FLT DIMPING; FLSH CAPS  
NAV-MCC/MKP, MKP-ELD)4C CLR FLT W/RHY-NAV\BC REIN\2012.dyd\HSCC.bat

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NOVEMBER 7, 2002 DATA REQUEST.



LT RH-NAV LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
RHY-NAV STAB: 1/03; T=0 3P FLT RHY500; 6% FLT DIMPING; FLSH CAPS  
NAV-MCC/MKP, MKP-ELD)4C CLR FLT W/RHY-NAV\BC REIN\2012.dyd\HSCC.bat

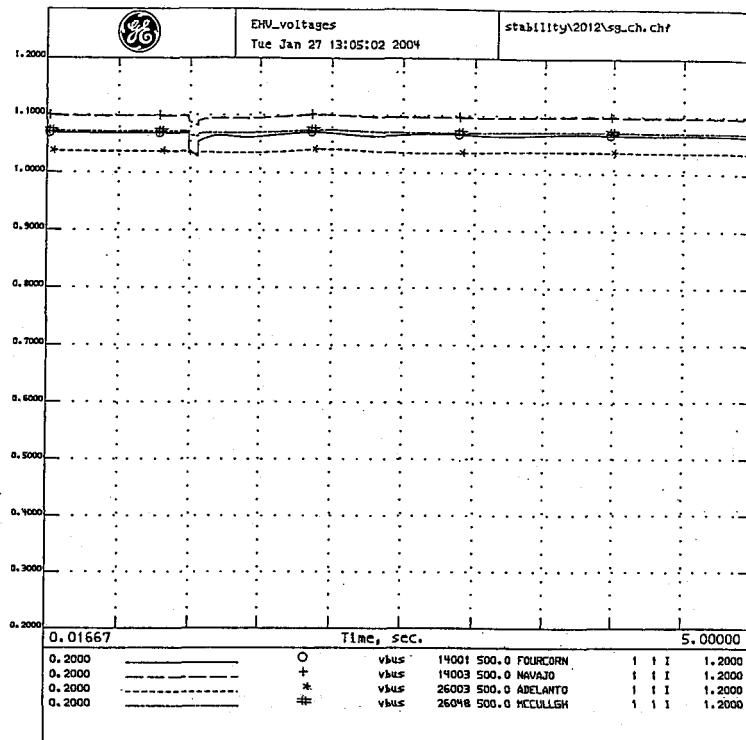
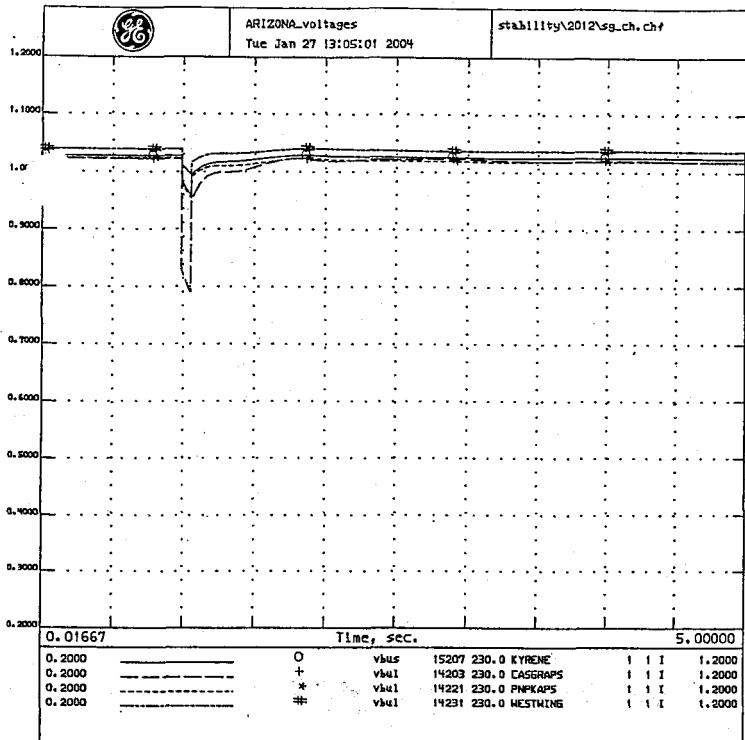
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RHY FLT RH-NAV LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
RHY-NAV STAB: 1/03; T=0 3P FLT RHY500; 6% FLT DIMPING; FLSH CAPS  
NAV-MCC/MKP, MKP-ELD)4C CLR FLT W/RHY-NAV\BC REIN\2012.dyd\HSCC.bat

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NOVEMBER 7, 2002 DATA REQUEST.

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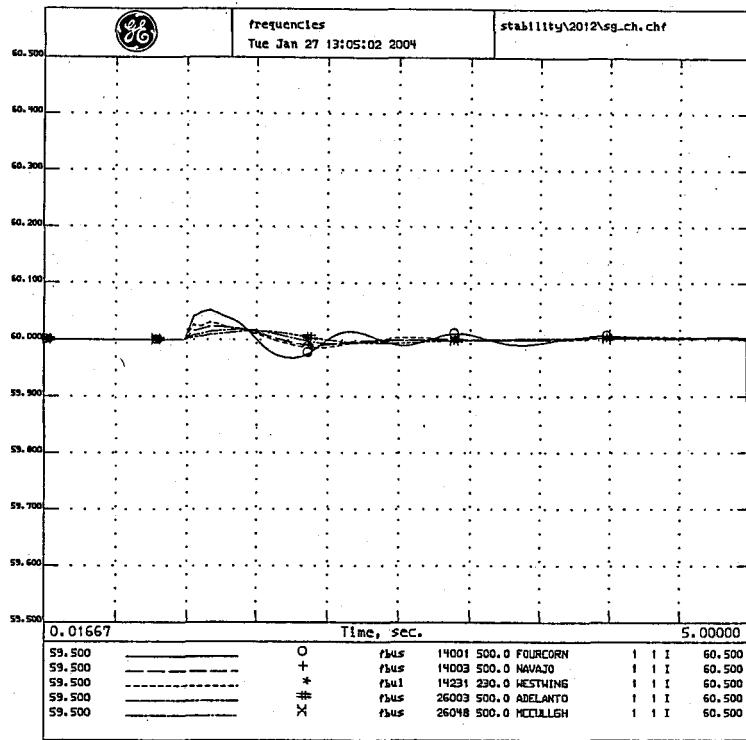
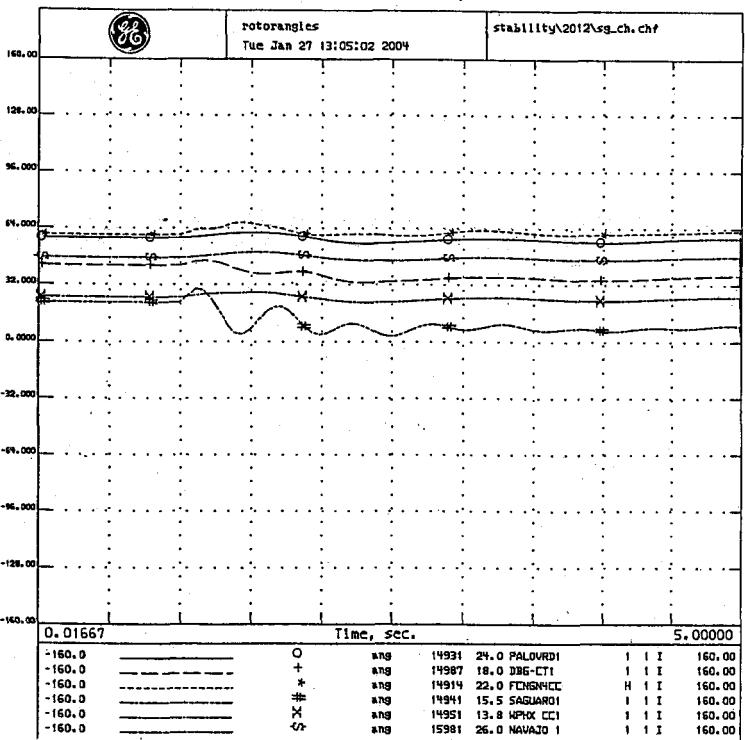


SAGUARO FLT SAG-CH LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
SAG-CH STAB #1 01/03; T=0 3P FLT SAG500;  
4C CLR FLT W/SAG-CH\2012.4y4\NSCC.bpt

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SAGUARO FLT SAG-CH LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
SAG-CH STAB #1 01/03; T=0 3P FLT SAG500;  
4C CLR FLT W/SAG-CH\2012.4y4\NSCC.bpt

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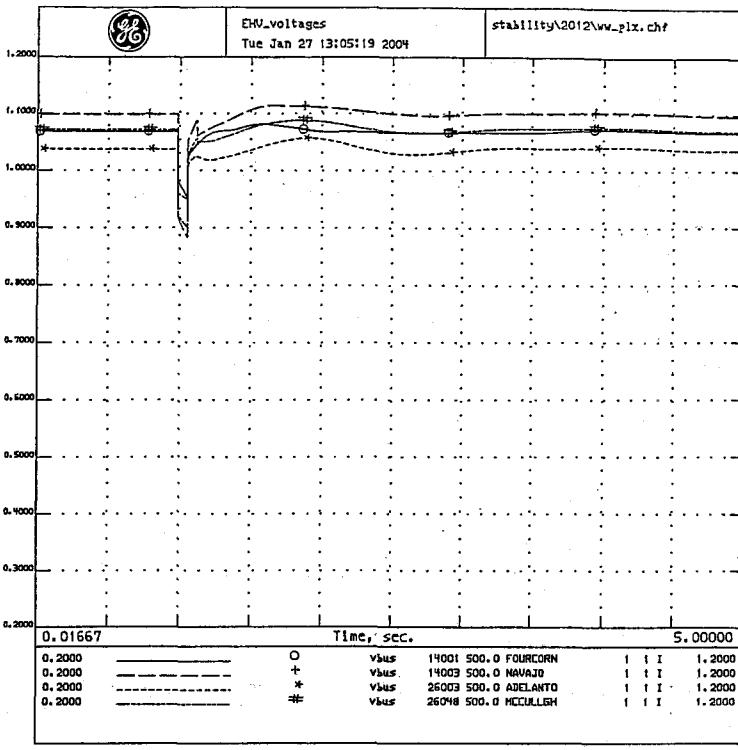
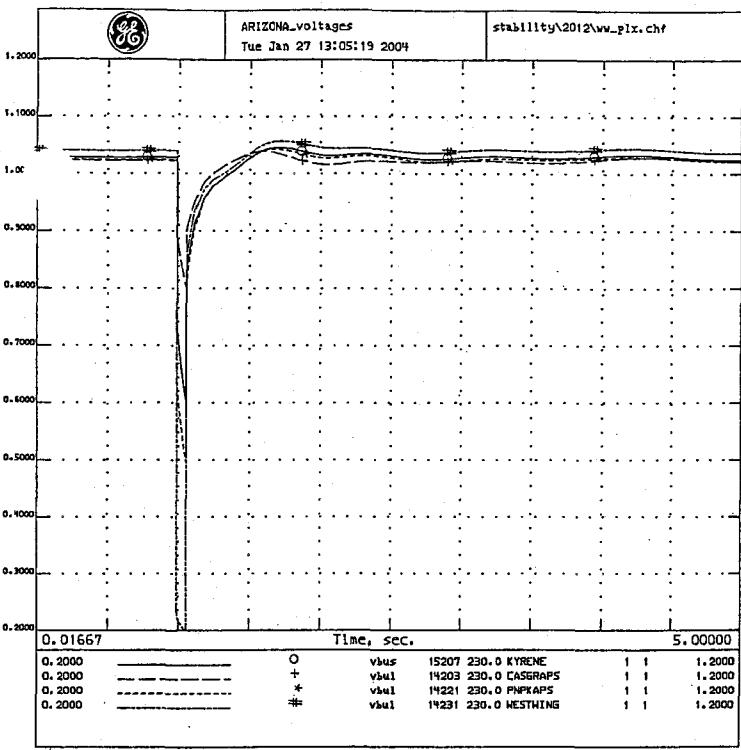
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2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
SAG-CH STAB #1 01/03; T=0 3P FLT SAG500;  
4C CLR FLT W/SAG-CH\2012.4y4\NSCC.bpt

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IARO FLT SAG-CH LINE OUT  
2012 HSIA APPROVED BASE CASE  
MAY 19, 2003  
SAG-CH STAB #1 01/03; T=0 3P FLT SAG500;  
4C CLR FLT W/SAG-CH\2012.4y4\NSCC.bpt

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C26

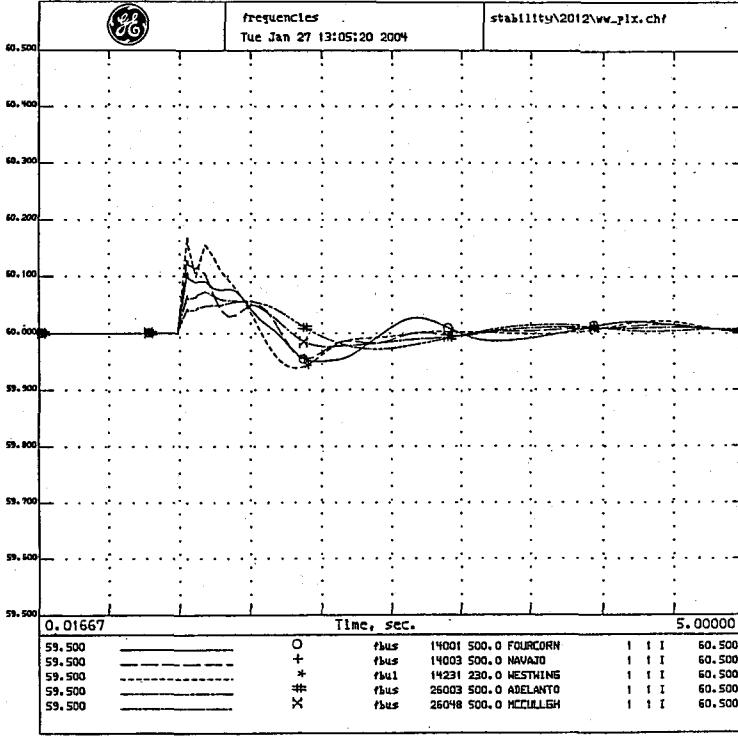
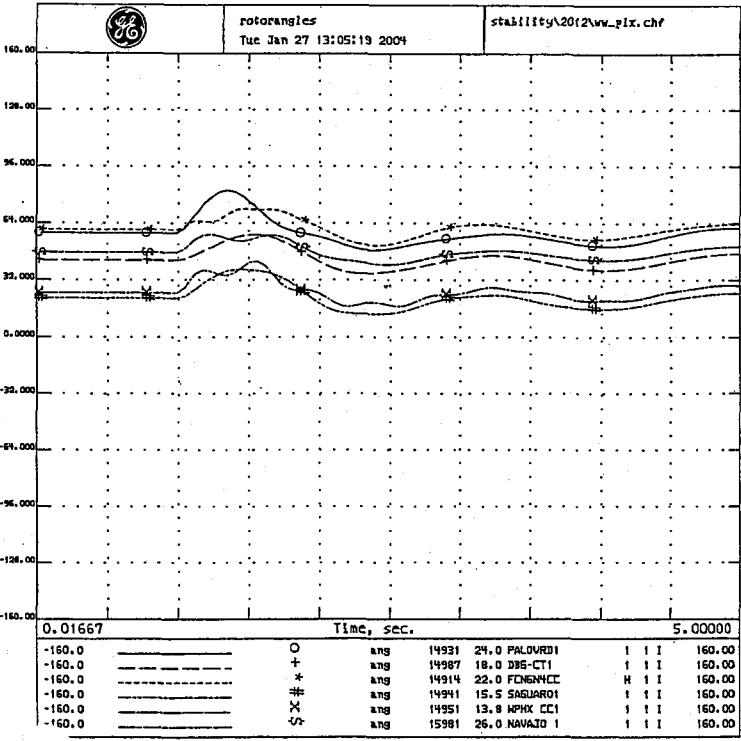


WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW\_PU line out  
MAY 19, 2003  
KMG-YAV STAB; 1/03; T=0 3P FLT KMG500;FLSH CAPS MKP-YAV/YAV-KMG,  
NAV-MKP/HNG;4C CLR FLT W/HNG-PAL;8C REIN|2012.4y4 HSCC.bat

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WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW\_PU line out  
MAY 19, 2003  
KMG-YAV STAB; 1/03; T=0 3P FLT KMG500;FLSH CAPS MKP-YAV/YAV-KMG,  
NAV-MKP/HNG;4C CLR FLT W/HNG-PAL;8C REIN|2012.4y4 HSCC.bat

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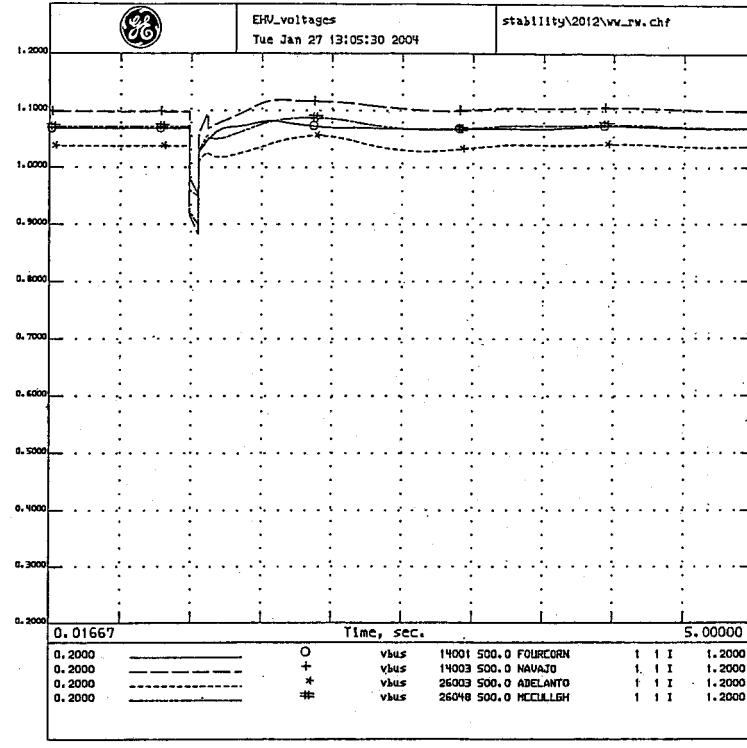
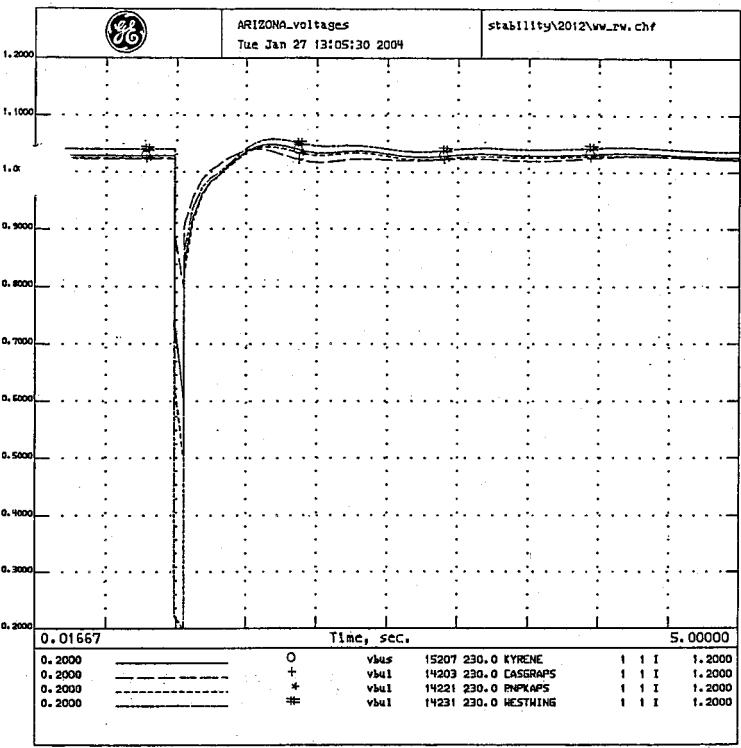


WESTERN ELECTRICITY COORDINATING COUNCIL  
WW\_FLT\_WW\_PU line out  
MAY 19, 2003  
KMG-YAV STAB; 1/03; T=0 3P FLT KMG500;FLSH CAPS MKP-YAV/YAV-KMG,  
NAV-MKP/HNG;4C CLR FLT W/HNG-PAL;8C REIN|2012.4y4 HSCC.bat

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MAY 19, 2003  
KMG-YAV STAB; 1/03; T=0 3P FLT KMG500;FLSH CAPS MKP-YAV/YAV-KMG,  
NAV-MKP/HNG;4C CLR FLT W/HNG-PAL;8C REIN|2012.4y4 HSCC.bat

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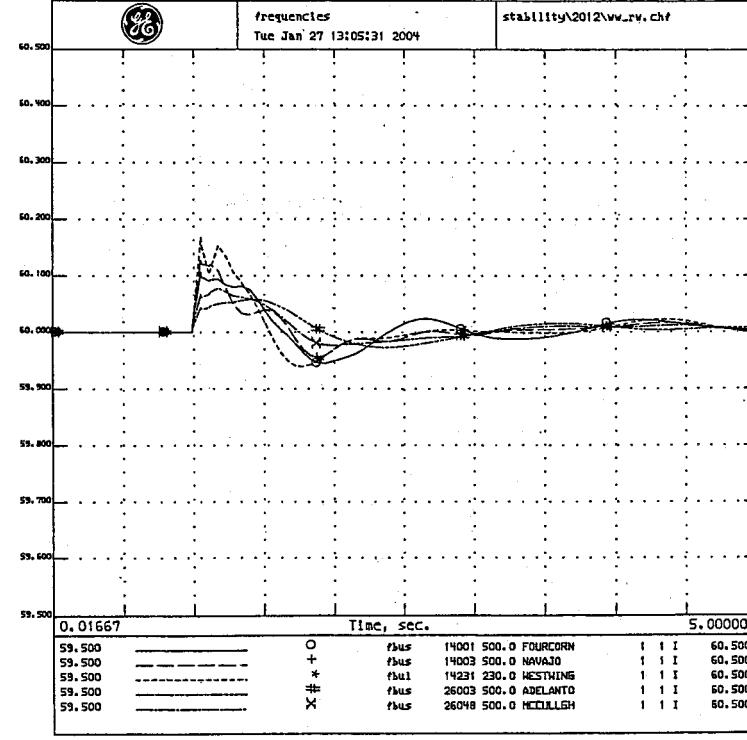
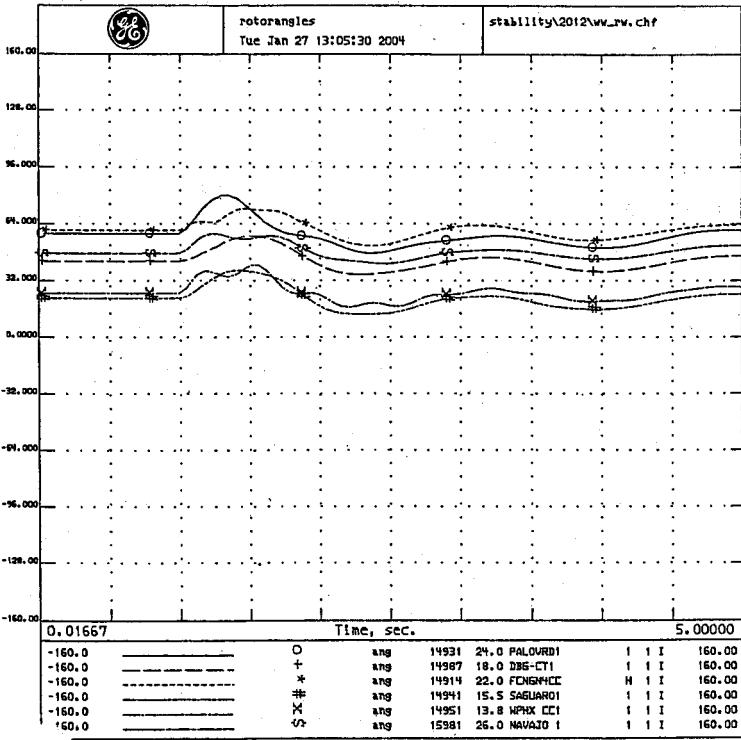


WESTERN ELECTRICITY COORDINATING COUNCIL  
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NAV-HKP/HNG;YC CLR FLT W/HNG-RHY;BC REIN;2012,4y4 HSCC.bat

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WW, FLT, WW-RWY line out  
MAY 19, 2003  
HNG-RW STAB; 1/03; T=0 3P FLT HNG500;FLSH CAPS MKP-YAU/YAU-HNG,  
NAV-HKP/HNG;YC CLR FLT W/HNG-RHY;BC REIN;2012,4y4 HSCC.bat

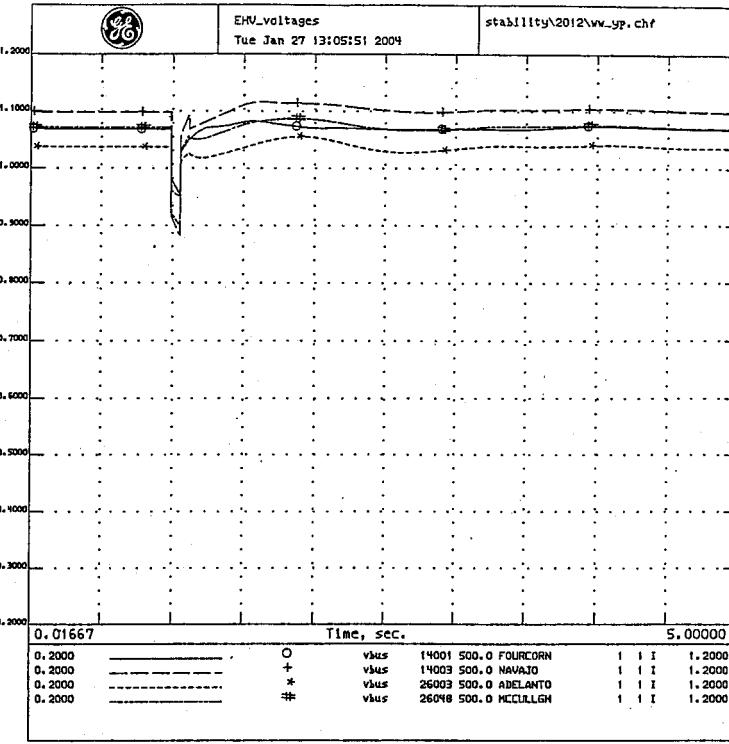
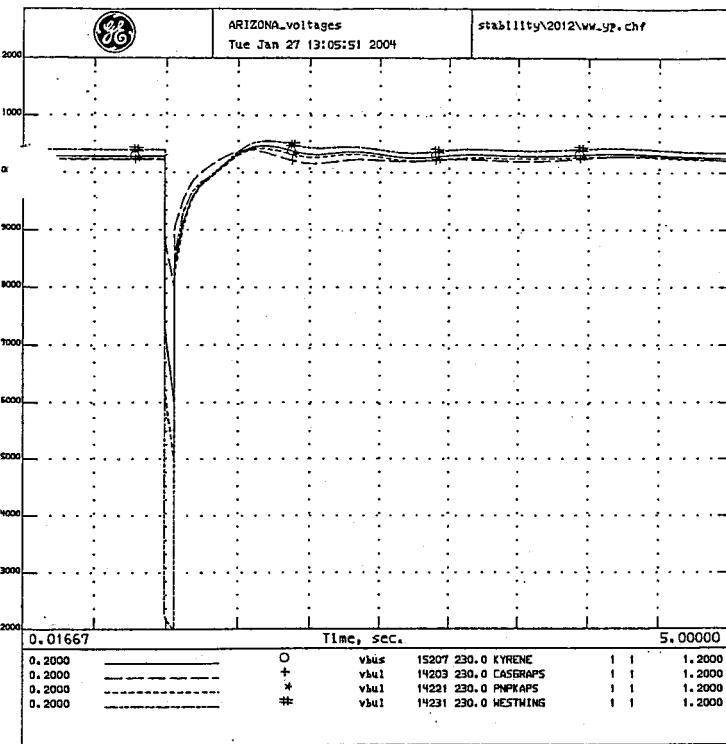
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WW, FLT, WW-RWY line out  
MAY 19, 2003  
HNG-RW STAB; 1/03; T=0 3P FLT HNG500;FLSH CAPS MKP-YAU/YAU-HNG,  
NAV-HKP/HNG;YC CLR FLT W/HNG-RHY;BC REIN;2012,4y4 HSCC.bat

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628



WESTERN ELECTRICITY COORDINATING COUNCIL

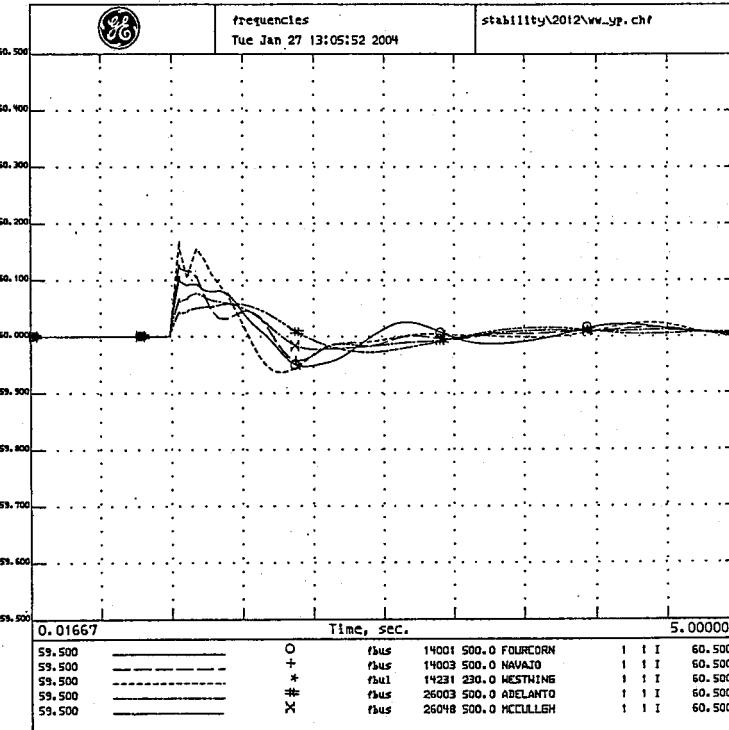
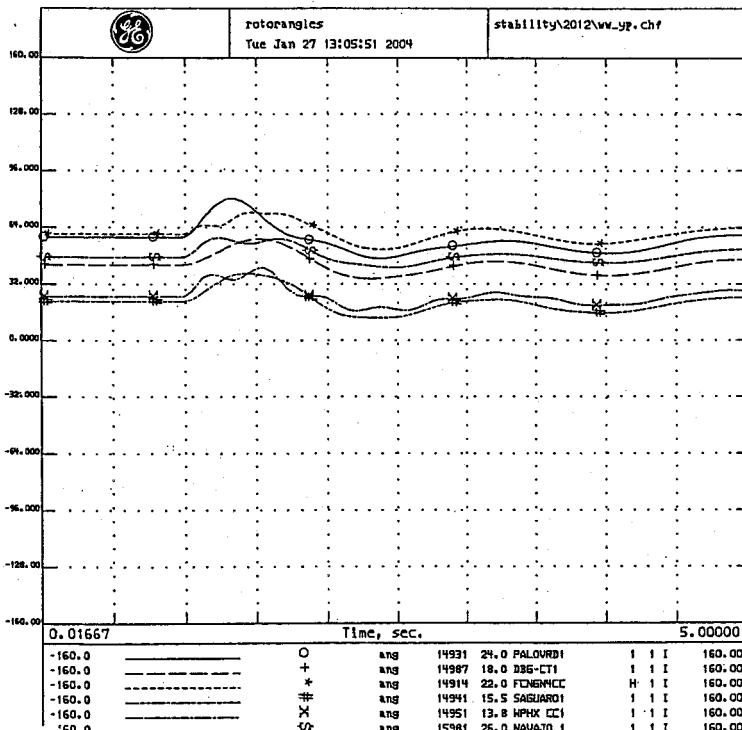
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WESTERN ELECTRICITY COORDINATING COUNCIL

WW\_FLT\_WW-YAV line out  
MAY 19, 2003  
WW-YAV STAB; 1/03; T=0 3P FLT WNG500;FLSH CAPS HNP-YAV/YAV-HNG,  
NAV-HNP/HNG;4C CLR FLT W/HNG-YAV;BC REIN;2012.4y4 NSCC.bat

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WW\_FLT\_WW-YAV line out  
MAY 19, 2003  
WW-YAV STAB; 1/03; T=0 3P FLT WNG500;FLSH CAPS HNP-YAV/YAV-HNG,  
NAV-HNP/HNG;4C CLR FLT W/HNG-YAV;BC REIN;2012.4y4 NSCC.bat

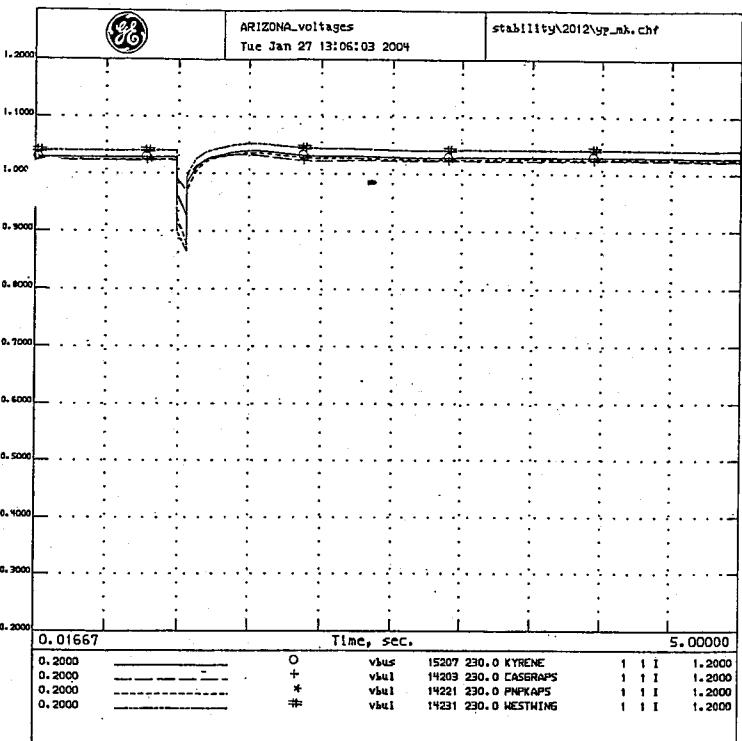
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WESTERN ELECTRICITY COORDINATING COUNCIL

WW\_FLT\_WW-YAV line out  
MAY 19, 2003  
WW-YAV STAB; 1/03; T=0 3P FLT WNG500;FLSH CAPS HNP-YAV/YAV-HNG,  
NAV-HNP/HNG;4C CLR FLT W/HNG-YAV;BC REIN;2012.4y4 NSCC.bat

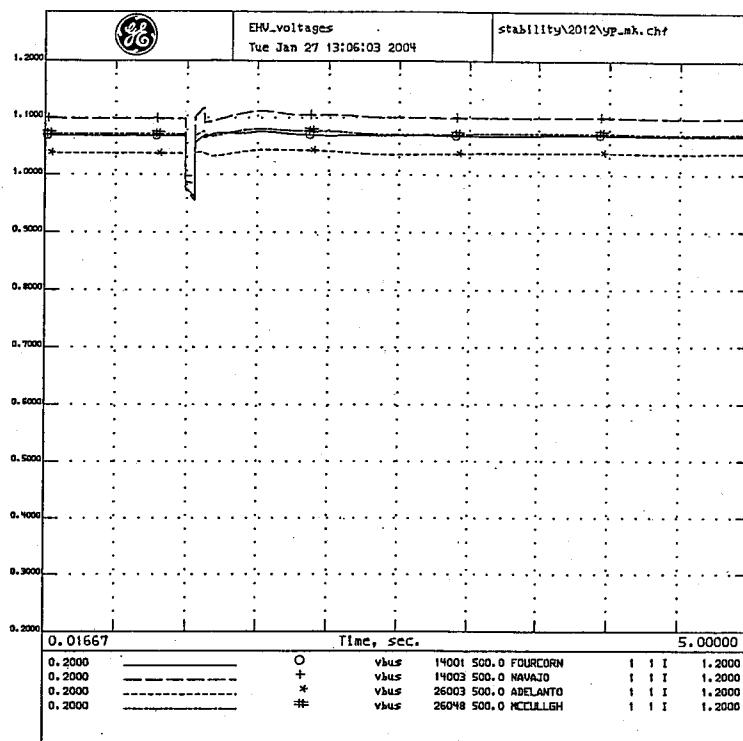
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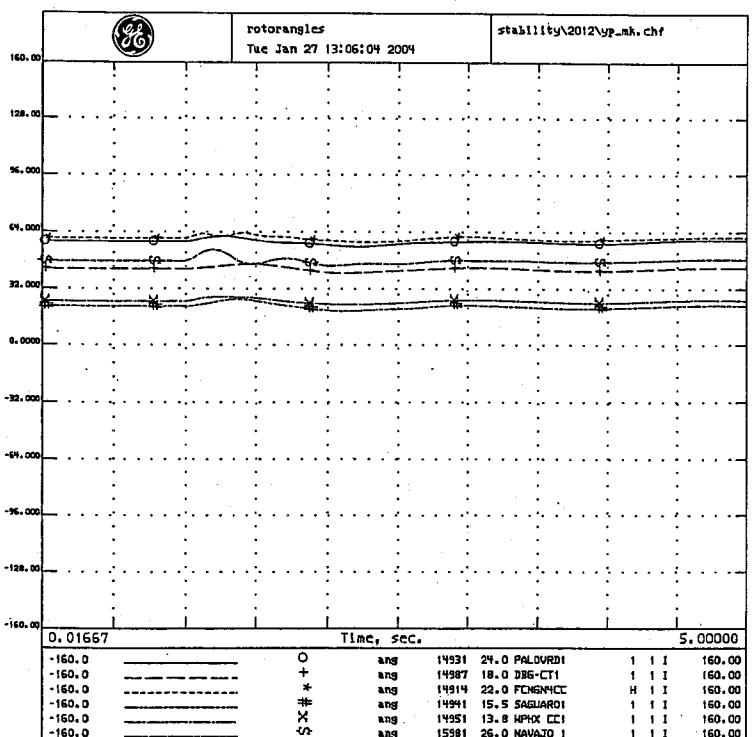
WESTERN ELECTRICITY COORDINATING COUNCIL  
YAV, FLT, Yav-Moen line out  
MAY 19, 2003  
YAV STAB: 1/03; T=0 3P FLT W/HG500/FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MKP/HNG/4C CLR FLT W/YAV-MNK/BC REIN\2012.4y4 HSCC.bat

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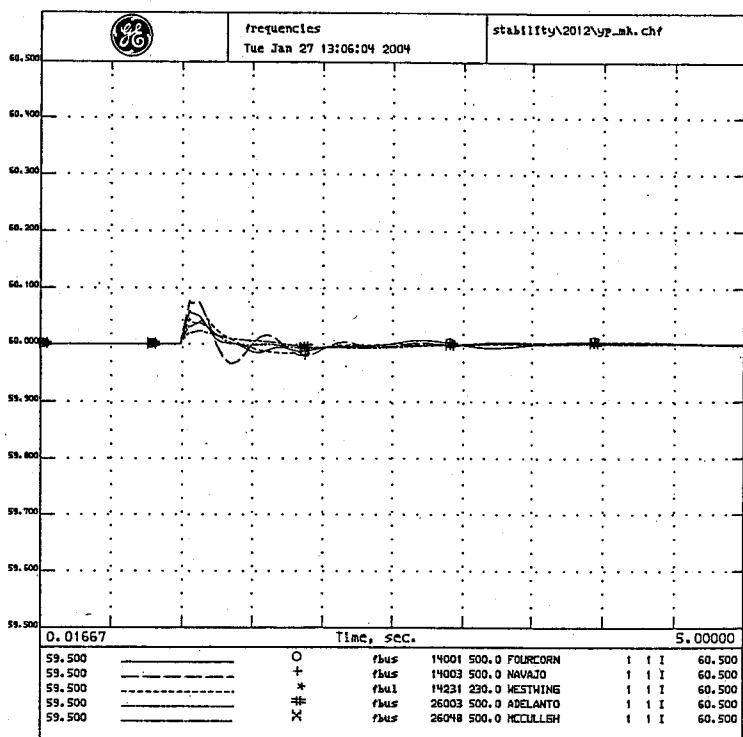
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YAV, FLT, Yav-Moen line out  
MAY 19, 2003  
YAV STAB: 1/03; T=0 3P FLT W/HG500/FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MKP/HNG/4C CLR FLT W/YAV-MNK/BC REIN\2012.4y4 HSCC.bat

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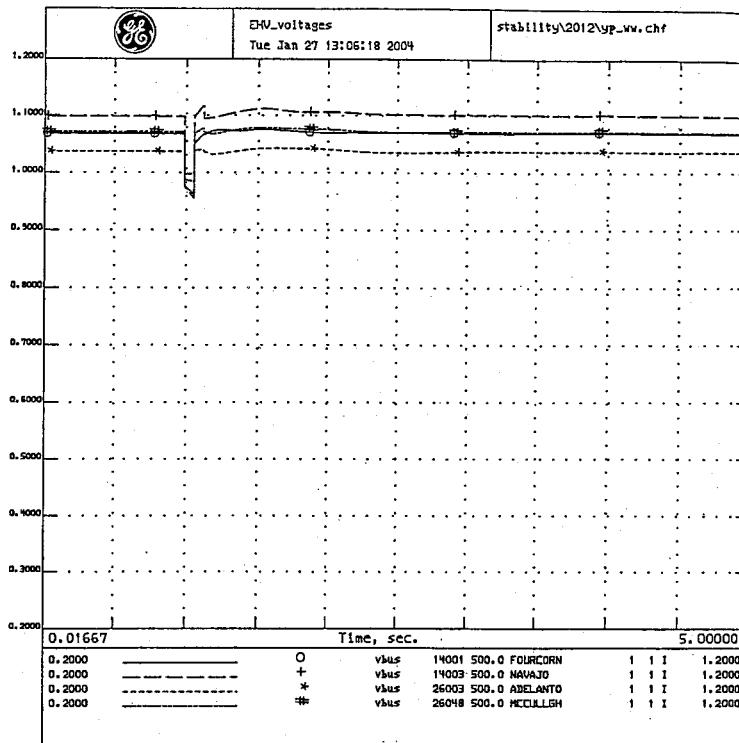
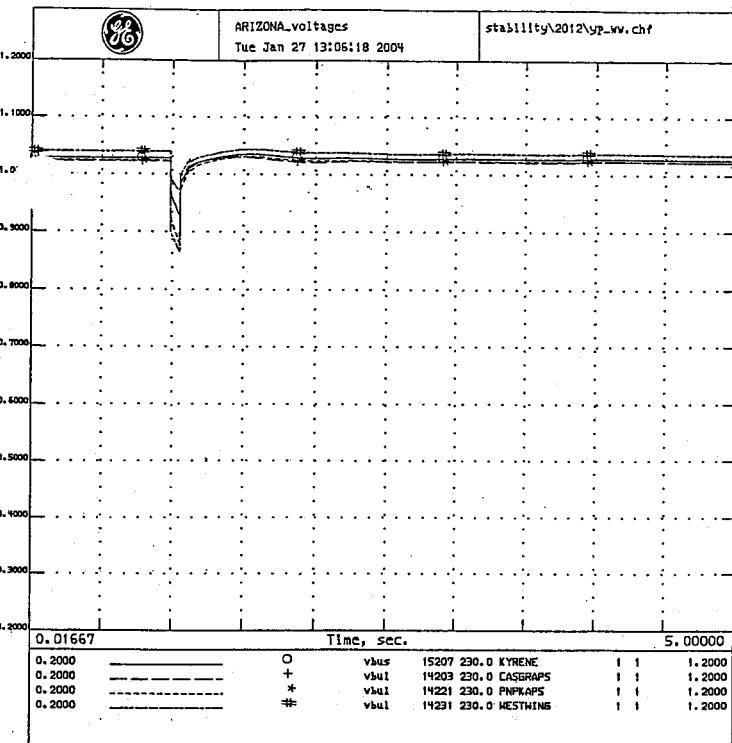
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YAV, FLT, Yav-Moen line out  
MAY 19, 2003  
YAV STAB: 1/03; T=0 3P FLT W/HG500/FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MKP/HNG/4C CLR FLT W/YAV-MNK/BC REIN\2012.4y4 HSCC.bat

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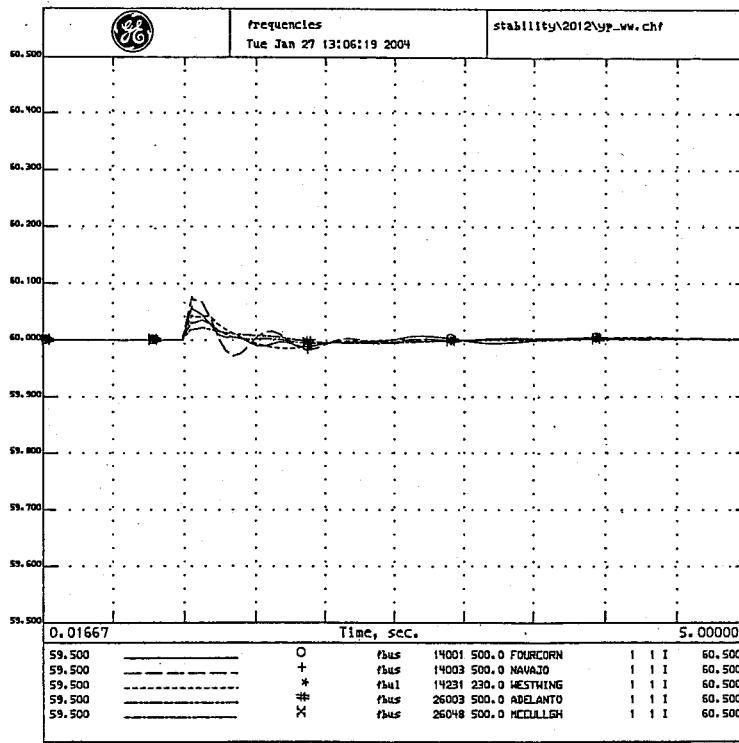
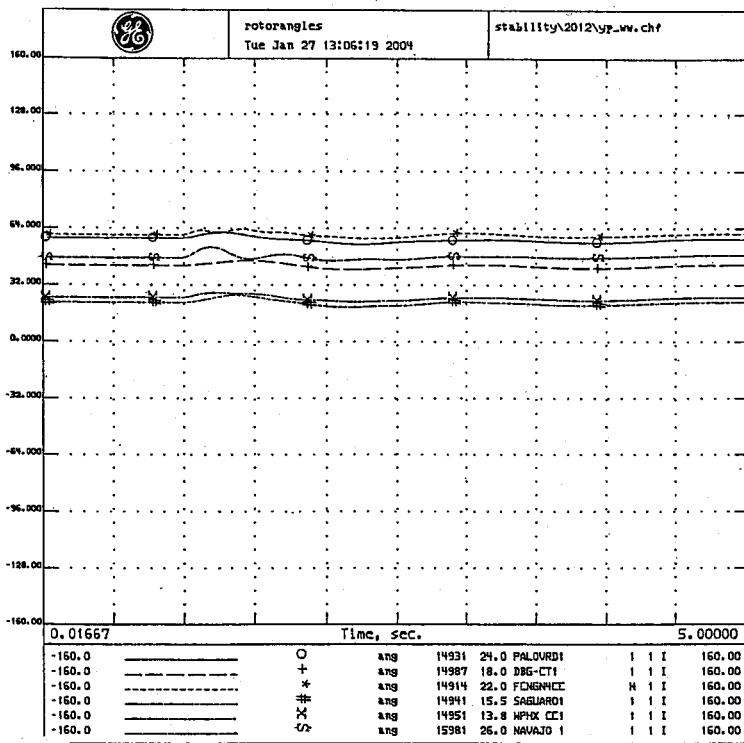
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YAV, FLT, Yav-Moen line out  
MAY 19, 2003  
YAV STAB: 1/03; T=0 3P FLT W/HG500/FLSH CAPS MKP-YAV/YAV-HNG,  
NAV-MKP/HNG/4C CLR FLT W/YAV-MNK/BC REIN\2012.4y4 HSCC.bat

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WESTERN ELECTRICITY COORDINATING COUNCIL  
YAV, FLT, Yav-WH line out  
MAY 19, 2003  
YAV STAB1 1/03; T=0 3P FLT WH6500;FLSH CAPS MKP-YAV/YAV-WH,  
NAV-MKP/WHG;HC CLR FLT W/YAV-WH;BC REIN;2012.4y4 NSCC.bat

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
CONTAINS THE NEW GOVERNOR MODELING RECEIVED IN RESPONSE TO THE  
NOVEMBER 7, 2002 DATA REQUEST.



WESTERN ELECTRICITY COORDINATING COUNCIL  
YAV, FLT, Yav-WH line out  
MAY 19, 2003  
YAV STAB1 1/03; T=0 3P FLT WH6500;FLSH CAPS MKP-YAV/YAV-WH,  
NAV-MKP/WHG;HC CLR FLT W/YAV-WH;BC REIN;2012.4y4 NSCC.bat

ALL COMMENTS RECEIVED FROM THE TSS REVIEW HAVE BEEN ADDED.  
MOST RECENT VERSION OF THE MASTER DYNAMICS FILE IS USED, WHICH  
CONTAINS THE NEW GOVERNOR MODELING RECEIVED IN RESPONSE TO THE  
NOVEMBER 7, 2002 DATA REQUEST.

C31

## **APPENDIX D**

Loop-in of the  
Jojoba-Kyrene 500-kV line  
into Rudd 500-kV substation

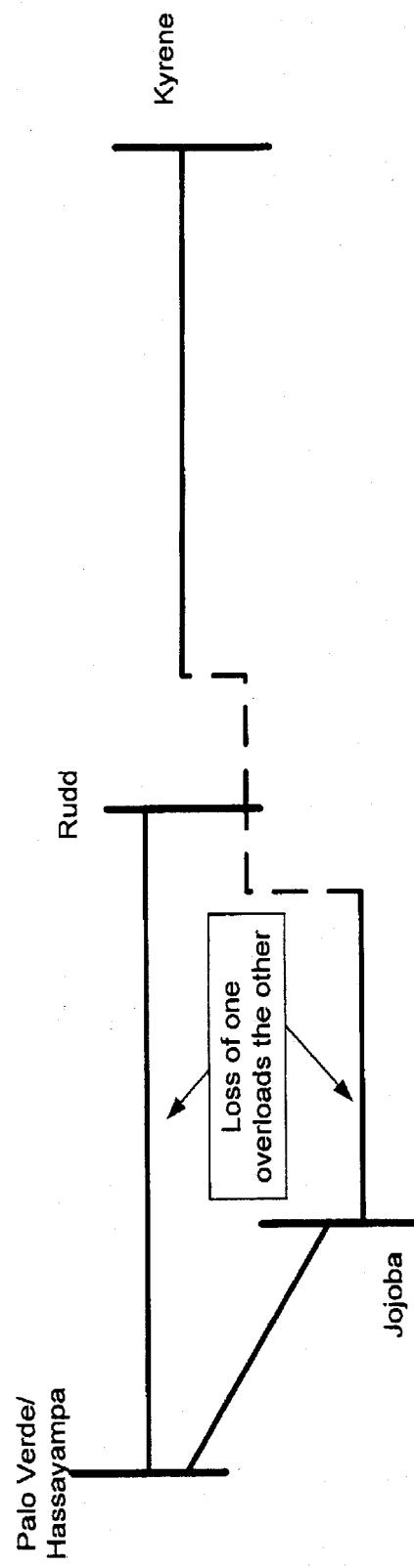
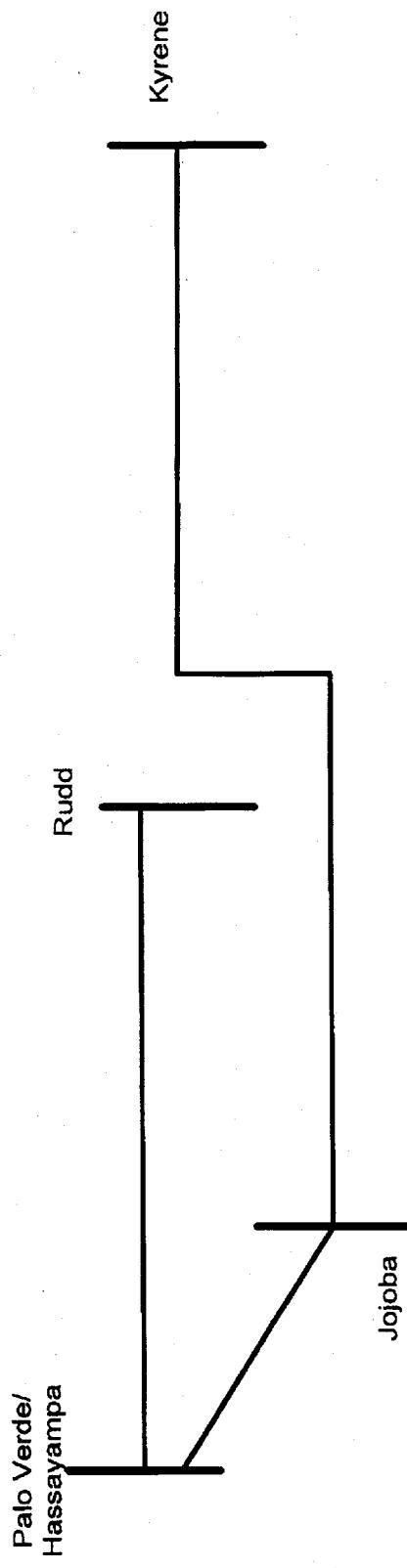
The interconnection was studied on the 2008 Base Case which includes the South East Valley project, the PV-TS5 500kV line, the TS5-TS1 230kV line, and the TS1-TS3 230kV line. Then it was studied on a case without those same projects, called Case 1. Both with and without were from a 2008 powerflow case. The studies were performed at both the Simultaneous Import Limit (SIL) and the Maximum Load Serving Capability (MLSC) point for each year. The effect of the addition was measured by the impact on the critical outages and critical elements which limit the load serving capability for each case.

	SIL	Critical Outage/ Critical Element	MLSC	Critical Outage/ Critical Element
<b>2008 Base Case</b>	10494 MW	Jojoba-Kyrene/ Voltage Collapse	13952 MW	Lincoln St.-W. Phx/ Glendale-Aqua Fria
w/cut-in	9629 MW	Palo Verde-Rudd/ Jojoba-Rudd	13340	Palo Verde-Rudd/ Jojoba-Rudd
<b>Drop in Load Serving Capability</b>	<b>865 MW</b>		<b>612 MW</b>	

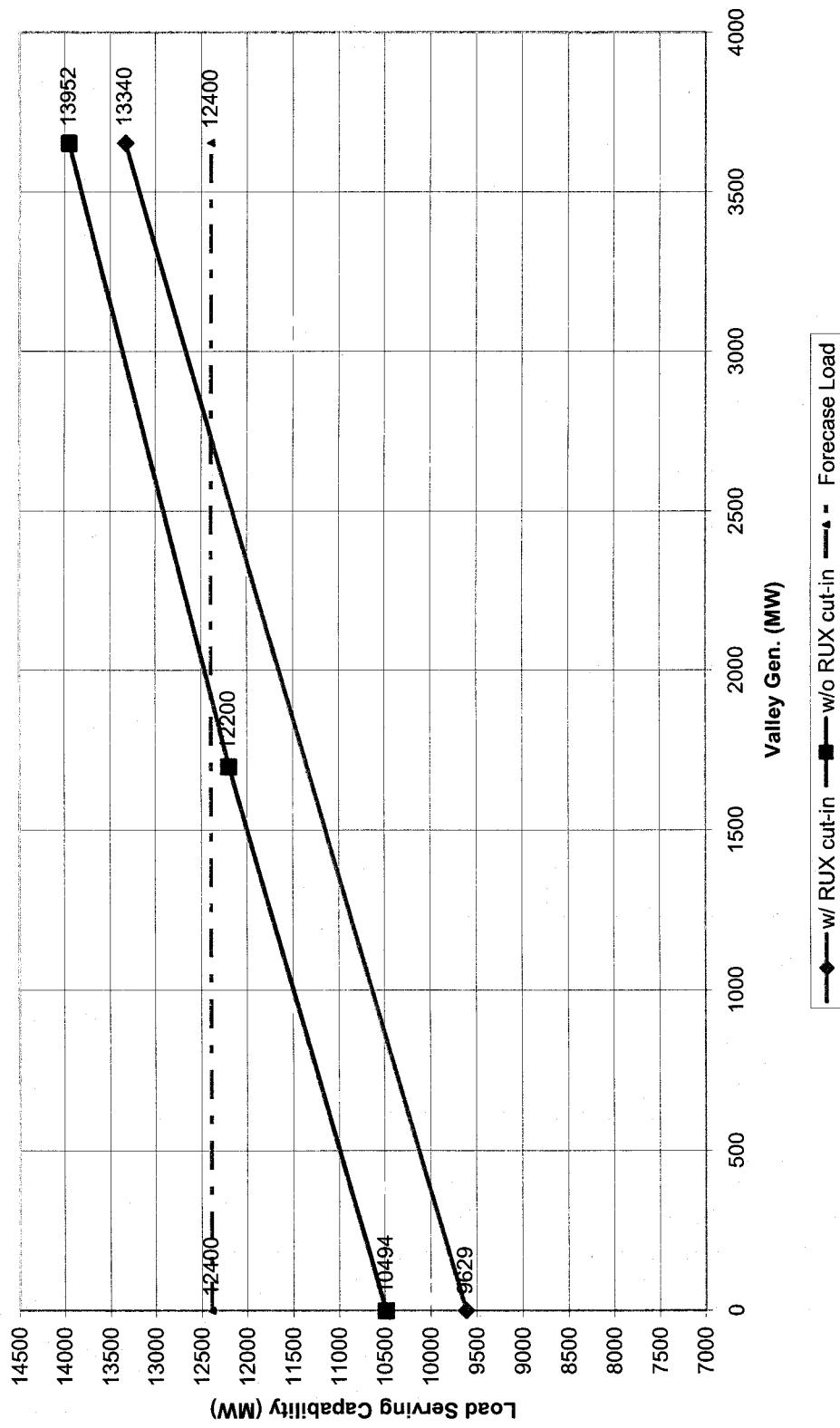
	SIL	Critical Outage/ Critical Element	MLSC	Critical Outage/ Critical Element
<b>2008 Case 1</b>	9762 MW	Jojoba-Kyrene/ Voltage Collapse	13332 MW	Palo Verde-Rudd/ Westwing-Surprise
w/cut-in	8420 MW	Palo Verde-Rudd/ Jojoba-Rudd	12419 MW	Palo Verde-Rudd/ Jojoba-Rudd
<b>Drop in Load Serving Capability</b>	<b>1342 MW</b>		<b>913 MW</b>	

From the above tables and the attached nomograms, addition of the Rudd cut-in of the Jojoba-Kyrene 500kV line significantly reduces the load serving capability of the system. With two 500kV lines feeding Rudd and one 500kV line continuing on from Rudd to feed Kyrene the loss of either 500kV line into Rudd will overload the other line, with the loss of the Palo Verde-Rudd 500kV line being slightly more detrimental than loss of the Jojoba-Rudd 500kV line. Both the 500kV lines into Rudd were studied with a 3000A rating.

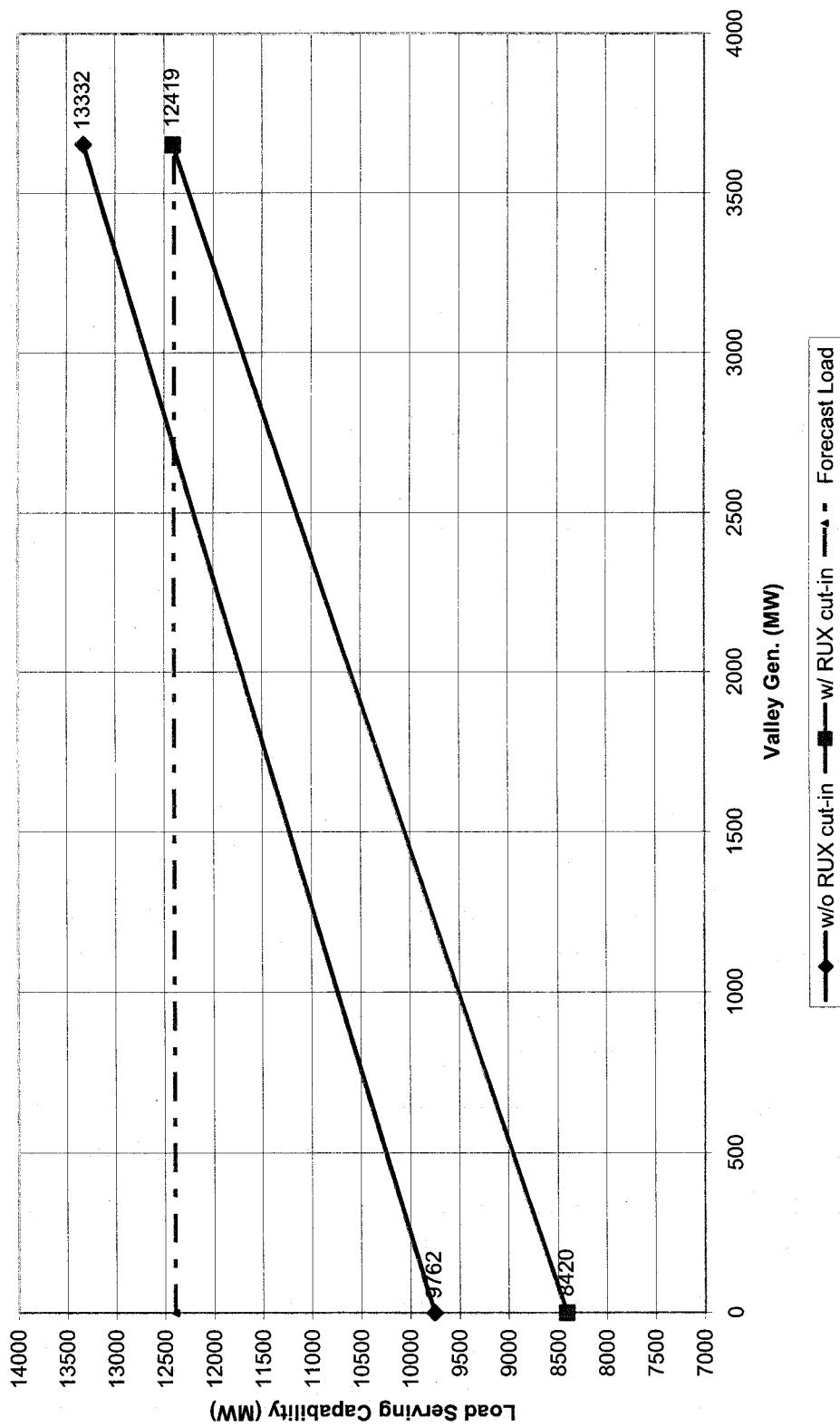
## Rudd Interconnection of Jojoba-Kyrene 500kV Line



**Rudd loop-in Jojoba-Kyrene Line  
With SEV, PV-TS5, TS1-TS3**



**Rudd Loop-in Jojoba-Kyrene Line  
w/o SEV, PV-TS5, TS1-TS3**





# **Reliability Must-Run Analysis**

**2004–2013**

**January 30, 2004  
APS Transmission Planning**

## TABLE OF CONTENTS

	<u>PAGE</u>
<b>List of Tables .....</b>	3
<b>List of Figures.....</b>	4
<b>I. Executive Summary .....</b>	5
A. Study Overview .....	6
B. Summary of Results.....	7
C. Report Conclusions.....	10
D. Report Organization.....	12
<b>II. Introduction.....</b>	13
A. Background of Study Requirement.....	13
B. Overview of RMR.....	13
C. Study Methodology.....	14
D. Determination of SIL and RMR Conditions.....	15
<b>III. Phoenix Load Pocket.....</b>	16
A. Description of Phoenix Area.....	16
B. Phoenix area Critical Outages.....	22
C. Phoenix Area - SIL for 2005, 2008 and 2012 .....	23
D. Generation Sensitivities .....	25
<b>IV. Yuma Area .....</b>	27
A. Description of Yuma Area.....	27
B. Yuma Area Critical Outages.....	29
C. Yuma Area - SIL for 2005, 2008 and 2012 .....	29
D. Generation Sensitivities .....	32
<b>V. Analysis of RMR Conditions.....</b>	33
A. Phoenix Area.....	33
1. Annual RMR Conditions .....	33
2. Maximum Load Serving Capability (MLSC).....	35
3. Area Load Forecast.....	36
4. Generation.....	37
5. Reserves .....	40
B. Yuma Area .....	40
1. Annual RMR Conditions .....	40
2. Maximum Load Serving Capability (MLSC).....	43
3. Area Load Forecast .....	43
4. Generation.....	44
5. Reserves .....	44

<b>VI. Economic Analysis of RMR.....</b>	<b>45</b>
A. Introduction.....	45
B. Phoenix.....	46
1. Phoenix Imports .....	46
2. Operation of Phoenix area Generating Units .....	46
3. Cost Impacts.....	47
4. Emissions Impact.....	47
C. Yuma .....	49
1. Yuma Imports .....	49
2. Operation of Yuma Units.....	49
3. Cost Impacts.....	50
4. Emission Impacts .....	50
<b>VII. Conclusions.....</b>	<b>51</b>

## **Appendices**

A. Regional Production Cost Modeling Assumptions.....	A1
B. Power Flow Output Results .....	B1 – B24

**LIST OF TABLES**

	<u>Page</u>
ES1. Phoenix area RMR Conditions and Costs .....	7
ES2. Yuma area RMR Conditions and Costs .....	8
ES3. Phoenix area Maximum Load Serving Capability .....	9
ES4. Yuma area Maximum Load Serving Capability .....	9
ES5. Phoenix area RMR Outside Economic Dispatch .....	10
ES6. Yuma area RMR Outside Economic Dispatch.....	10
ES7. Phoenix area Air Emissions Reduction.....	11
ES8. Yuma area Air Emissions Reduction .....	12
1. Phoenix area Load Sensitivity .....	17
2. 2005, 2008, and 2012 Phoenix area Simultaneous Import Limit .....	23
3. Generation Sensitivities Inside Phoenix .....	25
4. Generation Sensitivities Outside Phoenix.....	25
5. Yuma Projects .....	31
6. Phoenix RMR Conditions Without Phoenix area Generation .....	33
7. Phoenix area Maximum Load Serving Capability.....	36
8. Phoenix and Yuma Load and Energy .....	37
9. Phoenix area Generation .....	38
10. Yuma RMR Conditions Without Generation .....	41
11. Yuma area Maximum Load Serving Capability .....	43
12. Yuma area Generation .....	44
13. Impact of Eliminating Phoenix Import Limits.....	46
14. Phoenix Historical Capacity Factor .....	47
15. Phoenix area Air Emissions Reduction.....	48
16. Phoenix Power Plant Emissions.....	48
17. Impact of Eliminating Yuma Import Limits .....	49
18. Yuma Plants (Historical Generation .....	50
19. Yuma Power Plant Emissions.....	50
C1. Phoenix area Air Emissions Reduction.....	51
C2. Yuma area Air Emissions Reduction .....	52

**LIST OF FIGURES**

	<u>Page</u>
1. Phoenix area 2005 Load Description .....	18
2. Phoenix area 2008 Load Description .....	19
3. Phoenix area 2012 Load Description .....	20
4. Phoenix area 2005 Load Serving Capability .....	23
5. Phoenix area 2008 Load Serving Capability .....	24
6. Phoenix area 2012 Load Serving Capability .....	24
7. Yuma District Transmission System (2005).....	27
8. Yuma District Transmission System (2008).....	28
9. Yuma District Transmission System (2012).....	29
10. Yuma area 2005 Load Serving Capability.....	30
11. Yuma area 2008 Load Serving Capability.....	30
12. Yuma area 2012 Load Serving Capability.....	31
13. 2005 Phoenix Load Duration & RMR Condition .....	34
14. 2008 Phoenix Load Duration & RMR Condition .....	34
15. 2012 Phoenix Load Duration & RMR Condition .....	35
16. 2005 Yuma Load Duration & RMR Condition .....	41
17. 2008 Yuma Load Duration & RMR Condition .....	42
18. 2012 Yuma Load Duration & RMR Condition .....	42

# **APS Reliability Must-Run Analysis 2004-2013**

## **I. EXECUTIVE SUMMARY**

This report documents the study methodology, results, and conclusions of Arizona Public Service Company's (APS) Reliability Must-Run (RMR) Analysis for the ten years from 2004 to 2013. This analysis was conducted in response to the Arizona Corporation Commission's (ACC) Second Biennial Transmission Assessment (Assessment) and Decision No. 65476 (December 19, 2002). The 2004 RMR Analysis covers a ten-year period and includes detailed analysis of the years 2005, 2008, and 2012.

If a city or load pocket must be served by local generating units at certain peak times, then those units are designated as "reliability must-run" or RMR units. In APS' service territory there are two major areas where load cannot be served totally by power imported over transmission lines – the Phoenix metropolitan area which is served by a combination of APS and SRP facilities, and the APS service territory in the Yuma area.

While ninety-nine percent of the Phoenix area energy requirements can be met by remote generation, local generation is critically important for the reliability of the local power system. The November 2003 U.S.-Canada Power System Outage Task Force Interim Report: Causes of the August 14<sup>th</sup> Blackout in the United States and Canada pointed out the importance of the reactive capability of voltage support from local generation. Local generation can provide critical support for transmission contingencies and other power system disturbances and can prevent customer outages including blackout conditions such as those experienced in the Northeast on August 14, 2003.

Comments during the workshop for the 2003 RMR analysis held in February 2003 indicated that electric power system industry participants desired to have a more participative role in the 2004 RMR analysis. To facilitate this participation, APS and the other Arizona transmission providers utilized the Central Arizona Transmission Study forum to publicly determine the 2004 RMR study plan, had extensive discussion on study models and preliminary results, and ultimately conducted a workshop on January 15, 2004 to present the study results for comment. This process led to the decision to study the Phoenix area as a combined APS and Salt River Project (SRP) network, the determination of the specific years to study; 2005, 2008, and 2012, and the specific loads to include in the Phoenix area for the three study years.

The year 2005 was selected to provide a benchmark for the 2003 RMR study. The years 2008 and 2012 were selected as representative years during the ten-year window and because databases for these years were being used to perform studies in other study forums such as the Southwest Transmission Expansion Plan (STEP) planning group and the Seams Steering Group-Western Interconnection (SSG-WI).

This study found that the results for the 2005 study were similar to those from last year's study for 2005. The results for 2008 indicate lower RMR requirements than for 2005. In 2012, the RMR requirements are similar to those for 2005. However, in 2012 available Phoenix area

generation reserves are presently projected to be less than the reserve requirements. Although the reserve margin deficiency is not itself related to RMR, it is a load-serving issue that should be addressed. To mitigate the 2012 deficiency in Phoenix area reserves, APS and SRP are presently evaluating both transmission alternatives to increase import capability and alternatives to increase Phoenix area generation.

The cost of using must-run units can be measured by the difference between generation costs with the transmission limit and costs without the limit. This report looks at and compares the cost of serving these two areas with and without the existing transmission constraints.

This report concludes that for the Phoenix metropolitan area, the cost of RMR with the transmission limit is less than \$100,000 annually and does not at present outweigh the cost of transmission improvements beyond those already included in the APS and SRP ten-year plans. Costs to relieve import limitations were documented in the 2003 RMR study to be in excess of \$16 million. For Yuma, the report shows that the new North Gila 500/69-kV transformer and the new 230-kV line from Gila Bend-to-Yuma included in the present APS ten-year plan is sufficient to cost-effectively address RMR conditions. Environmental effects for both areas with and without transmission constraints are also documented in this report. Because there is such a small RMR requirement for both areas in all three years studied, the environmental effects of RMR are minimal.

## **A. Study Overview**

The existence of transmission import limited areas is not uncommon in the United States, and particularly in the West where load centers are generally separated by long distances. APS has transmission import-limited areas in Phoenix and Yuma. An import area is transmission limited when all load cannot be served solely by importing resources over local transmission lines, thus requiring some use of local generating units to reliably meet peak load.

The two transmission import-limited areas in APS' system were studied to determine:

- The system simultaneous import limit (SIL), which is the maximum amount of capacity that can be reliably imported into an area with no local generation;
- The maximum load serving capability (MLSC), which is the total load that can be reliably served from imports and from local generation;
- Annual RMR conditions, including magnitude of load in excess of the SIL and number of hours the load exceeds the SIL; and
- Estimated economic and environmental impacts of the import limits.

The Phoenix area is a tight network of APS and SRP load, resources, and transmission facilities. Because the Phoenix system is highly integrated, the import limits must be determined for the combined area. This analysis was coordinated with SRP personnel, who had significant involvement in the study and were helpful in the overall analysis. The Western Area Power Administration (WAPA) coordinated with APS and SRP in the study because their transmission facilities interface with the Phoenix network.

After the combined import limit (SIL) for the Phoenix area was determined, RMR conditions were evaluated for the Phoenix area based on the Phoenix area import limits, the Phoenix area load, and Phoenix area local generation, which includes generation owned by APS, SRP and Pinnacle West Energy Corporation (PWE).

The Yuma area, which has a forecast 2005 summer peak demand of approximately 344 MW, is served by an internal APS 69-kV sub-transmission network containing all of the load in the import-limited area. There are external ties to WAPA and the Imperial Irrigation District (IID), as well as a bulk power interface with the Hassayampa-to-North Gila transmission system. This analysis was coordinated with the WAPA Phoenix office to ensure accurate modeling.

## B. Summary of Results

Results of the analysis for the three years of the study, 2005, 2008, and 2012, assume that present plans for system improvements in place when the study was conducted are completed on schedule.

The following table summarizes the estimated RMR conditions and costs for the Phoenix area.

**Table ES1**  
**Phoenix area RMR Conditions and Costs**

Year	SIL <sup>1</sup> (MW)	Peak Demand (MW)	Max RMR <sup>2</sup> (MW)	RMR <sup>3</sup> Hours	RMR Energy <sup>4</sup> (GWH)	RMR Energy (% of total)	RMR Cost <sup>5</sup> (\$K)
2005	8,617	11,141	2,524	678	550	1.2	0.0
2008	10,511	12,425	1,914	338	222	0.4	0.0
2012	11,103	14,406	3,303	758	805	1.3	84.0

### Table Key:

<sup>1</sup>**SIL** – System Simultaneous Import Limit is the maximum amount of capacity that can be reliably imported into the area with no local generation operating.

<sup>2</sup>**Max RMR** – The amount of local generation required to meet the area peak demand (Peak Demand minus SIL).

<sup>3</sup>**RMR Hours** – The number of hours that the area's demand exceeds the SIL, thus requiring the use of local generation to meet load, even if otherwise economically dispatched.

<sup>4</sup>**RMR Energy** – The annual energy required to be met by local generation (in excess of the SIL).

<sup>5</sup>**RMR Cost** – The difference in annual generation cost with and without the transmission limitation.

The following table summarizes the estimated RMR conditions and costs for the Yuma area.

**Table ES2**  
**Yuma Area RMR Conditions and Costs**

Year	SIL <sup>1</sup> (MW)	Peak Demand (MW)	Max RMR <sup>2</sup> (MW)	RMR <sup>3</sup> Hours	RMR Energy <sup>4</sup> (GWH)	RMR Energy (% of total)	RMR Cost <sup>5</sup> (\$K)
2005	265	344	79	714	20	1.3	500.0
2008	292	380	88	676	21	1.2	0.0
2012	410	425	15	12	0	0.0	0.0

**Table Key:**

<sup>1</sup>**SIL** – System Simultaneous Import Limit is the maximum amount of capacity that can be reliably imported into the area with no local generation operating.

<sup>2</sup>**Max RMR** – The amount of local generation required to meet the area peak demand (Peak Demand minus SIL).

<sup>3</sup>**RMR Hours** – The number of hours that the area's demand exceeds the SIL, thus requiring the use of local generation to meet load, even if otherwise economically dispatched.

<sup>4</sup>**RMR Energy** – The annual energy required to be met by local generation (in excess of the SIL).

<sup>5</sup>**RMR Cost** – The difference in annual generation cost with and without the transmission limitation.

The following table shows the Phoenix area Maximum Load-Serving Capability (MLSC) for the three years studied and compares the MLSC to the forecasted peak demand. This includes the new generation of Santan 5 in the 2005 study and Santan 6 in the 2008 study. The MLSC is determined by adding the SIL and the local generation minus the local reserve requirement. APS determined the Phoenix area reserve requirements by performing a probabilistic analysis that considered the size and forced outage rates of the local generating units and resulted in 99 percent reliability of serving all load. This analysis resulted in reserve requirements of 809 MW, 865 MW, and 865 MW for the Phoenix area for the years 2005, 2008, and 2012 respectively.

**Table ES3**  
**Phoenix Area Maximum Load Serving Capability**

Year	SIL	Local Generation	Required Reserves	MLSC (SIL+LG-RR)	Peak Demand (MW)	Projected Reserves
2005	8,617	3,374	809	11,182	11,141	850
2008	10,511	3,649	865	13,295	12,425	1735
2012	11,103	3,649	865	13,887	14,406	346

The following table summarizes the Yuma area MLSC. The reserve requirements for the Yuma area were determined to be 138 MW for all years studied.

**Table ES4**  
**Yuma Area Maximum Load Serving Capability**

Year	SIL	Local Generation	Required Reserves	MLSC (SIL+LG-RR)	Peak Demand (MW)	Projected Reserves
2005	265	267	138	394	344	188
2008	292	267	138	421	380	179
2012	410	267	138	539	425	252

Local generating units are dispatched based on cost. Thus, most of the RMR hours shown above are dispatched in merit order. However, the presence of a transmission constraint may require local generation to be dispatched out of merit order or "out of the money." This report considered all Phoenix area and Yuma area transmission limitations and generation resources in determining the overall RMR situation. The economic impact of RMR can be seen from the following tables.

The following table summarizes the estimated total number of hours that local Phoenix generation must run out of economic dispatch, the amount of energy that is produced out of economic dispatch and the associated cost.

**Table ES5**  
**Phoenix area RMR Outside Economic Dispatch**

Year	Hours outside economic dispatch	Energy outside economic dispatch (GWH)	RMR Cost (\$K)
2005	18	6	0
2008	0	0	0
2012	14	1	84

The following table summarizes the estimated total number of hours that APS local Yuma generation must run out of economic dispatch, the amount of energy that is produced out of economic dispatch and the associated cost.

**Table ES6**  
**APS Yuma Area RMR Outside Economic Dispatch**

Year	Hours outside economic dispatch	Energy outside economic dispatch (GWH)	RMR Cost (\$K)
2005	336	8	500
2008	2	0	0
2012	0	0	0

### C. Report Conclusions

#### *Phoenix area Conclusions*

1. All Phoenix area transmission and local generation are necessary to reliably serve Phoenix area peak load in 2005 with the local generation reserve margin just exceeding the required reserve margin. In 2008, the local generation reserve margin significantly exceeds the required reserve margin. However, in 2012 the reserve margin is 346 MW which is 519 MW less than the required reserve margin of 865 MW. To mitigate this reserve deficiency APS and SRP are presently evaluating both transmission alternatives to increase import capability and alternatives to increase Phoenix area generation.

2. During the summer, Phoenix area load is expected to exceed the available transmission import capability for approximately 680 hours in 2005, 340 hours in 2008, and 760 hours in 2012. These hours represent only approximately one percent of the annual energy requirements for the Phoenix area.
3. From a total Phoenix load, transmission, and resources viewpoint, import limits are expected to cause a minimal amount of local generation to be dispatched out of economic dispatch order in 2005 and 2012, and no impact in 2008.
4. The estimated annual economic cost of Phoenix area RMR generation is negligible, therefore advancement of transmission projects to increase import capability are presently not cost justified.
5. Removing the transmission constraint could reduce total Phoenix area air emissions by the following annual amount for 2005. There is a minimal impact for years 2008 and 2012 due to the increased import capabilities and resources resulting in fewer hours of operating local generation.

**Table ES7  
Phoenix area Air Emissions Reduction**

<b>Pollutant</b>	<b>Reduction<sup>1</sup> (tons/year)</b>	<b>Reduction of Phoenix Area Emissions (% of total emissions from all sources)</b>
VOC	0.0	0.000
NO <sub>x</sub>	4.0	0.007
CO	1.0	0.000
PM <sub>10</sub>	0.0	0.000

<sup>1</sup>2005 results, impact for 2008 and 2012 are lower

6. Removing the import restriction into the Phoenix area has no impact on local generation capacity factor. The capacity factor ranges from approximately 11% in 2005 to 26% in 2012.

#### ***Yuma Area Conclusions***

7. All existing Yuma area transmission and generation resources are necessary to reliably serve the Yuma area load.
8. The Yuma area load is expected to exceed the available transmission import capability for 714 hours in 2005, 676 hours in 2008 and 12 hours in 2012 although the amount of total load in the Yuma area is approximately 350-425 MW.

9. From a total Yuma load, transmission, and resources viewpoint, the import constraint could cause APS Yuma generation to be dispatched out of economic dispatch order for 336 hours in 2005, 2 hours in 2008, and 0 hours in 2012.
10. The estimated annual economic cost of Yuma area generation required to run out of economic dispatch order is relatively small, therefore advancement of transmission projects to increase import capability are presently not cost justified.
11. Removing the transmission constraint could reduce total Yuma area air emissions by the following annual amount for 2005. There is a minimal impact for years 2008 and 2012 due to the increased import capabilities resulting in fewer hours of operating local generation.

**Table ES8**  
**Yuma Area Air Emissions Reduction**

Pollutant	Reduction <sup>1</sup> (tons/year)	Reduction of Yuma Area Emissions (% of total emissions from all sources)
VOC	1.0	Unavailable
NO <sub>x</sub>	20	Unavailable
CO	5	Unavailable
PM <sub>10</sub>	1.0	0.001

<sup>1</sup>2005 results, impact for 2008 and 2012 are lower

12. Removing the import restriction into the Yuma area could reduce the APS Yuma generation capacity factor from 1.6 percent to 1.2 percent in 2005.

#### **D. Report Organization**

This report is organized in eight sections. Section I provides an executive summary of the report. Section II provides general background information of the study requirements, an overview of RMR, and describes the study methodology. Section III describes the Phoenix area, the nature of the import limit, the resulting import limits for 2005, 2008, and 2012, and the impact of various generators in and around the Phoenix area on the import limit. Section IV provides a similar discussion of the Yuma area. Section V describes the RMR conditions such as number of hours, maximum capacity, and annual energy for the Phoenix and Yuma areas. Section VI provides results of the economic analysis of the Phoenix and Yuma area RMR conditions performed utilizing a regional planning model (GE MAPS) and emissions impact. Finally, Section VII lists the conclusions of the analysis.

## **II. INTRODUCTION**

### **A. Background of Study Requirement**

Like all large electric utilities, Arizona utilities have historically relied on both transmission, to deliver remote generation into its load centers, as well as local generation to reliably serve its customers. Due in part to environmental, economic, and fuel availability considerations, large base-load thermal generators have typically been located away from the load centers while smaller but less efficient intermediate and peaking units — with lower capacity factors — were located within the load centers. Although this local generation is relied on for a relatively small amount of energy, this local generation is critically important for the reliability of the local power system. The November 2003 U.S.-Canada Power System Outage Task Force Interim Report: Causes of the August 14<sup>th</sup> Blackout in the United States and Canada pointed out the importance of the reactive capability of voltage support from local generation. Local generation can provide critical support for transmission contingencies and other power system disturbances and can prevent customer outages including blackout conditions such as those experienced in the Northeast on August 14, 2003. Local generation also results in lower power system losses and lower capital expenses for transmission infrastructure.

In the past, vertically-integrated utilities, such as APS, managed the siting and construction of both generation and transmission resources needed to serve their customers. Electric systems were designed based on a detailed integrated resource planning process used to evaluate the appropriate balance of generation, transmission, and demand-side resources. Interconnections with neighboring systems were primarily intended to improve system reliability and lower the costs of reserves by allowing for sharing of capacity reserves by multiple systems. Each utility's system was primarily designed to accommodate that utility's resources and that utility's load.

The Commission's Second Biennial Transmission Assessment requires "any [Utility Distribution Company] that currently relies on local generation, or foresees a future time period when utilization of local generation may be required to assure reliable service for a local area, [to] perform and report the findings of an RMR study as a feature of their ten year plan filing with the Commission in January 2003 and 2004." The Assessment required that the RMR study filed in January 2003 evaluate RMR conditions through the 2005 summer peak. The January 2004 RMR study covers the 10-year period from 2004 to 2013.

### **B. Overview of RMR**

Local "load pockets" are areas that do not have enough transmission import capability to serve all load in the area solely by importing remote generation over local transmission facilities. For these areas, during peak hours of the year, local generation is required to serve that portion of the load that cannot reliably be served by transmission imports. This local generation requirement is often referred to as Reliability Must-Run or RMR generation. In these areas, during peak conditions, load is served by a combination of importing remote generation over transmission lines and operating local generation.

The maximum load that can be served in a load pocket with no local generation operating — in other words, the maximum load that can be served solely by importing remote generation — is referred to as the system Simultaneous Import Limit (SIL). The SIL is established through technical studies by ensuring that:

- With the local load at the SIL and no local generation operating there are no transmission system normal operating (N-0) limit violations of thermal loading or voltages, and
- Under all single contingency outage events (N-1) there are no emergency operating limit violations of thermal loading or voltages, and no system instability.

### **C. Study Methodology**

Import limit analysis was performed for the Phoenix and Yuma areas. See Appendix A for power flow results. The import limit area or load pocket is defined as that load which, when increased, would increase the severity of the limiting contingency. For example, load in Flagstaff has no impact on the severity of the limiting contingency for the Phoenix import limited area, and therefore Flagstaff is not included in the Phoenix load pocket. In contrast, downtown Phoenix load does impact the severity of the limiting contingency and therefore is included in the load pocket. All area contingencies known to result in system stress were evaluated to determine the critical contingency for the area. Import limits were determined by contingency conditions of thermal loading at the emergency rating of a facility, steady state voltages at the emergency voltage limit, and system instability including voltage instability.

Import limits were determined for the Phoenix and Yuma areas with no local generation operating, with maximum local generation operating, and sufficient points in between to determine curves which define import limits at all load levels. This methodology was applied to studies of the Phoenix area, which for 2005 and 2008 is constrained by both voltage instability and thermal loadings, depending on the local load level. In 2012 the Phoenix area is constrained solely by thermal loadings. For the Yuma studies, the limitations are primarily post-disturbance thermal constraints and voltage drop limits. Generator sensitivities were performed to determine the relative impact of various generators on the import limits for the Phoenix and Yuma areas.

From each year's forecasted peak load and historical daily load cycles, the annual RMR conditions were determined including magnitude of local load, both demand and energy, expected to exceed the SIL and the annual hours for which local load is expected to exceed the SIL.

An economic analysis was performed in each area for each year using the GE MAPS production-costing model to determine the cost of the import limits. GE MAPS is a regional generation and transmission simulation model and is discussed in more detail in Appendix B to this report.

Additional transmission alternatives to mitigate the import limits of the Phoenix and Yuma area were not studied due to the minimal amounts of RMR conditions that were identified in the study. The cost for any transmission alternative would significantly exceed the costs associated with any RMR conditions. This report concludes that for the Phoenix metropolitan area, the cost

of RMR with the transmission limit is less than \$100,000 annually and costs to relieve import limitations were documented in the 2003 RMR study to be in excess of \$16 million.

#### **D. Determination of SIL and RMR Conditions**

In this analysis, assessments of the SIL and RMR conditions for the Phoenix area and the Yuma area were performed for the years 2005, 2008, and 2012. The year 2005 was selected to provide a benchmark for the 2003 RMR study. The years 2008 and 2012 were selected as representative years during the ten-year window and because databases for these years were being used to perform studies in other study forums such as the Southwest Transmission Expansion Plan (STEP) planning group and the Seams Steering Group-Western Interconnection (SSG-WI). Base case and contingency power flow, stability, and voltage stability analyses were performed to determine import limitations. The initial starting cases were based on WECC heavy summer full loop base cases in GE Power Flow format for the corresponding year. Those base cases model the entire Western Interconnection's transmission system and were reviewed and then updated to represent expected loads and system configuration for 2005, 2008 and 2012. All cases were coordinated between APS, SRP, Tucson Electric Power Company (TEP), Southwest Transmission Cooperative (SWTC), and WAPA to capture the most accurate expected operating conditions for the Arizona transmission system. Also, the 2012 case is consistent with the 2012 case used in the CATS Phase III study.

### **III. PHOENIX LOAD POCKET**

#### **A. Description of Phoenix Area**

During summer 2005, the Phoenix area — which consists of both APS' and SRP's integrated network — will be served from the following major Extra High Voltage (EHV) substations: Westwing, Pinnacle Peak, Kyrene, Rudd, Browning, and Silverking. These EHV stations form the “cornerstones” of an extensive internal network of 230-kV transmission lines that constitute the high voltage energy delivery system within the Phoenix load area. By summer 2008, two new EHV substations will be added to the existing major EHV substations serving the Phoenix area. They are the TS5 substation and the South East Valley (SEV) substation. And, in 2012 the Raceway substation is added.

Since the summer of 2002, APS has served some northwest Phoenix area load from the Raceway substation, which has been built as an interconnection to the WAPA Westwing-to-Waddell 230-kV line. Because this line has no interconnections with other Phoenix area 230-kV lines, this load does not significantly impact the contingency response of the Phoenix area and is therefore not included in the Phoenix area load determination, until the 2012 case when Raceway becomes interconnected to Pinnacle Peak and the new 500-kV substation.

Because the City of Mesa load is served by dedicated resources external to Phoenix, the economic RMR analysis is performed with this load excluded.

Energy flows into the EHV delivery points from the EHV transmission lines and then is stepped down to 230-kV and transmitted into the load center via the 230-kV transmission lines. These loads, with area losses, are measured by determining the flows from the EHV substations into the load area to include all of these load stations. The specific loads to be included in the Phoenix area load for each of the three years was determined by sensitivity analysis performed early in the study effort to determine the impact of various loads on the severity of the critical contingency. Table 1 shows the results of the sensitivity analysis which was performed on a preliminary 2008 case.

**Table 1**  
**Phoenix Area Load Sensitivity**

<b>Palo Verde-Rudd Outage</b>			<b>Jojoba-Kyrene Outage</b>		
<b>Westwing-Surprise 230kV line</b>			<b>Kyrene 230kV Voltage</b>		
	<b>Overload</b>	<b>% INCREASE</b>		<b>ΔV</b>	<b>% INCREASE</b>
<b>Base Case</b>	<b>100.0%</b>	<b>xxx</b>	<b>Base Case</b>	<b>4.72</b>	<b>XXX</b>
Surprise	107.2%	7.2%	Browning	5.83	1.11
White Tanks	102.6%	2.6%	Santan	5.43	0.71
West Phoenix	102.1%	2.1%	Kyrene	5.35	0.63
Country Club	101.8%	1.8%	Thunderstone	5.35	0.63
Ocotillo	101.4%	1.4%	Ocotillo	5.20	0.5
TS3	101.3%	1.3%	Country Club	5.15	0.43
Buckeye	101.0%	1.0%	Pinnacle Peak	5.10	0.38
Kyrene	101.0%	1.0%	Moonshine (EMA)	5.08	0.36
Thunderstone	101.0%	1.0%	Gavilan Peak	5.08	0.36
Santan	101.0%	1.0%	West Phoenix	5.04	0.32
TS1	101.0%	1.0%	White Tanks	4.99	0.27
Mooshine (EMA)	101.0%	1.0%	Buckeye	4.93	0.21
Pinnacle Peak	100.9%	0.9%	Surprise	4.93	0.21
Gavilan Peak	100.8%	0.8%	Raceway	4.90	0.18
Browning	100.7%	0.7%	Yavapai	4.82	0.1
Jojoba	100.7%	0.7%	Casa Grande	4.75	0.03
Moonshine	100.7%	0.7%			
Case Grande	100.4%	0.4%			
Gila Bend	100.4%	0.4%			
Yavapai	100.1%	0.1%			
Avery	99.8%	-0.2%			
Raceway	99.6%	-0.4%			

The sensitivity analysis confirmed that all of the Phoenix area load included in last year's study was appropriate, but that load at Buckeye, Gila Bend, the Eastern Mining Area, and Gavilan Peak should also be included. Figure 1 shows all of these loads included for the 2005 study. Figure 2 shows, in 2008, the Phoenix area load is expanded to include loads supplied by the new bulk power substations TS5 and South East Valley (SEV). Figure 3 shows, in 2012, the Phoenix area load is expanded to include loads supplied from the bulk substation at Raceway.

**Figure 1**

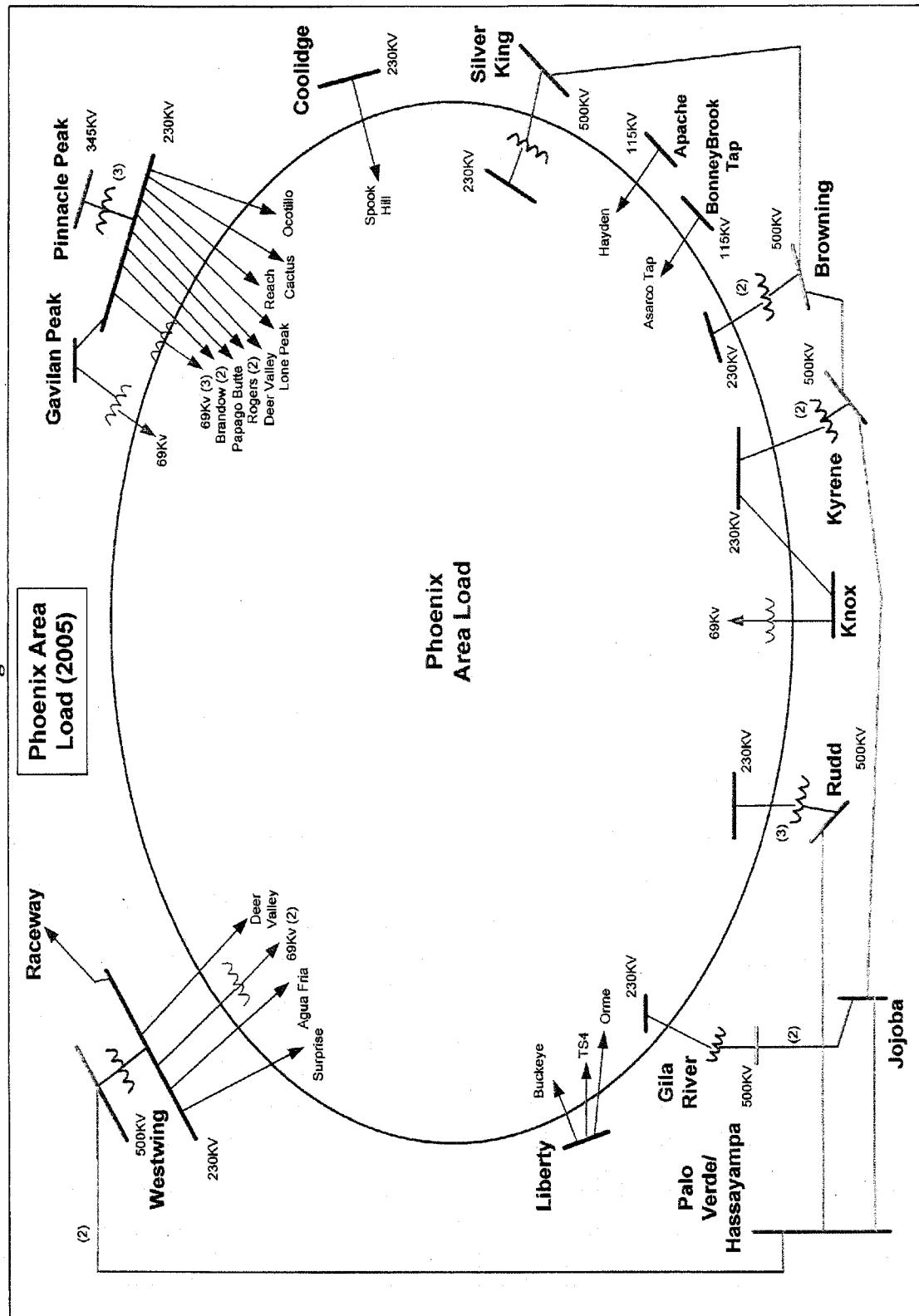
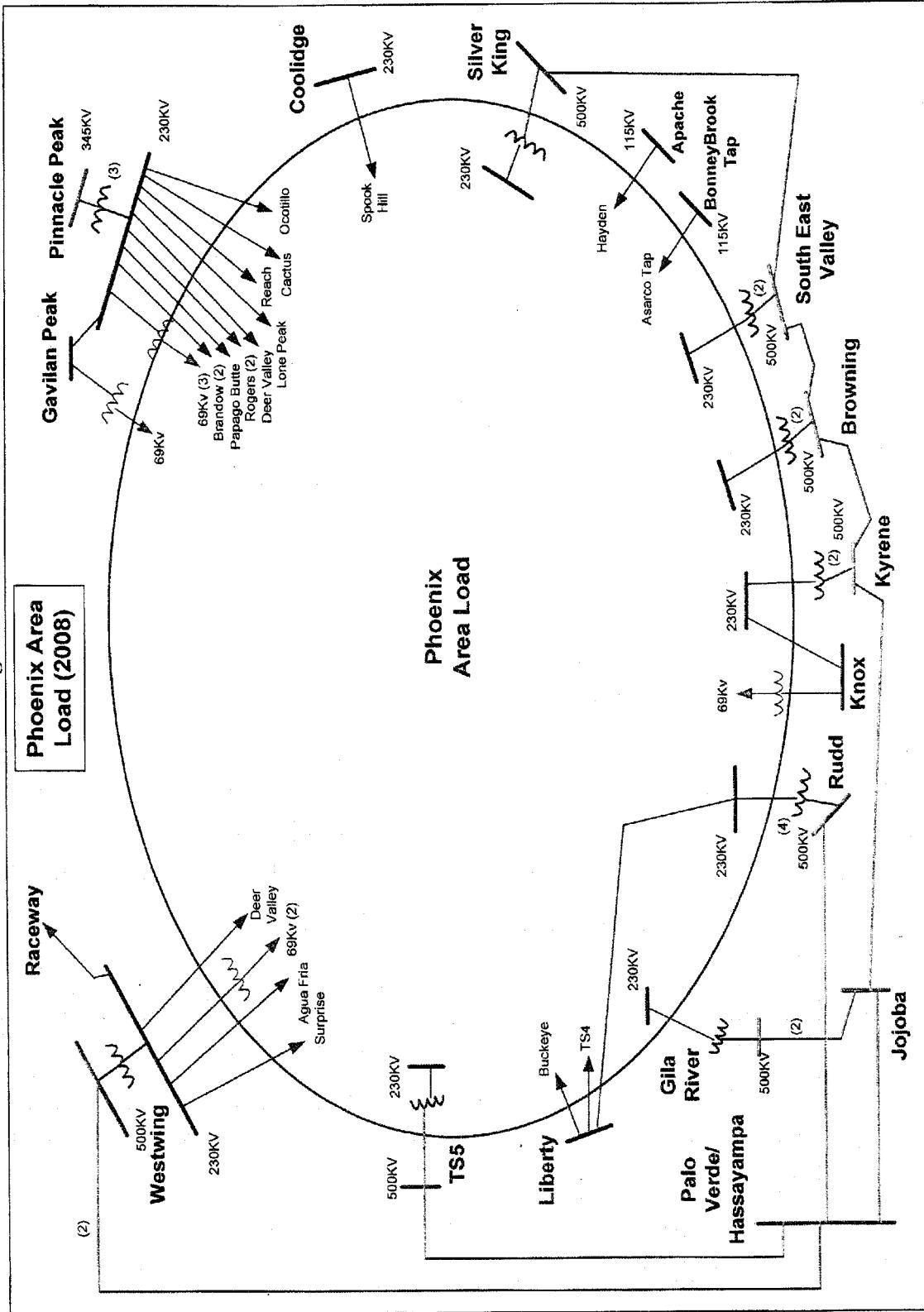
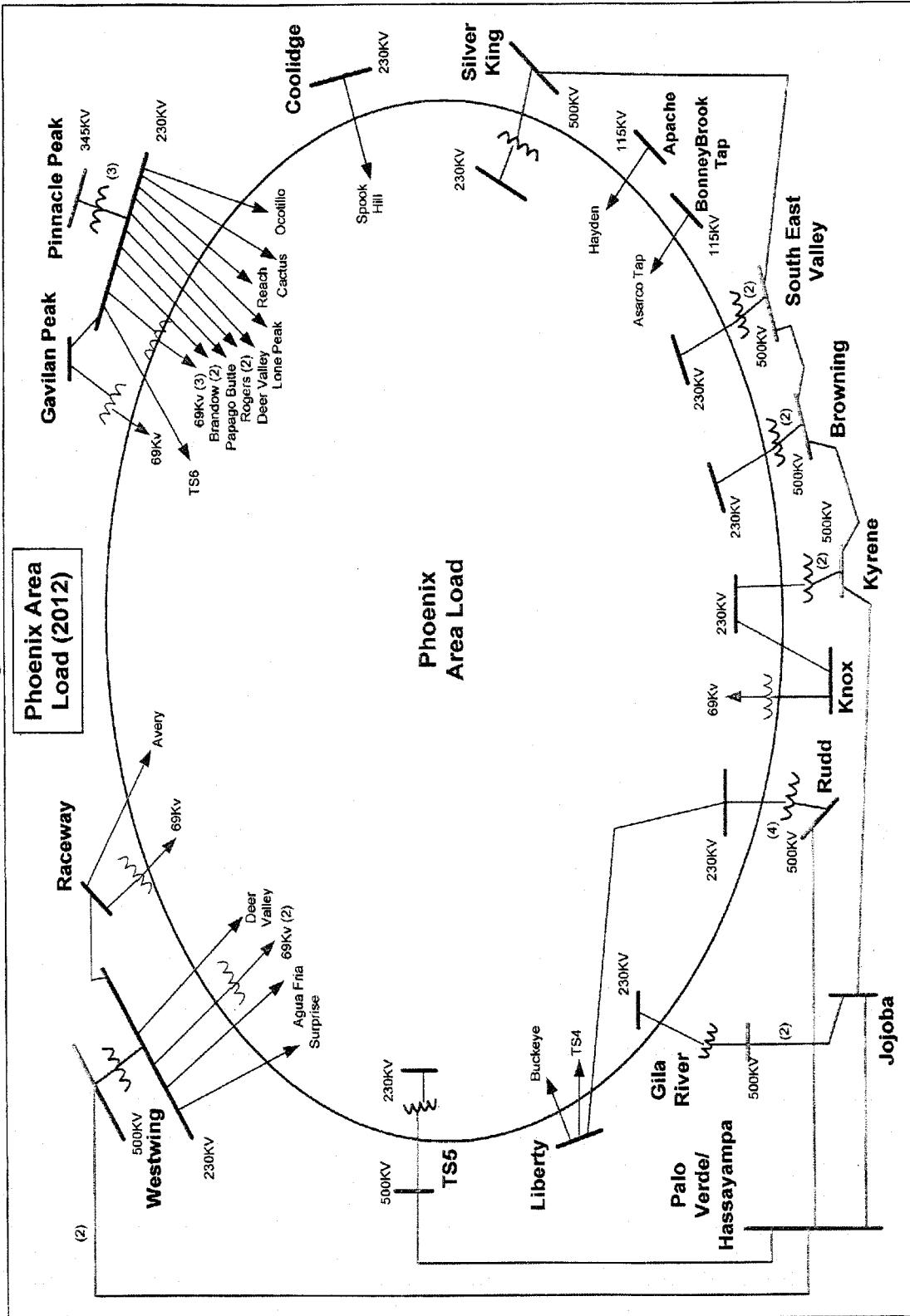


Figure 2



**Figure 3**



In performing the Phoenix area studies several planned projects were added to reflect transmission system upgrades for the next ten years. They are listed below under one of the three study years they will first appear:

**Projects in service by 2005**

- Gavilan Peak substation connected to Pinnacle Peak-Prescott 230-kV line
- Reach 2<sup>nd</sup> 230/69-kV transformer addition
- Browning 230/69-kV, 280 MVA transformer addition
- Cactus 3<sup>rd</sup> 230/69-kV transformer addition
- North Gila 2<sup>nd</sup> 500/69-kV transformer addition
- Surprise 2<sup>nd</sup> 230/69-kV transformer addition
- West Phoenix 3<sup>rd</sup> 230/69-kV transformer addition
- Thunderstone 2 new 230/69-kV, 280 MVA transformer additions
- Alexander 69-kV 46mvar capacitors addition
- Santan CC5 550 MW generation addition

**Projects in service by 2008**

- Silver King substation connected to Cholla-Saguaro 500-kV line
- South East Valley project
- A new Avery 230/69-kV substation with a 230/69-kV transformer and a 230-kV line from Raceway substation
- A new TS5 500/230-kV substation with two 500/230-kV transformers, a 500-kV line to Palo Verde area
- A new TS1 230/69-kV substation with a 230/69-kV transformer, a 230-kV line to TS5 substation
- A new TS3 230/69-kV substation with a 230/69-kV transformer, a 230-kV line to TS1 substation, and connected to Rudd-TS4 230-kV line
- Lincoln Street 2<sup>nd</sup> 230/69-kV transformer addition
- Rudd 4<sup>th</sup> 500/230-kV transformer addition
- A new Jojoba 230/69-kV substation with a 230/69-kV transformer and connected to Gila River-Liberty 230-kV line
- Santan CC6 275 MW generation addition

**Projects in service by 2012**

- A new Raceway 500-kV substation connected to Navajo-Westwing 500-kV line and a 500-kV line to TS5 substation
- A new TS2 230-kV substation with a 230/69-kV transformer and connected to TS1-TS3 230-kV line
- A new TS6 230/69-kV substation with a 230/69-kV transformer and connected to a new Avery-Pinnacle Peak 230-kV line
- Meadowbrook 2<sup>nd</sup> 230/69-kV transformer addition
- Alexander 2<sup>nd</sup> 230/69-kV transformer addition

## **B. Phoenix Area Critical Outages**

### **1. 2005**

The analysis determined that the critical single contingency for the Phoenix load area with less than 1400 MW of local Phoenix area generation is the loss of the Jojoba-to-Kyrene 500-kV transmission line. The loss of this major 500-kV line to the Phoenix area results in significantly higher flows on the remaining transmission lines and causes a large increase in reactive power (Var) losses in the transmission network. The increase in Var consumption results in insufficient Vars for voltage support in the load area. Consequently, this condition creates low voltages in the system and makes the area deficient in reactive power. The system is constrained by voltage instability, with local Phoenix area generation below 1400 MW. With local Phoenix area generation above 1400 MW, the critical single contingency for the Phoenix load area is also the loss of the Jojoba-to-Kyrene 500-kV transmission line. But, with at least 1400 MW of local generation on-line, the loss of the line results in a thermal overload of the Rudd-to-Orme 230-kV transmission line. Thus, the system is constrained by this thermal overload when local Phoenix area generation is above 1400 MW.

### **2. 2008**

The analysis determined that the critical single contingency for the Phoenix load area with less than 1600 MW of local Phoenix area generation is the loss of the Jojoba-to-Kyrene 500-kV transmission line. The loss of this major 500-kV line to the Phoenix area results in significantly higher flows on the remaining transmission lines and causes a large increase in reactive power (Var) losses in the transmission network. The increase in Var consumption results in insufficient Vars for voltage support in the load area. Consequently, this condition creates low voltages in the system and makes the area deficient in reactive power. The system is constrained by voltage instability, with local Phoenix area generation below 1600 MW. With local Phoenix area generation above 1600 MW, the critical single contingency for the Phoenix load area is the loss of the Agua Fria-to-Glendale 230-kV transmission line. With at least 1600 MW of local generation on-line, the loss of the Agua Fria-to-Glendale 230-kV transmission line results in a thermal overload of the West Phoenix-to-Lincoln Street 230-kV transmission line. Thus, the system is constrained by this thermal overload when local Phoenix area generation is above 1600 MW.

### **3. 2012**

The analysis determined that the critical single contingency for the Phoenix load area at all load and generation levels is the loss of the Palo Verde-to-Rudd 500-kV transmission line. The loss of this major 500-kV line results in significantly higher flows on the underlying 230-kV transmission system and causes a thermal overload on the Westwing-to-Surprise 230-kV transmission line. Thus, the system is constrained by this thermal overload for the loss of the Palo Verde-to-Rudd 500-kV transmission line.

The voltage stability analysis was performed using Q-V analysis on the most reactive deficient buses in the Phoenix area. These buses were the Kyrene 500-kV, Kyrene 230-kV, Browning 230-kV, Westwing 230-kV, and the Pinnacle Peak 230-kV buses.

Q-V analysis is performed by adding reactive load at the critical bus until the voltage reaches a minimum value which indicates potential voltage instability. The import limit is determined as the lesser of 95% of the import with zero reactive margin or 100% of the import with a 5% voltage drop following the worst single-contingency per WECC planning criteria.

### C. Phoenix Area – SIL for 2005, 2008, and 2012

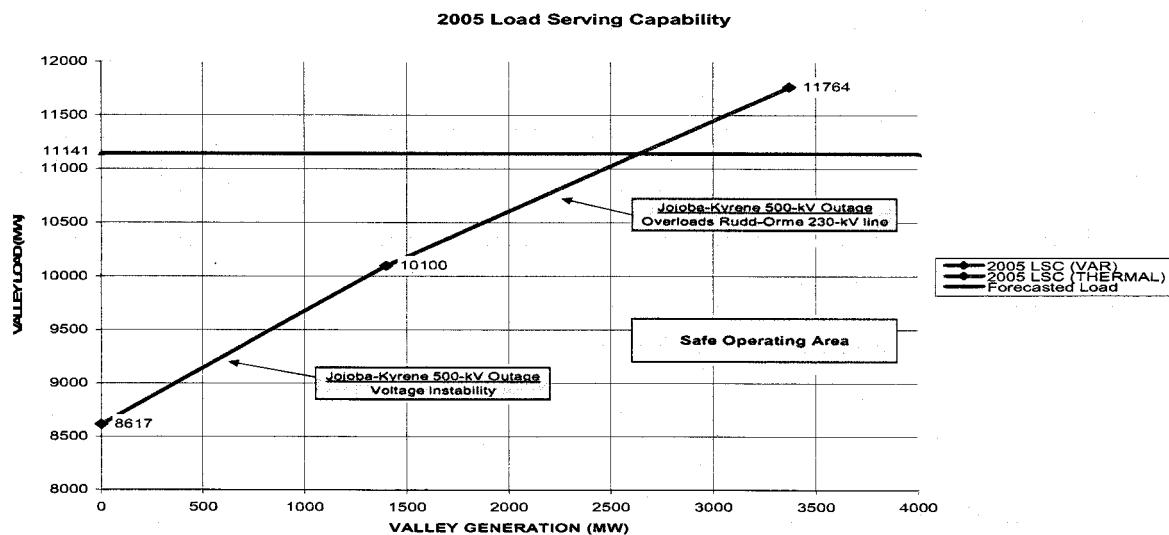
Analysis of the Phoenix area transmission network resulted in area import limits based on the limits discussed above. Operation of the Phoenix system within these limits ensures that the area does not experience voltage instability or thermal overloading of a system element after a critical contingency. Voltage instability is characterized by a progressive fall in voltage magnitude at a particular location of the power system that may spread throughout the network causing a complete area voltage collapse and blackout. A thermal overload occurs when more power flows through an element than the emergency rating of that element. The Phoenix area SIL for the years 2005, 2008, and 2012 are outlined in Table 2.

**Table 2**  
**2005, 2008, and 2012 Phoenix area Simultaneous Import Limit**

Year	SIL (MW)
2005	8,617
2008	10,511
2012	11,103

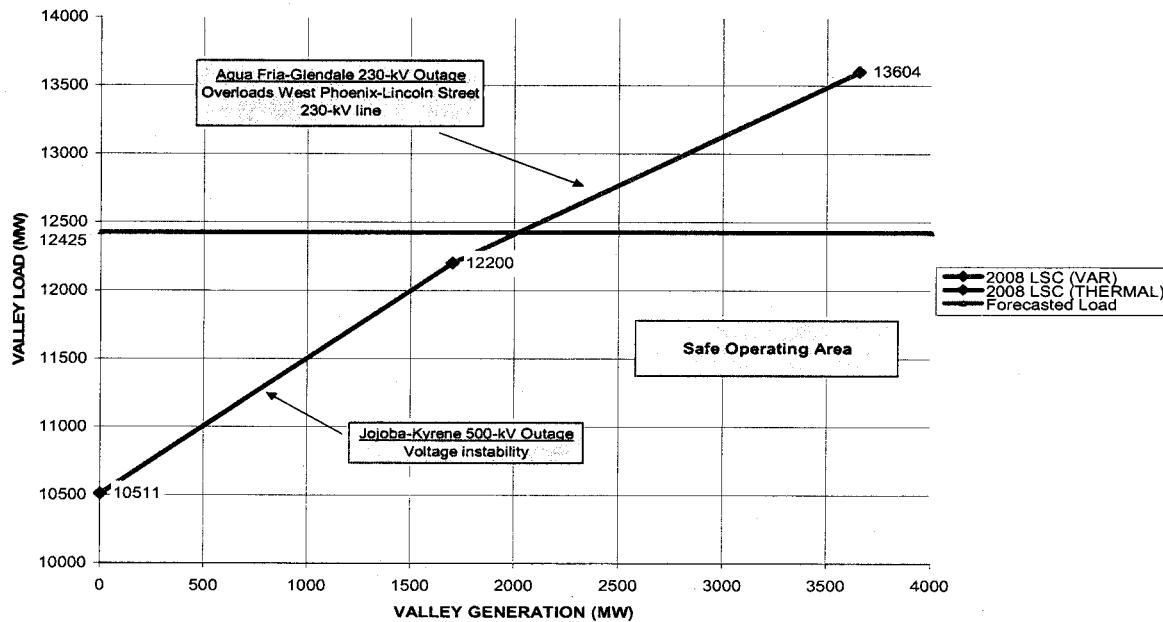
The maximum Phoenix area load-serving capability for various generation levels is shown in Figures 4, 5, and 6.

**Figure 4**



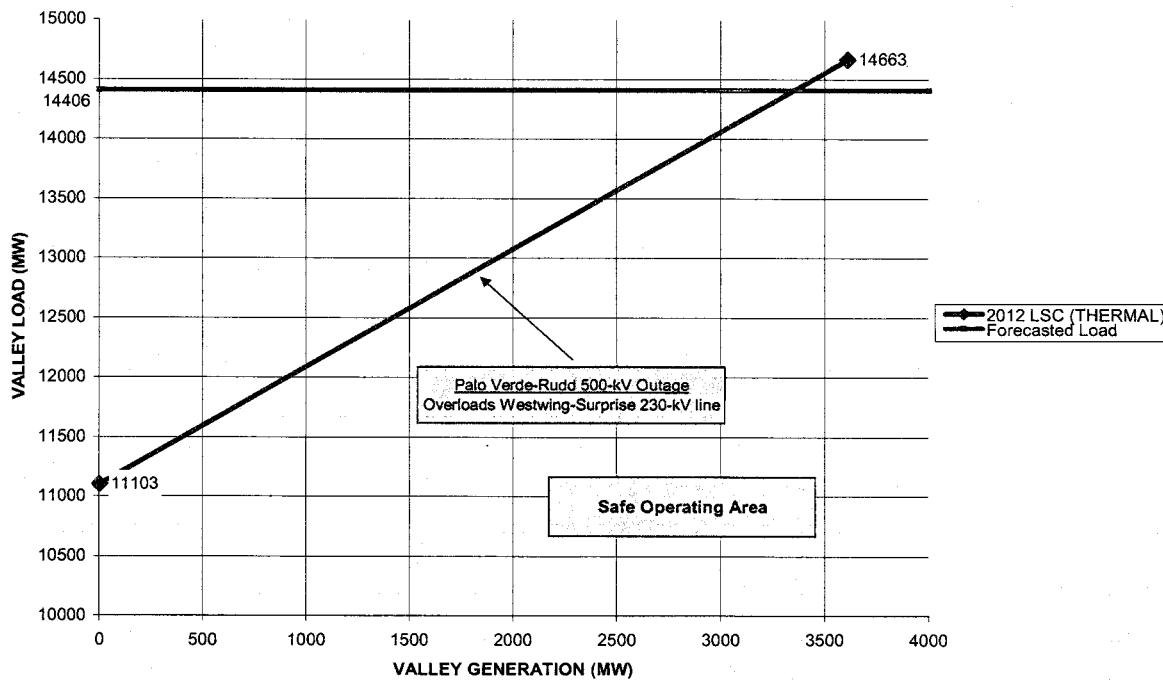
**Figure 5**

**2008 Load Serving Capability**



**Figure 6**

**2012 Load Serving Capability**



#### D. Generation Sensitivities

Sensitivity analyses of generation impact on load-serving capability were also conducted. These sensitivities were done with the maximum level of local generation. The following tables provide the results of these analyses for units that are both within and outside the Phoenix area.

Generation sensitivities inside the Phoenix area are listed in Table 3.

**Table 3**  
**Generation Sensitivities Inside Phoenix**

<b>Generation Source Increase by 100 MW</b>	<b>2005 Load Serving Capability Increase (MW)</b>	<b>2008 Load Serving Capability Increase (MW)</b>	<b>2012 Load Serving Capability Increase (MW)</b>
Agua Fria Generation	25	0	115
Kyrene Generation	170	56	58
Ocotillo Generation	62	257	83
Santan Generation	144	50	61
West Phoenix Generation	12	0	117

Generation sensitivities outside of the Phoenix Metro area are listed in Table 4.

**Table 4**  
**Generation Sensitivities Outside Phoenix**

<b>Generation Source Increase by 100 MW</b>	<b>2005 Load Serving Capability Increase (MW)</b>	<b>2008 Load Serving Capability Increase (MW)</b>	<b>2012 Load Serving Capability Increase (MW)</b>
Sundance Generation	94	26	54
Desert Basin Generation	114	28	32
Hassayampa Area Generation	0	0	0
Panda Gila River Generation	0	0	11

The results indicate that the effectiveness of a generator is dependant upon the critical outage, whether the limitation is thermal or voltage, the critical element, and the location of the generator in respect to the direction the power is flowing through the critical element. For example, in 2005 with the critical outage being the Jojoba-Kyrene 500-kV line and the critical element being

the Rudd-Orme 230-kV line, the generators that will allow the load-serving capability to increase the greatest are those that inject their power to the east of the Orme substation. And, in 2008, with the critical outage being the Agua Fria-Glendale 230-kV line and the critical element being the West Phoenix-Lincoln Street 230-kV line, because they inject power east of Lincoln Street the Ocotillo generators are most effective in increasing the load-serving capability. In contrast, with the West Phoenix generators injecting power immediately upstream of the critical element, they will be least effective in increasing the load-serving capability.

#### IV. YUMA AREA

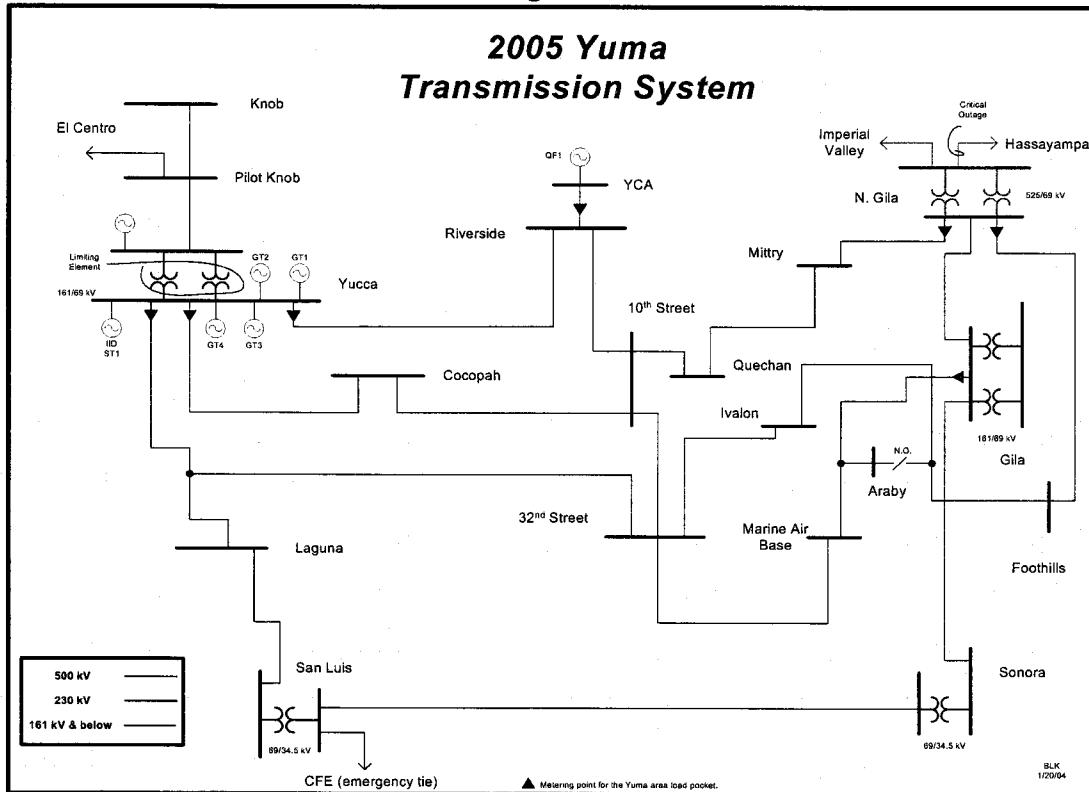
##### A. Description of Yuma Area

Currently the Yuma area is served from three transmission sources:

- APS' North Gila 500/69-kV substation, which is located east of Yuma. Two 69-kV lines extend west and southwest from this substation into Yuma to serve Yuma area load. A third 69-kV line interconnects into WAPA's Gila substation.
- WAPA's Gila 161/69-kV station, which is also located east of Yuma. From this station, APS has one 69-kV line into the Yuma load area and one 69-kV tie to APS' North Gila substation.
- APS' Yucca 69-kV station, which is located on the west side of Yuma near the Colorado River. APS' local generation is located at this station, along with three 69-kV lines into the load area and an interconnection to IID's 161-kV system through two 161/69-kV transformers. The IID 75 MW steam-generating unit is also located at this substation.

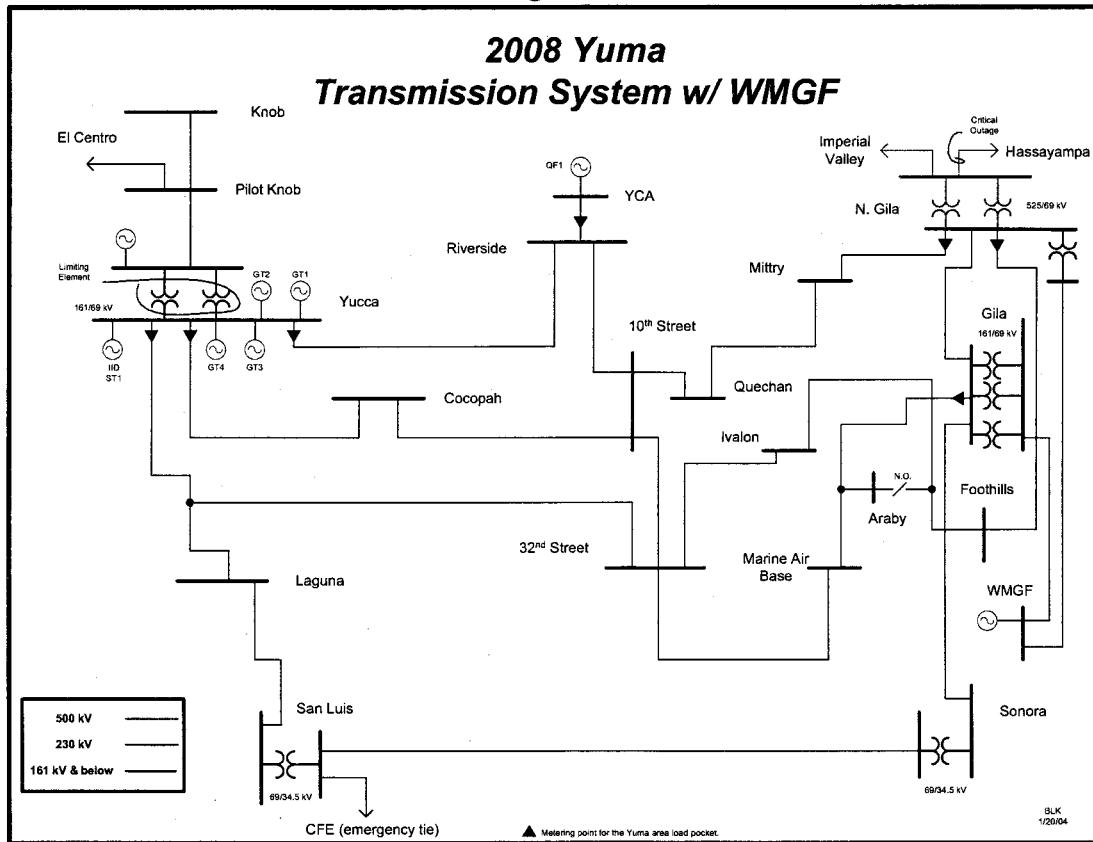
Figure 7 shows the transmission system in 2005 and the metering points for the Yuma area load pocket. The second North Gila 500/69-kV transformer is planned in 2005 as a result of the 2003 RMR study.

Figure 7



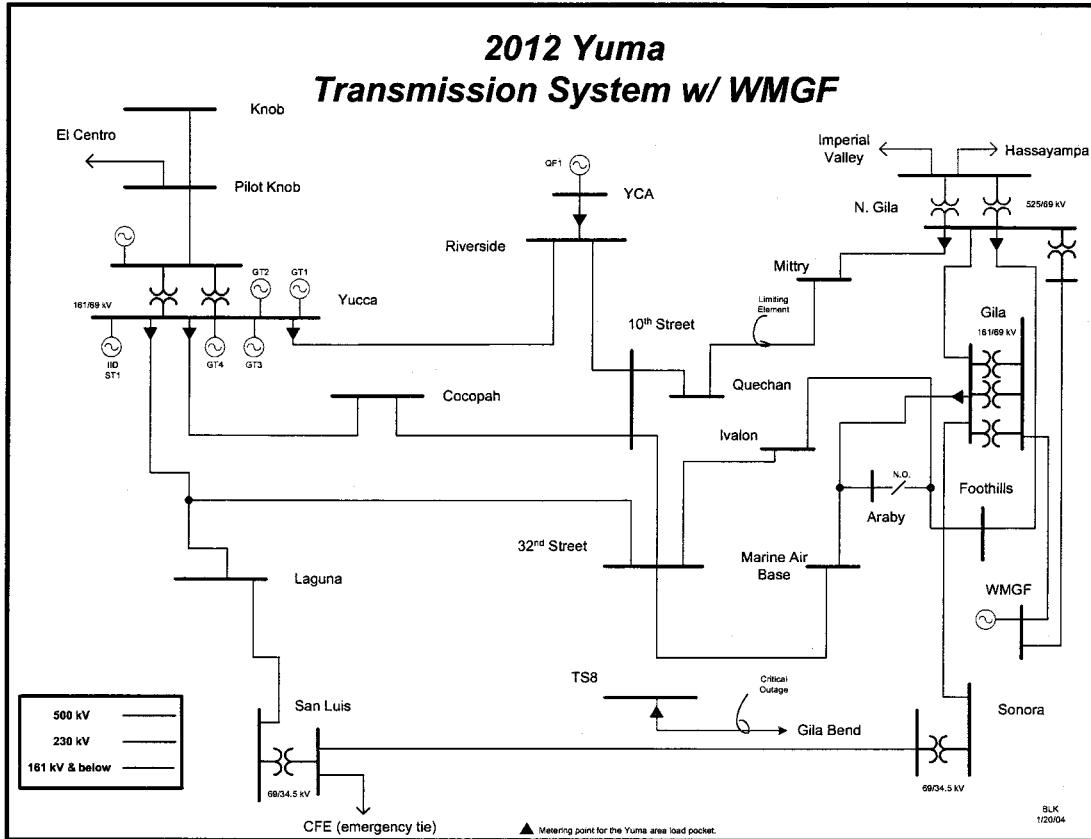
The Welton-Mohawk interconnection facilities and generators, which are planned for 2006, were modeled in the 2008 case. The interconnection facilities will consist of a 161-kV line and a third 161/69-kV transformer to WAPA's Gila substation, along with a 161-kV line and 161/69-kV to APS' North Gila 69-kV substation. These facilities can be seen below in Figure 8.

**Figure 8**



The only change in the model of the Yuma area for 2012 was the addition of the 230-kV line from Gila Bend to the Yuma area. The specific Yuma termination for this line has not yet been determined and for the 2012 analysis it was assumed to be interconnected to the 32<sup>nd</sup> Street substation. This can be seen in Figure 9.

**Figure 9**



### B. Yuma Area Critical Outages

Several critical contingencies exist affecting the determination of the system import limit for the Yuma area during the 2004-2013 time frame. For the 2004-2011 time frame, these include the Hassayampa-N.Gila 500-kV line, the Yucca-Laguna tap 69-kV line, and the N. Gila-Gila 69-kV line. In 2012 and beyond, the loss of the new TS8-Gila Bend 230-kV line also becomes a critical contingency.

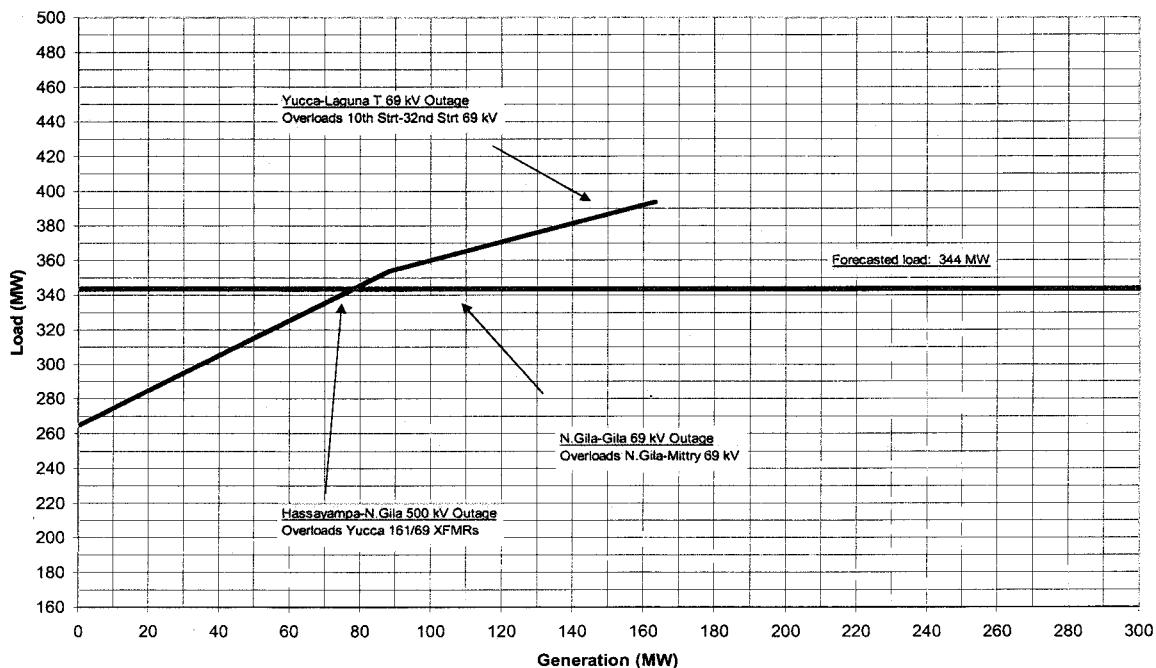
A loss of the Hassayampa-N.Gila 500-kV line typically overloads the Yucca 161/69-kV transformers, while the N.Gila-Gila 69-kV outage results in overloading the N.Gila-Mittry 69-kV line or the Mittry-Quechan 69-kV line. An outage of the Yucca-Laguna tap 69-kV line causes an overload on the Riverside-10<sup>th</sup> Street 69-kV line. In 2012, a loss of the Gila Bend-TS8 230-kV line causes the flows on the Mittry-Quechan 69-kV line and Yucca-Laguna tap 69-kV line to overload.

### C. Yuma Area - SIL for 2005, 2008 and 2012

With planned system additions for the Yuma area, along with some accelerated projects (see Table 2), the SIL for the Yuma area will increase each study period. For 2005, 2008, and 2012 the SIL will be 265 MW, 292 MW and 410 MW, respectively. Results of these studies are shown in Figures 10 through 12.

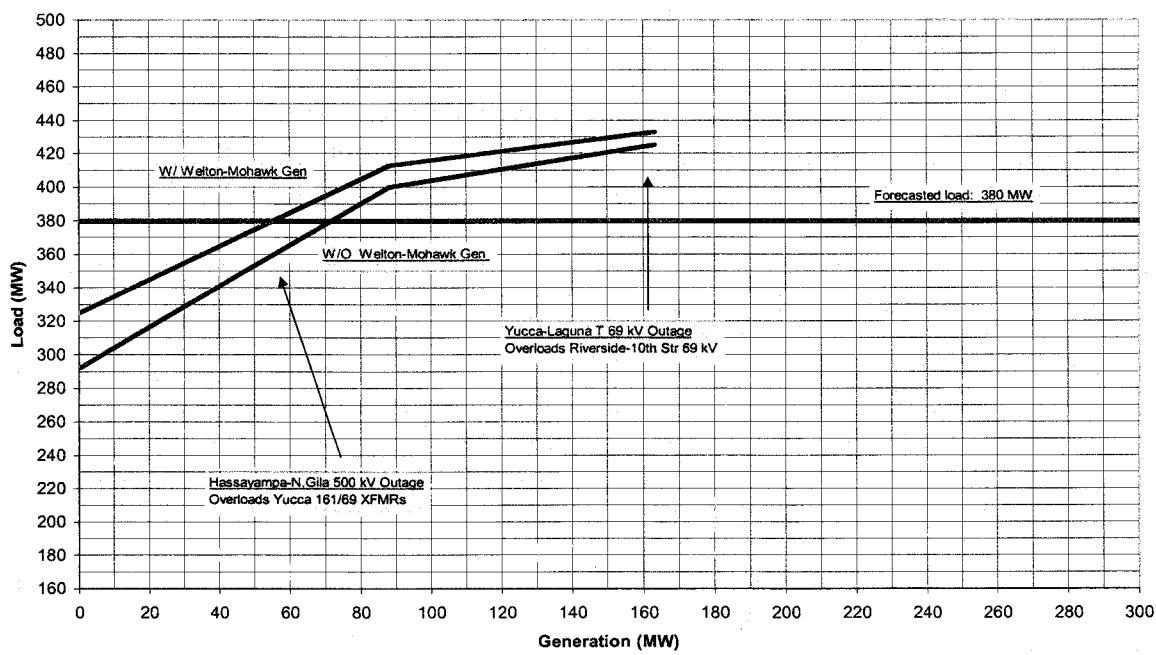
**Figure 10**

Yuma Area 2005

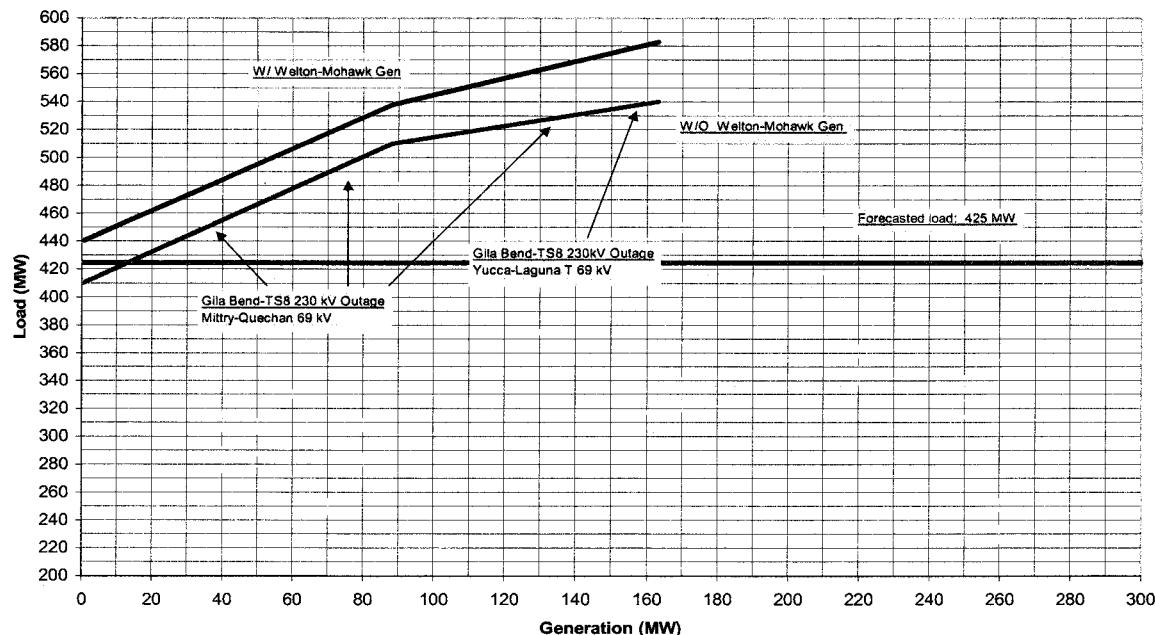


**Figure 11**

Yuma Area 2008



**Figure 12**  
**Yuma Area 2012**



Also, the load listed along the vertical axis is the sum of the entire load within the Yuma area. In performing this analysis, all previously planned projects were included in the model as well as some additional projects that were added to the sub-transmission plans. Also, several previously planned shunt capacitor banks were accelerated and several new banks were added to maximize the capability of the transmission system by ensuring that the area was not severely voltage limited. These projects are listed in Table 5.

**Table 5**  
**Yuma Projects**

Study Case	Case Description	
	System	Projects Added
2005 base case	Existing	Foothills 69-kV, 32Mvar cap banks Gila cap bank Laguna cap bank 2 <sup>nd</sup> N.Gila 500/69-kV transformer
2008 base case	2005 base case	32 <sup>nd</sup> Street-10 <sup>th</sup> Street 69-kV reconductor N.Gila-Mittry 69-kV reconductor 32 <sup>nd</sup> Street-Ivalon 69-kV reconductor
2012 base case	2008 base case	Gila Bend-TS8 230-kV line TS8 cap banks

#### **D. Generation Sensitivities**

Welton-Mohawk is a planned generating facility located east of Yuma that is scheduled for commercial operation during 2006. The net capacity of this planned facility is 310 MW. Figures 11 and 12 show import limits for the Yuma area for 2008 and 2012 with and without the Welton Mohawk plant modeled. For each of these years the case with Welton-Mohawk includes the generation modeled at full output. From Figure 12 it is seen that Yuma area import increases approximately 10 MW for each 100 MW of Welton-Mohawk generation. However, the effect of the Welton-Mohawk on Yuma import capability is somewhat less in the 2008 timeframe, as seen in Figure 11. With the Welton-Mohawk generation off-line, the interconnection facilities by themselves bring no additional import capability. The remaining generation in the Yuma area is located at or near the Yucca power plant and has equal impact on the import limit into the Yuma area.

## V. ANALYSIS OF RMR CONDITIONS

### A. Phoenix Area

#### *1. Annual RMR Conditions*

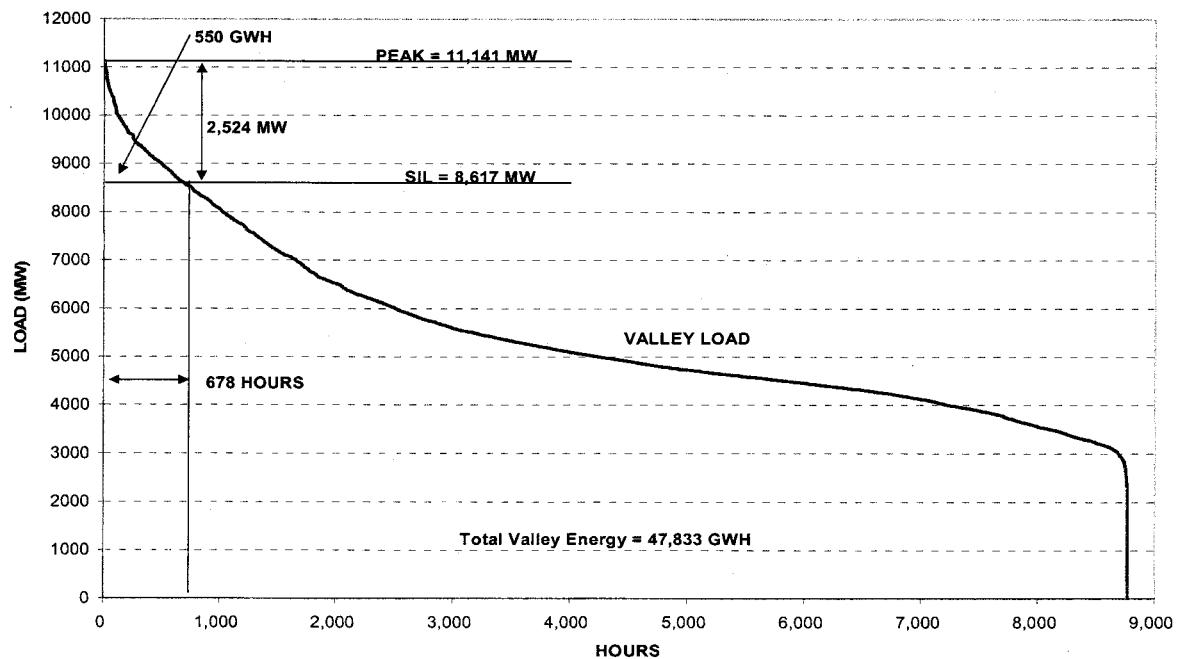
An RMR condition exists when the local load is greater than the SIL. In such cases, the RMR condition is the amount of generation that must be located inside of the constrained load area to meet the utility's peak load. RMR conditions for the Phoenix area are shown in Table 6 and are represented in the load-duration curves in Figures 13, 14, and 15.

**Table 6**

<b>Phoenix RMR Conditions Without Valley Generation</b>			
	(MW)		
	<b>PHOENIX</b>		
	<b>2005</b>	<b>2008</b>	<b>2012</b>
<b>Peak Load</b>	<b>11,141</b>	<b>12,425</b>	<b>14,406</b>
<b>Generation</b>	-	-	-
<b>Reserves</b>	-	-	-
<b>Net Valley Generation</b>	-	-	-
<b>Import Capability</b>	<b>8,617</b>	<b>10,511</b>	<b>11,103</b>
<b>Net Gen + Import</b>	<b>8,617</b>	<b>10,511</b>	<b>11,103</b>
<b>Must-Run Generation</b>	<b>2,524</b>	<b>1,914</b>	<b>3,303</b>
<b>Hours Load Exceeds Gen + Imp</b>	<b>678</b>	<b>338</b>	<b>758</b>
<b>Energy - GWH</b>	<b>550</b>	<b>222</b>	<b>805</b>
<b>Energy Percent of Valley Load</b>	<b>1.2%</b>	<b>0.4%</b>	<b>1.3%</b>

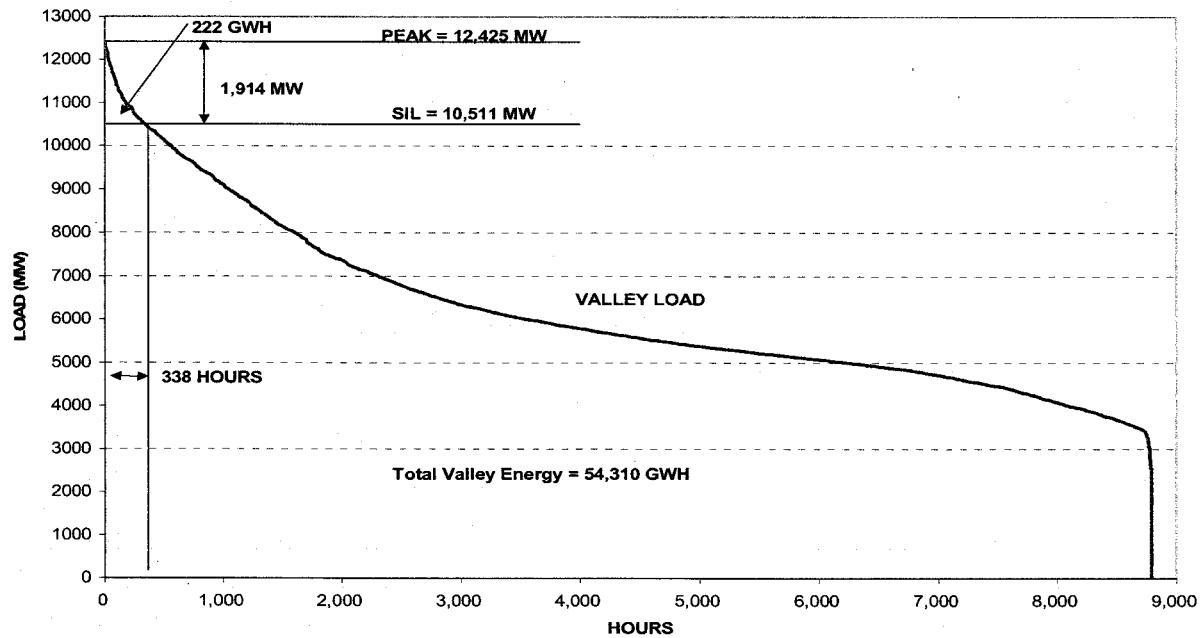
**Figure 13**

**PHOENIX LOAD DURATION & RMR CONDITION (2005)**



**Figure 14**

**PHOENIX LOAD DURATION & RMR CONDITION (2008)**



**Figure 15**

**PHOENIX LOAD DURATION & RMR CONDITION (2012)**

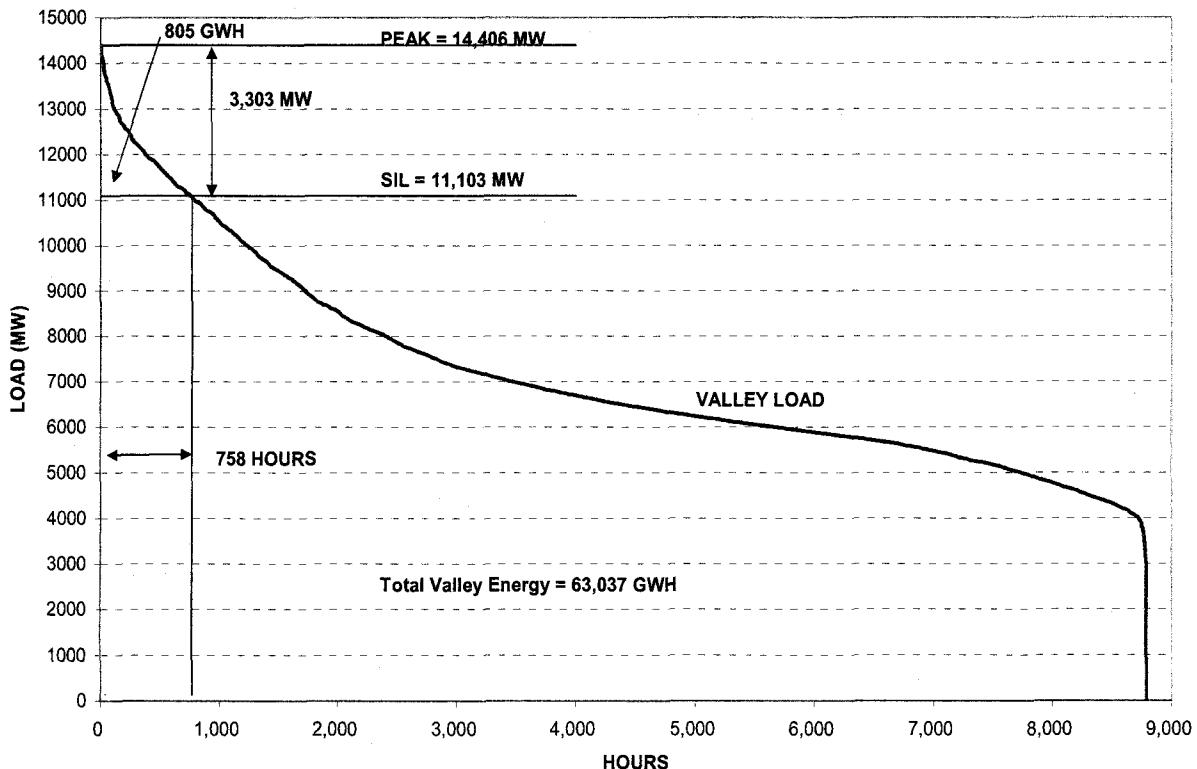


Table 6 shows that Phoenix is expected to require from 2,524 MW to 3,303 MW of local generation resources over and above its import capability to meet peak load. These resources can be located inside the Phoenix area constraint. For Phoenix, generation is estimated to be in a must-run condition for between 678 to 758 hours per year. However, because RMR occurs only at peak, the amount of associated energy is only approximately one percent of the total Phoenix area energy requirements, as shown in Figures 13, 14, and 15 above.

## 2. Maximum Load Serving Capability (MLSC)

MLSC is the maximum load that can be reliably served in the load pocket. It is the import capability plus the generation capability located inside the load pocket, minus a reserve margin allowance for generation reliability. Based on the load forecast and SIL presented in this analysis, and existing and planned local generation, the following MLSCs for Phoenix were developed. The approach used also shows how much generation or transmission may be needed to reliably meet load.

These results along with the generation and transmission assumptions are depicted in Table 7. As shown on this table, additional resources are not required in years 2005 and 2008, but in 2012, 519 MW of either additional transmission import capability or local generation is necessary to serve the Phoenix area load reliably. However, the energy associated with this capacity need is very small — 6 GWH.

**Table 7**

<b>Phoenix Area Maximum Load Serving Capability</b>			
(MW)			
<b>PHOENIX</b>			
	<u>2005</u>	<u>2008</u>	<u>2012</u>
<b>Peak Load</b>	11,141	12,425	14,406
<b>Valley Generation</b>	3,374	3,649	3,649
<b>Required Reserves</b>	(809)	(865)	(865)
<b>Net Valley Generation</b>	2,565	2,784	2,784
<b>SIL</b>	8,617	10,511	11,103
<b>MLSC</b>	11,182	13,295	13,887
<b>Projected Reserves</b>	850	1735	346
<b>Hours Load Exceeds MLSC</b>	-	-	26
<b>Energy - GWH</b>	-	-	6
<b>Energy Percent of Valley Load</b>	0.0%	0.0%	0.0%

### **3. Area Load Forecast**

The actual peak load within the Phoenix area constraint is shown in Table 8 for 1999-2003, along with projected peak load for 2005, 2008 and 2012. This peak load represents load growth as well as the expanding boundaries of the Phoenix area, as discussed in Section III, part A and shown in Figures 1, 2, and 3. Projected peak load is based on the same assumptions embodied in APS' total system load forecast used for budgeting and planning. This peak load is the load measured just inside the defined Phoenix area constraint. The peak load is net of EHV transmission losses of about 3.8 percent.

Table 8

Phoenix and Yuma Load and Energy Forecast (MW / GWH)								
	HISTORICAL					FORECAST		
	<u>1999</u>	<u>2000</u>	<u>2001</u>	<u>2002</u>	<u>2003</u>	<u>2005</u>	<u>2008</u>	<u>2012</u>
<b>PHOENIX</b>								
LOAD	7,854	8,688	9,179	9,290	9,663	11,141	12,425	14,406
ENERGY	35,232	38,711	39,654	40,426	42,140	47,833	54,310	63,037
Load Factor	51.2%	50.7%	49.3%	49.7%	49.8%	49.0%	49.8%	49.8%
<b>APS YUMA</b>								
LOAD	270	273	296	292	321	344	380	425
ENERGY	1,197	1,262	1,330	1,332	1,394	1,517	1,663	1,869
Load Factor	50.6%	52.6%	51.2%	52.0%	49.6%	50.4%	49.8%	50.0%

The Phoenix area has historically had about a 50 percent load factor. Phoenix area APS load forecasts were developed by estimating a multiple regression model using historic hourly load data, weather, and number of retail customers. These historic relationships (correlations) were used against the metro area customer forecast, and a forecast of Phoenix weather to produce the APS Phoenix area load. The same process was followed to develop the hourly forecast load for SRP. The SRP forecast was then added to the APS forecast to obtain a total valley load forecast.

#### 4. Generation

There are currently three owners of generation electrically located inside the Phoenix area — APS with 660 MW, SRP with 1,523 MW, and PWEC with 641 MW. Load serving entities (i.e., APS and SRP) own a combined total of 2,183 MW of local generation that is currently in service. Table 9 shows operational data associated with each unit.

Table 9

PHOENIX AREA GENERATION									
OWNER	PLANT	TYPE	SUMMER CAPABILITY	MINIMUM LOAD	MINIMUM UP TIME	MINIMUM DOWN TIME	FOR EFOR	FUEL TYPE	
APS	Ocotillo 1	ST	110	30	8	8	4%	6%	NG
APS	Ocotillo 2	ST	110	30	8	8	4%	6%	NG
APS	Ocotillo GT1	GT	50	4	1	8	10%	12%	NG
APS	Ocotillo GT2	GT	50	4	1	8	10%	12%	NG
APS	West Phoenix GT1	GT	50	4	1	8	10%	12%	NG
APS	West Phoenix GT2	GT	50	4	1	8	10%	12%	NG
APS	West Phoenix CC1	CC	80	30	3	8	3.5%	7%	NG
APS	West Phoenix CC2	CC	80	30	3	8	3.5%	7%	NG
APS	West Phoenix CC3	CC	80	30	3	8	3.5%	7%	NG
PWEC	West Phoenix CC4	CC	112	84	6	4	4%	4%	NG
PWEC	West Phoenix CC5	CC	529	178	4	4	8%	8%	NG
SRP	Agua Fria 1	ST	113	57	8	8	4%	6%	NG
SRP	Agua Fria 2	ST	113	57	8	8	4%	6%	NG
SRP	Agua Fria 3	ST	181	92	8	8	4%	6%	NG
SRP	Agua Fria 4	GT	73	35	1	8	10%	12%	NG
SRP	Agua Fria 5	GT	73	32	1	8	10%	12%	NG
SRP	Agua Fria 6	GT	73	32	1	8	10%	12%	NG
SRP	Crosscut HY1	HY	3	N/A	N/A	N/A	0%	0%	WAT
SRP	Kyrene 1	ST	34	14	8	8	4%	6%	NG
SRP	Kyrene 2	ST	72	29	8	8	4%	6%	NG
SRP	Kyrene GT4	GT	59	25	1	8	10%	12%	NG
SRP	Kyrene GT5	GT	53	24	1	8	10%	12%	NG
SRP	Kyrene GT6	GT	53	24	1	8	10%	12%	NG
SRP	Kyrene CC1	CC	250	161	4	4	8%	8%	NG
SRP	Santan 1	CC	92	35	3	8	3.5%	7%	NG
SRP	Santan 2	CC	92	35	3	8	3.5%	7%	NG

<b>SRP</b>	<b>Santan 3</b>	CC	92	36	3	8	3.5%	7%	NG
<b>SRP</b>	<b>Santan 4</b>	CC	92	35	3	8	3.5%	7%	NG
<b>SRP</b>	<b>Santan 5</b>	CC	550	330	4	4	8%	8%	NG
<b>SRP2</b>	<b>Santan 6</b>	CC	275	165	6	4	8%	8%	NG
<b>SRP</b>	<b>South Consolidated 1</b>	HY	1						WAT
<b>SRP</b>	<b>Transport GT1</b>	GT	4						NG
<b>PHOENIX TOTAL</b>			<b>3,649</b>						

**NOTES:**

1) Based on WECC data as of 1/1/2003

2) Santan expansion assumes an in-service date of 5/2005 (ST5) & 5/2006 (ST6)

APS owns West Phoenix CC 1-2-3, West Phoenix CT 1-2, Ocotillo ST 1-2, and Ocotillo CT 1-2. These units collectively have a 660 MW summer rating. These units have historically operated at capacity factors in the 3-30 percent range, and are expected to operate at lower capacity factors for the next few years as new high-efficiency plants come on line in Arizona and the Southwest.

SRP owns the Agua Fria, Kyrene and Santan generating stations inside the Phoenix area, totaling 1,523 MW of generation. These units were mostly built in the late 1950s to the mid-1970s. The new Kyrene CC unit went into service in 2002. SRP plans to construct another 825 MW of combined-cycle generation at the Santan plant. For this study, it is assumed the new Santan units will go into service in 2005 (Santan 5) and 2006 (Santan 6).

PWEC has constructed West Phoenix CC 4 (112 MW), which went into service in June 2001, and the West Phoenix CC 5 (529 MW) unit, which came on-line in July 2003. These units improve reliability to the Phoenix area.

### ***5. Reserves***

Reliability within a load pocket such as Phoenix must be evaluated differently than for an unconstrained system. For example, although a 15 percent reserve margin or a largest hazard margin may be adequate for unconstrained total system loads, it does not provide adequate reliability to load pockets that cannot access all reserves present in the WECC interconnected system. APS performs an analysis that considers the size, forced outage rate, and effective forced outage rate of each unit in the load pocket to determine the probability that enough generation will be available when needed. The required reserve values used for this study were based on a 99% reliability criteria. This criteria results in a reserve requirement for Phoenix of 809 MW in 2005. It means that at least 2565 MW (3374 MW Phx generation less 809 MW reserves) will be available to meet load 99% of the time. This means that if the GE MAPS simulation was run for 100 simulated years, all load would be served in 99 of them. The reserve requirement will change as resources are installed and/or retired. The reserve requirement is 865 MW once the Santan unit 6 is in-service.

The reserve values are used in calculating the load serving capability for the Phoenix load area. In addition, the loads used in this analysis are based on Phoenix experiencing average weather. If the Phoenix area has a hot summer, the load would be higher than projected, and the gas turbine and combined-cycle units' output would be reduced due to the hotter weather.

## **B. Yuma Area**

### ***1. Annual RMR Conditions***

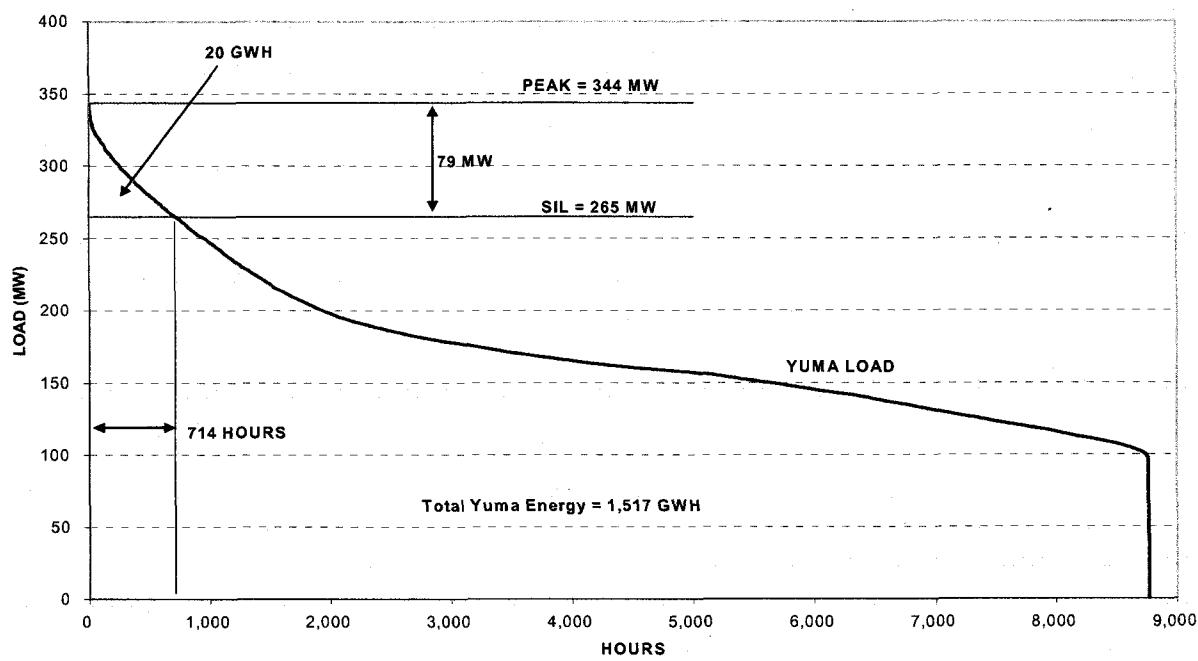
RMR conditions for the Yuma constrained area are shown in Table 10 and pictorially represented in a load-duration curve in Figures 16, 17, and 18. Table 10 shows that APS requires 88 MW (2008) of resources over and above its transmission import capability to meet peak load in Yuma. These resources can be APS-owned generation or non-APS owned generation located inside the constrained area. APS is in a must-run condition for between 714 to 12 hours per year

in Yuma and the amount of associated energy is approximately 1.0 percent of APS' total Yuma energy requirement.

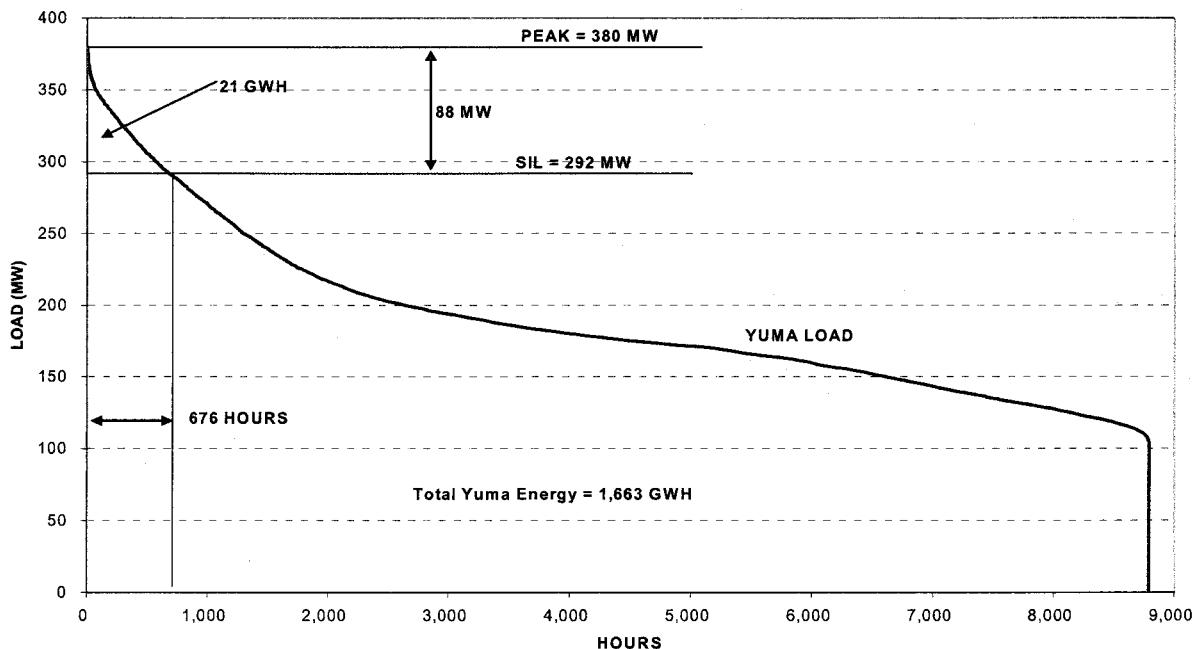
**Table 10**

<b>Yuma RMR Conditions Without Generation</b>			
	<b>(MW)</b>		
	<b>YUMA</b>		
	<b>2005</b>	<b>2008</b>	<b>2012</b>
<b>Peak Load</b>	<b>344</b>	<b>380</b>	<b>425</b>
<b>Generation</b>	-	-	-
<b>Reserves</b>	-	-	-
<b>Net Generation</b>	-	-	-
<b>Import Capability</b>	<b>265</b>	<b>292</b>	<b>410</b>
<b>Net Gen + Import</b>	<b>265</b>	<b>292</b>	<b>410</b>
<b>Must-Run Generation</b>	<b>79</b>	<b>88</b>	<b>15</b>
<b>Hours Load Exceeds Gen + Imp</b>	<b>714</b>	<b>676</b>	<b>12</b>
<b>Energy - GWH</b>	<b>20</b>	<b>21</b>	<b>0</b>
<b>Energy Percent of Yuma Load</b>	<b>1.3%</b>	<b>1.2%</b>	<b>0.0%</b>

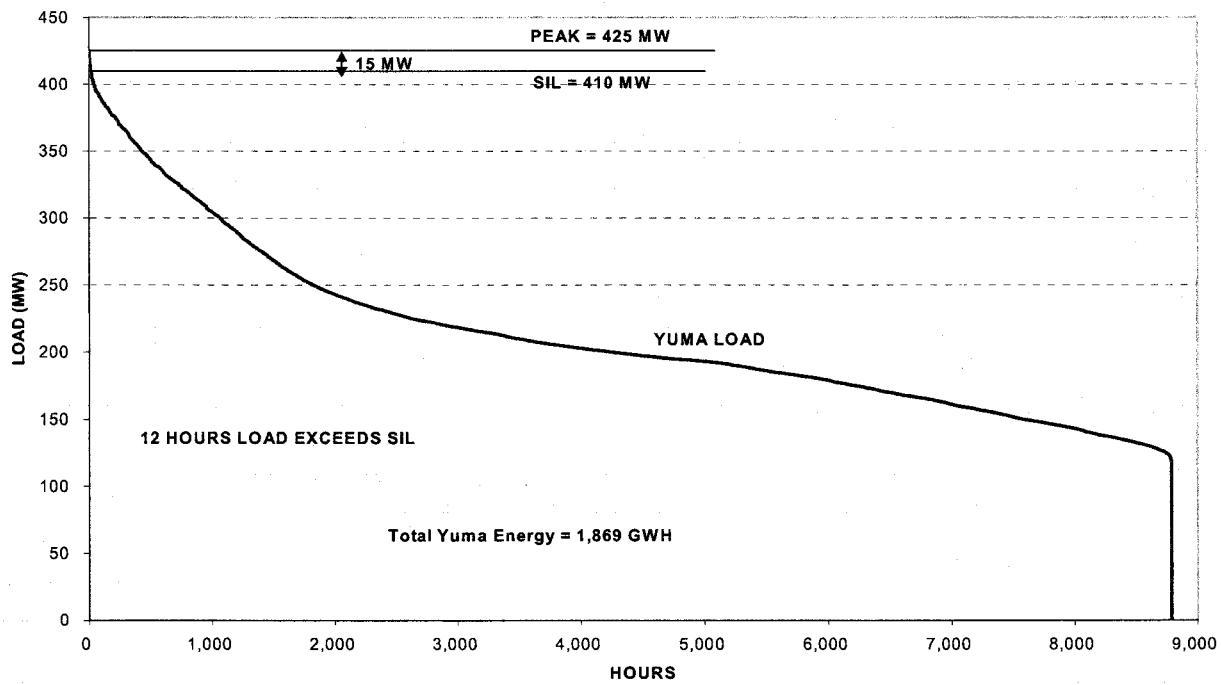
**Figure 16**  
**YUMA LOAD DURATION & RMR CONDITION (2005)**



**Figure 17**  
**YUMA LOAD DURATION & RMR CONDITION (2008)**



**Figure 18**  
**YUMA LOAD DURATION & RMR CONDITION (2012)**



## 2. Maximum Load Serving Capability (MLSC)

Based on the load forecast and SIL presented in this report, and the 267 MW of local generation, the following MLSCs were developed. This approach also shows how much generation or transmission may be needed to reliably meet load. As shown in Table 11, from 2005 to 2012 APS could serve 394 to 539 MW of load without additional resources. With a load forecast of between 344 MW to 425 MW, this resource need can be met from non-APS owned generation (Yucca steam and YCA units) within the load pocket. Also, when the Yucca steam and YCA units are running, APS' requirement for generation inside the load pocket is reduced on a one-for-one basis.

Table 11

Yuma Area Maximum Load Serving Capability			
	(MW)		
	YUMA		
	<u>2005</u>	<u>2008</u>	<u>2012</u>
<b>Peak Load</b>	<b>344</b>	<b>380</b>	<b>425</b>
<b>Local Generation</b>	<b>267</b>	<b>267</b>	<b>267</b>
<b>Required Reserves</b>	<b>(138)</b>	<b>(138)</b>	<b>(138)</b>
<b>Net Local Generation</b>	<b>129</b>	<b>129</b>	<b>129</b>
<b>SIL</b>	<b>265</b>	<b>292</b>	<b>410</b>
<b>MLSC</b>	<b>394</b>	<b>421</b>	<b>539</b>
<b>Projected Reserves</b>	<b>188</b>	<b>179</b>	<b>252</b>
<b>Hours Load Exceeds MLSC</b>	-	-	-
<b>Energy - GWH</b>	-	-	-
<b>Energy Percent of Yuma Load</b>	<b>0.0%</b>	<b>0.0%</b>	<b>0.0%</b>

## 3. Area Load Forecast

Table 8 shows APS' Yuma peak load for 1999-2003, and projected peak for 2005, 2008 and 2012. Projected peak is based on the same assumptions used in APS' total system load forecast used for budgeting and planning. This peak is the load measured just inside the Yuma area. It is net of EHV transmission losses of about 3.8 percent. Yuma load represents approximately 5 percent of APS' total system load. Yuma has historically had a slightly higher load factor than that of the Phoenix area — 52 percent compared to 50 percent. Yuma area APS load forecasts were developed by estimating a multiple regression model using historic hourly load data, weather, and number of retail customers. These historic relationships (correlations) were used

against the Yuma area customer forecast, and a forecast of Yuma weather to produce the Yuma area load.

#### *4. Generation*

APS, IID and YCA own generation inside the Yuma load pocket. These plants have a summer capacity rating of 267 MW. Five of the six units run on natural gas while the other plant (Yucca CT 4) runs on oil. Additional power plant data for this generation is provided in Table 12. Of these plants, only the combustion turbines are owned by APS.

Although operated by APS, IID dispatches its steam plant to meet its load and spinning reserve needs. YCA is a cogeneration plant that has a contract with San Diego Gas & Electric (SDG&E). Although APS has no dispatch rights to these units, whenever the units are running they provide internal generation in the Yuma area for purposes of using the import nomogram.

**Table 12**

YUMA AREA GENERATION										
<u>OPERATOR</u>	<u>PLANT</u>	<u>TYPE</u>	<u>SUMMER CAPABILITY<sup>1</sup></u>	<u>MINIMUM LOAD</u>	<u>MINIMUM UP TIME</u>	<u>MINIMUM DOWN TIME</u>	<u>FOR</u>	<u>EFOR</u>	<u>FUEL TYPE</u>	
APS	Yucca GT1	GT	18	2	1	2	10%	10%	NG	
APS	Yucca GT2	GT	18	2	1	2	10%	10%	NG	
APS	Yucca GT3	GT	52	5	1	2	10%	10%	NG	
APS	Yucca GT4	GT	51	5	1	2	10%	10%	FO2	
APS SUBTOTAL			139							
IID	Yuma Axis 1	ST	75	18	8	8	4%	6%	NG	
YCA	Yuma Cogen 1	CC	36	14	N/A	N/A	3.5%	7%	NG	
YCA	Yuma Cogen 2	CC	17	7	N/A	N/A	3.5%	7%	NG	
YCA SUBTOTAL			53							
YUMA TOTAL			267							

NOTES: 1) Based on WECC data as of 1/1/2003

#### *5. Reserves*

Using a probabilistic generation analysis, the reserve margin for Yuma was calculated to be 138 MW.

## **VI. ECONOMIC ANALYSIS OF RMR**

### **A. Introduction**

To consider potential economic effects resulting from using local generation or arising from RMR conditions, an economic analysis was performed using a regional dispatch model. For this economic analysis, the production cost of meeting Phoenix loads was determined with the existing transmission import limitations in place. Next, a second hypothetical case was built in which the transmission import limits were removed. Comparing the two cases shows the economic costs of the transmission constraint.

These two cases were simulated with GE MAPS and their outputs were compared to determine the cost of transmission constraints. GE MAPS is a detailed regional production-costing model that includes the generation and transmission system of the entire WECC. GE MAPS dispatches all generators on an economic basis to meet the overall WECC system load within constraints for individual system control area's reserve requirements and within transmission constraints. The GE MAPS model also shows sales of economic generation to, and economic purchases from, other utilities in the region subject to regional transmission constraints.

Much of the data used in modeling comes from public sources, however some of GE MAPS assumptions have been developed by APS and can be found in Appendix A. The GE MAPS database on existing generation was initially developed by several utilities in the West in the early 1990s to evaluate the economics of interregional transmission projects. It has been enhanced by the WECC in the mid-1990s and, like many other users of the model, APS continues to enhance it to reflect system improvements and resources. This model includes all new generation expected to be built in the West, including the plants under construction or in operation near Hassayampa.

The transmission modelings in GE MAPS are based on the WECC's bulk power flow cases, and were updated to reflect expected system enhancements for 2005, 2008, and 2012. Transmission modeling of Yuma was enhanced by APS to accurately model the transmission constraints in that load pocket, based on APS' operational experience. The transmission model is an electrical flow model as opposed to a transport model. That means that transmission flows are subject to physical electrical constraints as well as scheduling constraints. Electrical constraints of the system are based on the WECC's path rating catalog, with additional local constraints such as the Phoenix import constraints. A description of GE MAPS (Appendix B) as well as some of its output is provided in Appendices C and D to this report.

The following items were quantified based on the GE MAPS simulations:

- Number of hours per year the Phoenix and Yuma area transmission system is expected to be constrained by the import limits;
- Phoenix and Yuma generation capacity factors;
- Cost to serve the Phoenix system, including fuel, variable O&M, purchase power cost and wholesale interchange sales margins; and

- Phoenix and Yuma generation emissions.

West Phoenix CC 4 and 5 and Santan CC 5 and 6 were included in the simulation. When the new combined cycles are operating, whether they are producing power for APS, SRP, or another entity, they mitigate must-run conditions in the Phoenix area because the plants are electrically located inside the Phoenix area constraint. Thus, if these units are scheduled outside the Phoenix area, a like-amount of power can be counter-scheduled back into the Phoenix area without affecting the transmission import limits. Due to the high efficiency of new combined cycle units, it is anticipated that older existing generation within the Phoenix area will operate less than it has historically. This older existing generation, however, remains particularly valuable as inexpensive capacity reserves.

## B. Phoenix

### *1. Phoenix Imports*

Table 13 shows that under economic dispatch conditions for Phoenix area generation, Phoenix approached its transmission import limits less than 0.5% of the hours in a year.

Table 13

	IMPACT OF ELIMINATING PHOENIX IMPORT LIMITS						Difference		
	With Import Limits			Without Import Limits			(With minus Without)		
	2005	2008	2012	2005	2008	2012	2005	2008	2012
<u>Hours Limiting</u>	18	0	14	0	0	0	18	0	14
<u>Phx Plant Generation (GWH)</u>	3,330	4,808	8,164	3,323	4,808	8,163	6	0	1
<u>Phx Plant Capacity Factor</u>	11.3%	15.0%	25.5%	11.3%	15.0%	25.5%	0.0%	0.0%	0.0%
<u>Cost of Constraints (\$K)</u>							0	0	84

### *2. Operation of Phoenix area Generating Units*

Historically the Phoenix area's combined-cycle power plant capacity factors have ranged from 10 to 46 percent, with an average of about 24 percent. Capacity factors for steam-fired plants ranged from 6 to 42 percent, averaging about 15 percent. Capacity factors for simple-cycle combustion turbines ranged 0 to 22 percent, averaging about 4 percent. Historical capacity factors are shown in Table 14 by plant type for the period 1993 to 2002.

Operation of these units in 1999-2002 was higher than the historical average because the Western Interconnection and the Phoenix area both experienced high price volatility, high load growth, and few new generation resources had been added since the 1980s. With new higher-efficiency power plants coming on line, as well as the presence of the new Palo Verde-Rudd 500 kV transmission line, the older Phoenix area units are expected to run at lower capacity factors. As noted above, however, these units remain critical to maintaining Phoenix area reliability.

Even if the Phoenix area transmission import limits were totally eliminated, these older units would still be needed to economically meet summer peak loads. Elimination of the constraints has a minor impact on the capacity factors of all Phoenix area plants. Removing the transmission constraint reduces local generation by less than 6 GWH per year. Table 13 summarizes the results of the simulation analysis.

**Table 14**

<b>PHOENIX AREA POWER PLANT HISTORICAL CAPACITY FACTOR (%)</b>										
	<u>1993</u>	<u>1994</u>	<u>1995</u>	<u>1996</u>	<u>1997</u>	<u>1998</u>	<u>1999</u>	<u>2000</u>	<u>2001</u>	<u>2002</u>
<b>TOTAL PHOENIX</b>										
STEAM	6.6	6.3	6.5	6.7	7.1	10.0	21.2	26.5	42.0	14.2
COMBINED CYCLE	16.5	19.3	17.2	12.9	10.6	17.0	27.7	36.3	46.0	34.3
COMBUSTION TURBINE	0.6	0.9	0.4	0.5	1.0	1.8	2.6	5.8	21.9	4.2

### *3. Cost Impacts*

An estimate of the cost of the transmission import constraints can be determined by comparing the system cost to serve Phoenix customers with and without constraints. Costs included in the analysis are fuel, variable O&M, purchased power and wholesale sale margin credits. The results of this analysis showed no significant costs as a result of the constraint. See Table 13.

### *4. Emissions Impact*

In addition to economic modeling, the GE MAPS analysis evaluated the change in plant air emissions that would result from removing the transmission constraint. Specifically, the emission impact to the Phoenix area from removing transmission constraints and “moving” generation outside the Phoenix area was calculated. Four criteria pollutants are routinely tracked for power plants: NO<sub>x</sub>, CO, VOCs and PM<sub>10</sub>. Maricopa County is a non-attainment area for CO and PM<sub>10</sub>. NO<sub>x</sub> and VOCs are precursors for ozone and therefore are included.

The emissions impact from power plant emissions in the Phoenix area was estimated by using the average emission rates of normal operation (such as starts-and-stops, short run times) of APS Phoenix area units along with the modeled change in energy production. Emissions were also estimated for the other non-APS Phoenix area units. Changes in emissions resulting from entirely

eliminating the transmission import constraint into Phoenix are shown in Table 15. For comparison purposes, total emissions in Maricopa County were estimated by Maricopa County Environmental Services Department for 1999. Their emissions estimates include all stationary point sources, area sources, non-road mobile sources and on-road mobile and biogenic sources. To put the results into perspective, changes in Phoenix area power plant emissions are shown as a percentage of total Maricopa County emissions.

**Table 15**  
**Phoenix Area Air Emissions Reduction**

Pollutant	Reduction <sup>1</sup> (tons/year)	Reduction of Phoenix Area Emissions (% of total emissions from all sources)
VOC	0.0	0.000
NO <sub>x</sub>	4.0	0.007
CO	1.0	0.000
PM <sub>10</sub>	0.0	0.000 <sup>2</sup>

<sup>1</sup>2005 results, impact for 2008 and 2012 is negligible

<sup>2</sup>Reduction % is based on 1994 actual emissions.

Table 16 shows APS and Phoenix area emissions by type.

**Table 16**

PHOENIX POWER PLANT EMISSIONS (TONS)						Difference (With minus Without)			
	With Import Limits			Without Import Limits			2005	2008	2012
	2005	2008	2012	2005	2008	2012			
<u>NOx</u>	245	339	698	241	339	696	4	0	2
<u>CO</u>	68	101	187	67	101	186	1	0	1
<u>PM<sub>10</sub></u>	85	124	214	85	124	214	0	0	0
<u>VOC</u>	31	45	79	31	45	79	0	0	0

## C. Yuma

### *1. Yuma Imports*

Transmission imports to the Yuma load pocket are provided in Appendix D. Unlike the Phoenix area, these imports do approach their limits at various times throughout the year. These plots are included in Appendix D for the cases in which the limits were removed.

Table 17 shows that APS could approach its import limits for 336 hours per year. The energy associated with these hours amounts to 8 GWH. During these hours, it would have been more economical to import cheaper power either generated on APS own units outside the Yuma area or purchased from the wholesale market if the import limits were increased.

Table 17

IMPACT OF ELIMINATING YUMA IMPORT LIMITS									
	With Import Limits			Without Import Limits			Difference (With minus Without)		
	2005	2008	2012	2005	2008	2012	2005	2008	2012
<u>Hours Limiting</u>	336	2	0	0	0	0	336	2	0
<u>Yuma Generation (GWH)</u>									
APS	8	0	0	0	0	0	8	0	0
Yuma	30	25	23	22	25	23	8	0	0
<u>Yuma Plant Capacity Factor</u>									
APS	0.6%	0.0%	0.1%	0.0%	0.0%	0.1%	0.6%	0.0%	0.0%
Yuma	1.6%	1.3%	1.2%	1.2%	1.3%	1.2%	0.4%	0.0%	0.0%
<u>Cost of Constraints (\$K)</u>									
APS							500	0	0

### *2. Operation of Yuma Units*

Historically, the Yucca CTs have operated at capacity factors of between 0.5 up to 18 percent, as shown in Table 18. On average they are in the 1 to 2 percent range.

Table 18

	<u>1993</u>	<u>1994</u>	<u>1995</u>	<u>1996</u>	<u>1997</u>	<u>1998</u>	<u>1999</u>	<u>2000</u>	<u>2001</u>	<u>2002</u>
<b>YUCCA</b>										
CT1	0.3	0.6	0.4	0.4	1.1	1.5	1.4	5.0	23.4	4.0
CT2	0.4	0.4	0.5	0.4	1.2	1.5	1.4	6.9	21.8	4.6
CT3	1.5	1.4	1.0	1.4	2.8	3.6	3.5	12.2	22.0	14.4
CT4	0.0	0.2	0.0	0.2	0.2	0.7	0.3	4.8	11.9	0.3
<b>Total Yucca</b>	<b>0.7</b>	<b>0.7</b>	<b>0.5</b>	<b>0.7</b>	<b>1.4</b>	<b>2.0</b>	<b>1.8</b>	<b>7.9</b>	<b>18.4</b>	<b>6.6</b>
<b>YUMA AXIS</b>	<b>18.4</b>	<b>15.9</b>	<b>15.3</b>	<b>33.3</b>	<b>45.2</b>	<b>45.4</b>	<b>53.7</b>	<b>41.3</b>	<b>53.0</b>	<b>48.0</b>
<b>TOTAL YUMA</b>	<b>6.7</b>	<b>5.9</b>	<b>5.5</b>	<b>11.7</b>	<b>16.2</b>	<b>16.7</b>	<b>19.3</b>	<b>19.2</b>	<b>30.1</b>	<b>20.6</b>

### 3. Cost Impacts

The GE MAPS analysis indicates that the Yuma import limit will be constraining from 336 hours in 2005 and zero hours in 2012. The cost of this constraint in 2005 is approximately \$500,000. See Table 17.

### 4. Emission Impacts

The emission impact on the Yuma area due to a potential relieving of transmission constraints and “moving” generation outside of the Yuma area was determined by GE MAPS similarly to the Phoenix analysis. Unlike Phoenix, however, Yuma County is a non-attainment area for PM<sub>10</sub> only. Impacts on power plant emissions in Yuma were estimated by using average emission rates of normal operation (such as starts-and-stops, short run times) of APS units along with the change in energy production. Emissions were also estimated for the other non-APS units. By entirely eliminating the import limits into Yuma, emissions produced by power plants located inside the Yuma load pocket would change as shown in Table 19.

Table 19  
YUMA POWER PLANT EMISSIONS (TONS)  
(Includes Yucca 1-4 and Yuma Axis)

	With Import Limits			Without Import Limits			Difference (With minus Without)		
	<u>2005</u>	<u>2008</u>	<u>2012</u>	<u>2005</u>	<u>2008</u>	<u>2012</u>	<u>2005</u>	<u>2008</u>	<u>2012</u>
<u>NOx</u>	37	19	19	17	19	19	20	0	0
<u>CO</u>	10	5	5	5	5	5	5	0	0
<u>PM<sub>10</sub></u>	2	2	2	1	2	2	1	0	0
<u>VOC</u>	2	0	0	0	0	0	1	0	0

## VII. CONCLUSIONS

### *Phoenix area Conclusions*

1. All Phoenix area transmission and local generation are necessary to reliably serve Phoenix area peak load in 2005 with the local generation reserve margin just exceeding the required reserve margin. In 2008, the local generation reserve margin significantly exceeds the required reserve margin. However, in 2012 the reserve margin is 346 MW which is 519 MW less than the required reserve margin of 865 MW. Although the reserve margin deficiency is not itself related to RMR, it is a load-serving issue that should be addressed. To mitigate this deficiency APS and SRP are presently evaluating both transmission alternatives to increase import capability and alternatives to increase Phoenix area generation.
2. During the summer, Phoenix area load is expected to exceed the available transmission import capability for approximately 680 hours in 2005, 340 hours in 2008, and 760 hours in 2012. These hours represent only approximately one percent of the annual energy requirements for the Phoenix area.
3. From a total Phoenix load, transmission, and resources viewpoint, import limits are expected to cause a minimal amount of local generation to be dispatched out of economic dispatch order in 2005 and 2012, and no impact in 2008.
4. The estimated annual economic cost of Phoenix area RMR generation is negligible, therefore advancement of transmission projects to increase import capability are presently not cost justified.
5. Removing the transmission constraint could reduce total Phoenix area air emissions by the following annual amount for 2005. There is a minimal impact for years 2008 and 2012 due to the increased import capabilities and resources resulting in fewer hours of operating local generation.

**Table C1**  
**Phoenix area Air Emissions Reduction**

Pollutant	Reduction <sup>1</sup> (tons/year)	Reduction of Phoenix Area Emissions (% of total emissions from all sources)
VOC	0.0	0.000
NO <sub>x</sub>	4.0	0.007
CO	1.0	0.000
PM <sub>10</sub>	0.0	0.000

<sup>1</sup>2005 results, impact for 2008 and 2012 is negligible

6. Removing the import restriction into the Phoenix area has no impact on local generation capacity factor. The capacity factor ranges from approximately 11% in 2005 to 26% in 2012.

#### ***Yuma Area Conclusions***

7. All existing Yuma area transmission and generation resources are necessary to reliably serve the Yuma area load.
8. The Yuma area load is expected to exceed the available transmission import capability for 714 hours in 2005, 676 hours in 2008 and 12 hours in 2012 although the amount of total load in the Yuma area is approximately 350-425 MW.
9. From a total Yuma load, transmission, and resources viewpoint, the import constraint could cause APS Yuma generation to be dispatched out of economic dispatch order for 336 hours in 2005, 2 hours in 2008, and 0 hours in 2012.
10. The estimated annual economic cost of Yuma area generation required to run out of economic dispatch order is relatively small, therefore advancement of transmission projects to increase import capability are presently not cost justified.
11. Removing the transmission constraint could reduce total Yuma area air emissions by the following annual amount for 2005. There is a minimal impact for years 2008 and 2012 due to the increased import capabilities resulting in fewer hours of operating local generation.

**Table C2**  
**Yuma Area Air Emissions Reduction**

<b>Pollutant</b>	<b>Reduction<sup>1</sup> (tons/year)</b>	<b>Reduction of Yuma Area Emissions (% of total emissions from all sources)</b>
VOC	1.0	Unavailable
NO <sub>x</sub>	20	Unavailable
CO	5	Unavailable
PM <sub>10</sub>	1.0	0.001

<sup>1</sup>2005 results, impact for 2008 and 2012 is negligible

12. Removing the import restriction into the Yuma area could reduce the APS Yuma generation capacity factor from 1.6 percent to 1.2 percent in 2005.

## **Appendix A**

### **Regional Production Cost Modeling Assumptions**

**Regional Production Cost Modeling Assumptions**

Regional load forecasts were based on the WECC's Estimated Loads and Resources report dated April, 2003.

Hydro modeling assumed average hydro conditions.

Generation additions were based on the WECC's Estimated Loads and Resources report dated April, 2003. The following amounts of new generation were added in the Arizona-New Mexico-Southern Nevada region:

2003-2005 8,800 MW

2006-2008 2,100 MW

2009-2012 600 MW

Generation retirements included Mohave 1&2 in 2006 in the AZ-NM-S Nev subregion, and a few more in the California subregion.

Generation Units Operational Characteristics (Average Values – AZ-NM-S Nev)

Fuel Type	Technology	Size MW	Install Date	Heat Rate Btu/kWh	VOM \$/MWH	EFOR %
Gas/Oil	Steam			12,000	2.0	6%
Gas	SC	<100	Pre 2000	14,000	4.1	10%
Gas	SC	>100	Post 2000	10,500	4.1	5%
Gas	CC	<100	Pre 2000	8,700	2.0	5%
Gas	CC	500	Post 2000	7,000	3.0	5%
Coal	Steam	<500		11,200	1.4	7%
Coal	Steam	>500		10,000	1.4	9%

Natural gas price forecast was based on the average of several industry forecasts, delivered to Arizona.

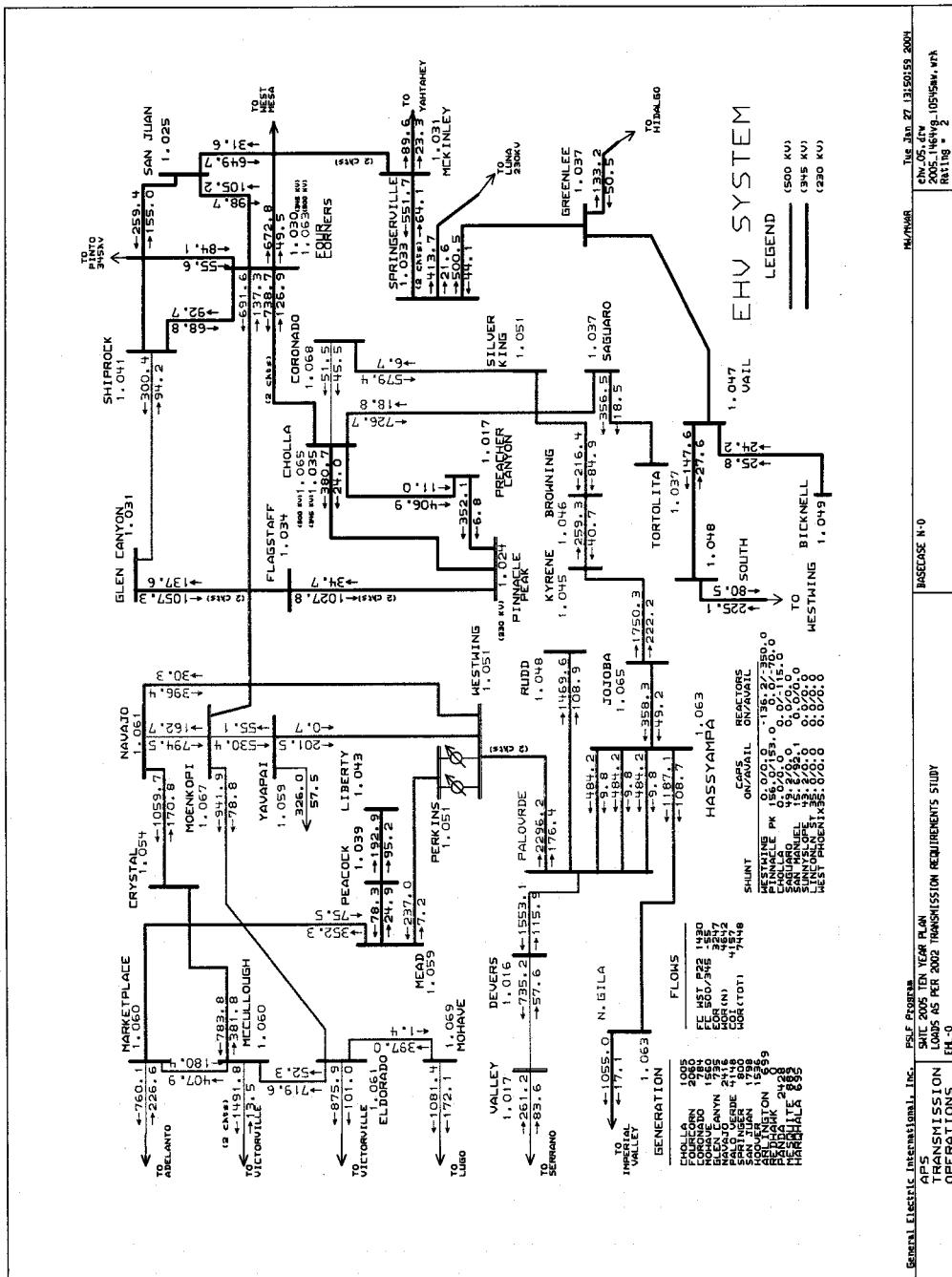
2005 – 4.73 \$/MMBtu

2008 – 4.35 \$/MMBtu

2012 – 4.93 \$/MMBtu

## **Powerflow Output Results**

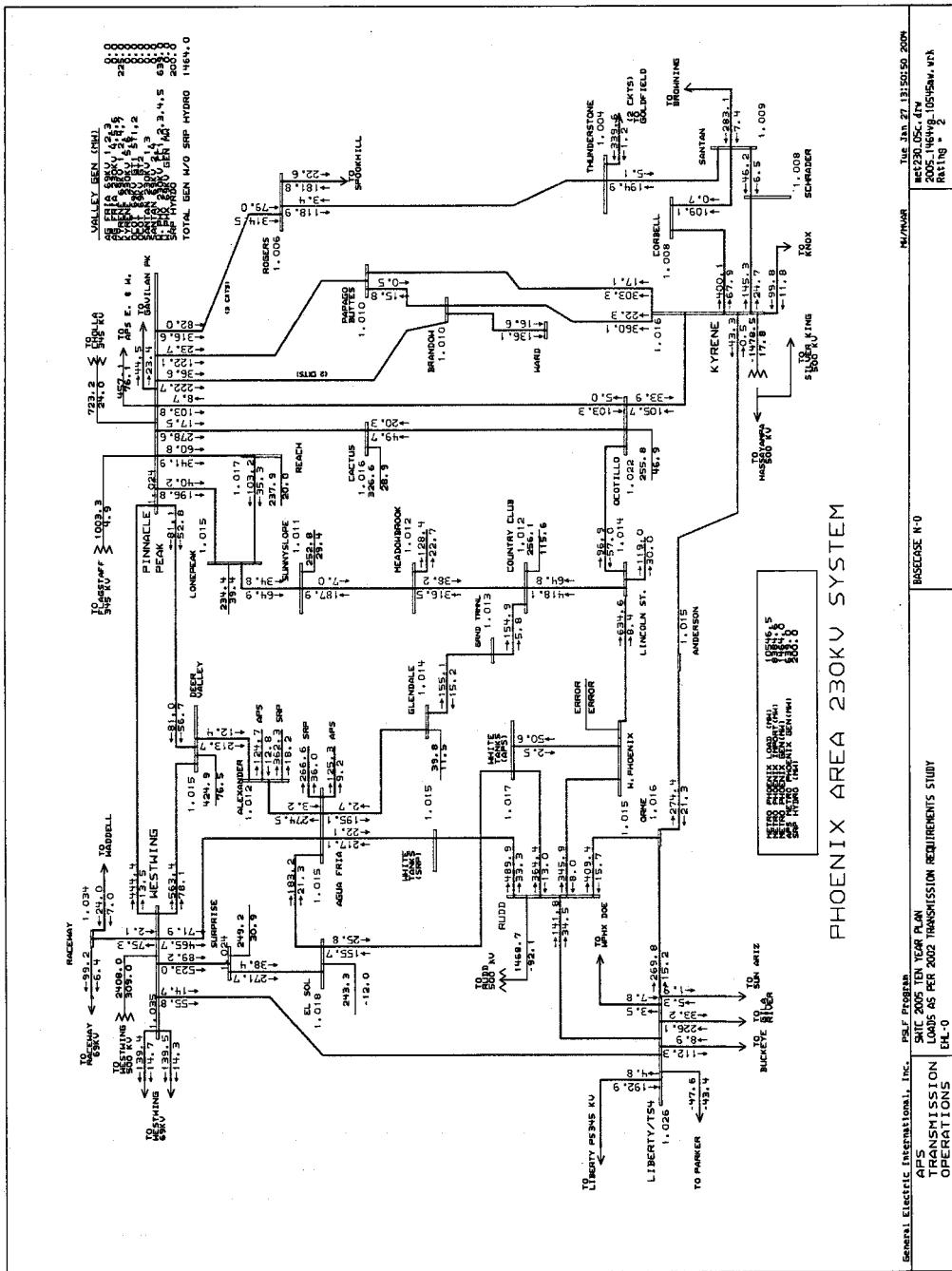
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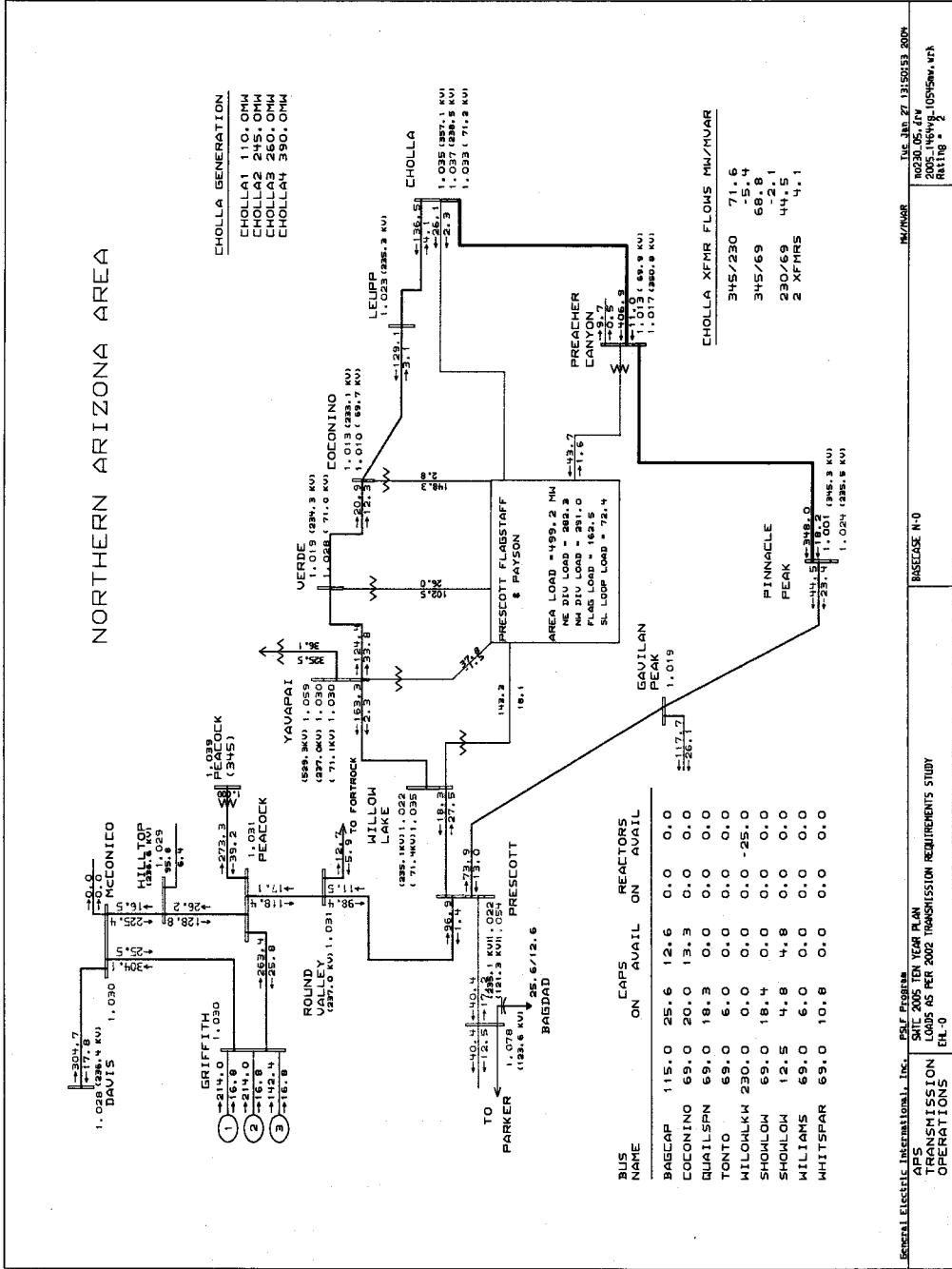


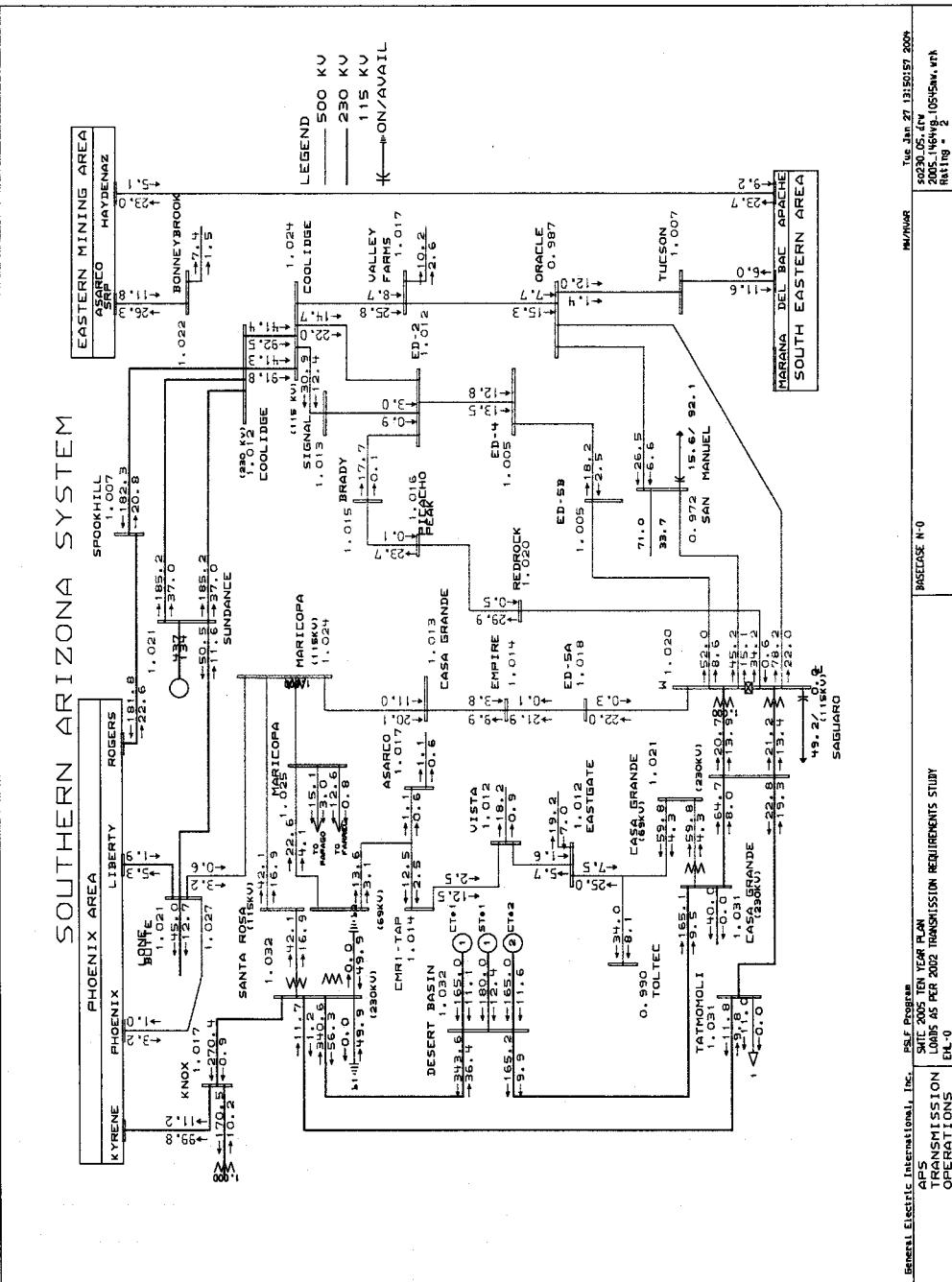
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LOADS AS PER 2002 TRANSMISSION REQUIREMENTS STUDY  
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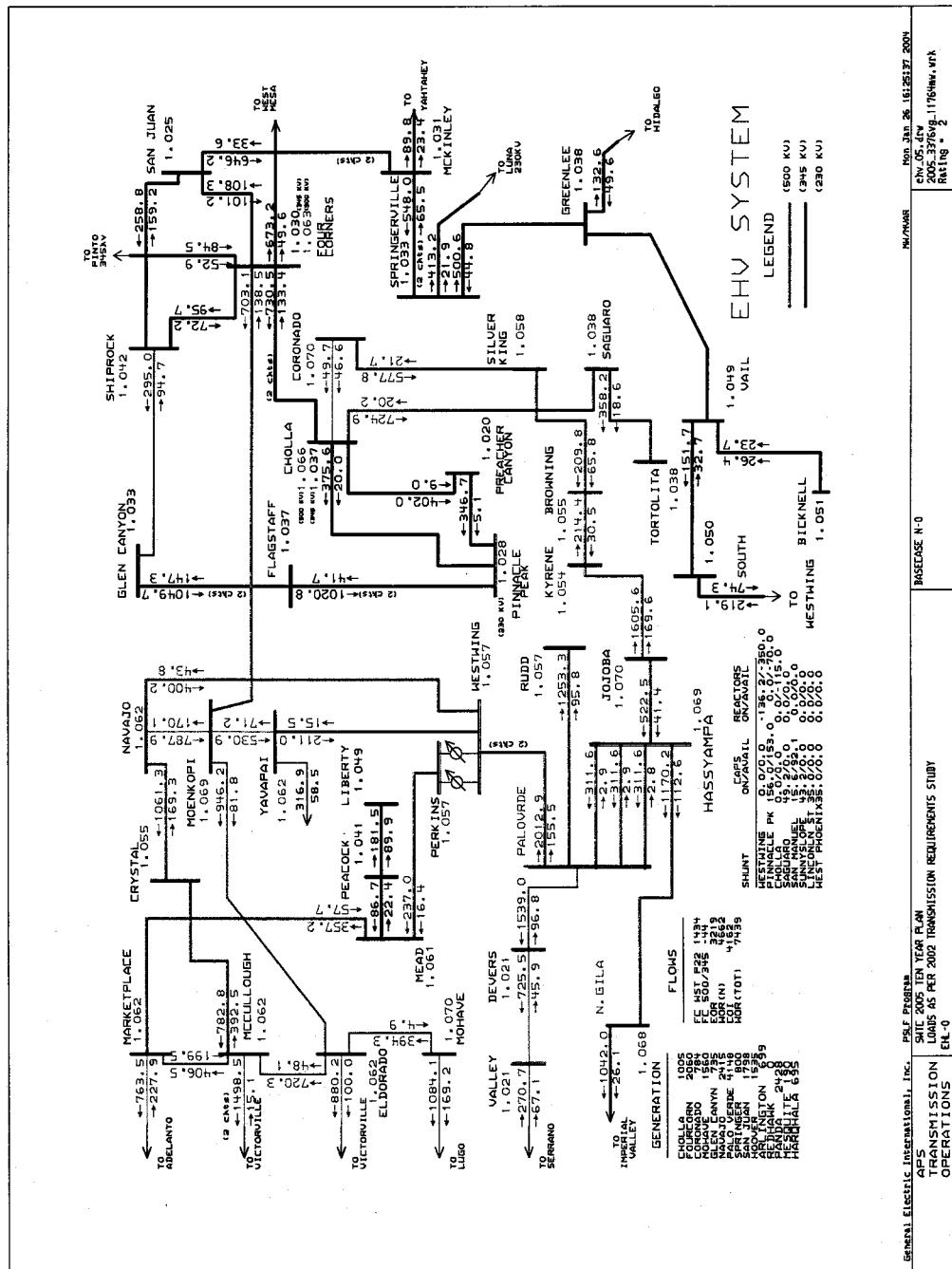
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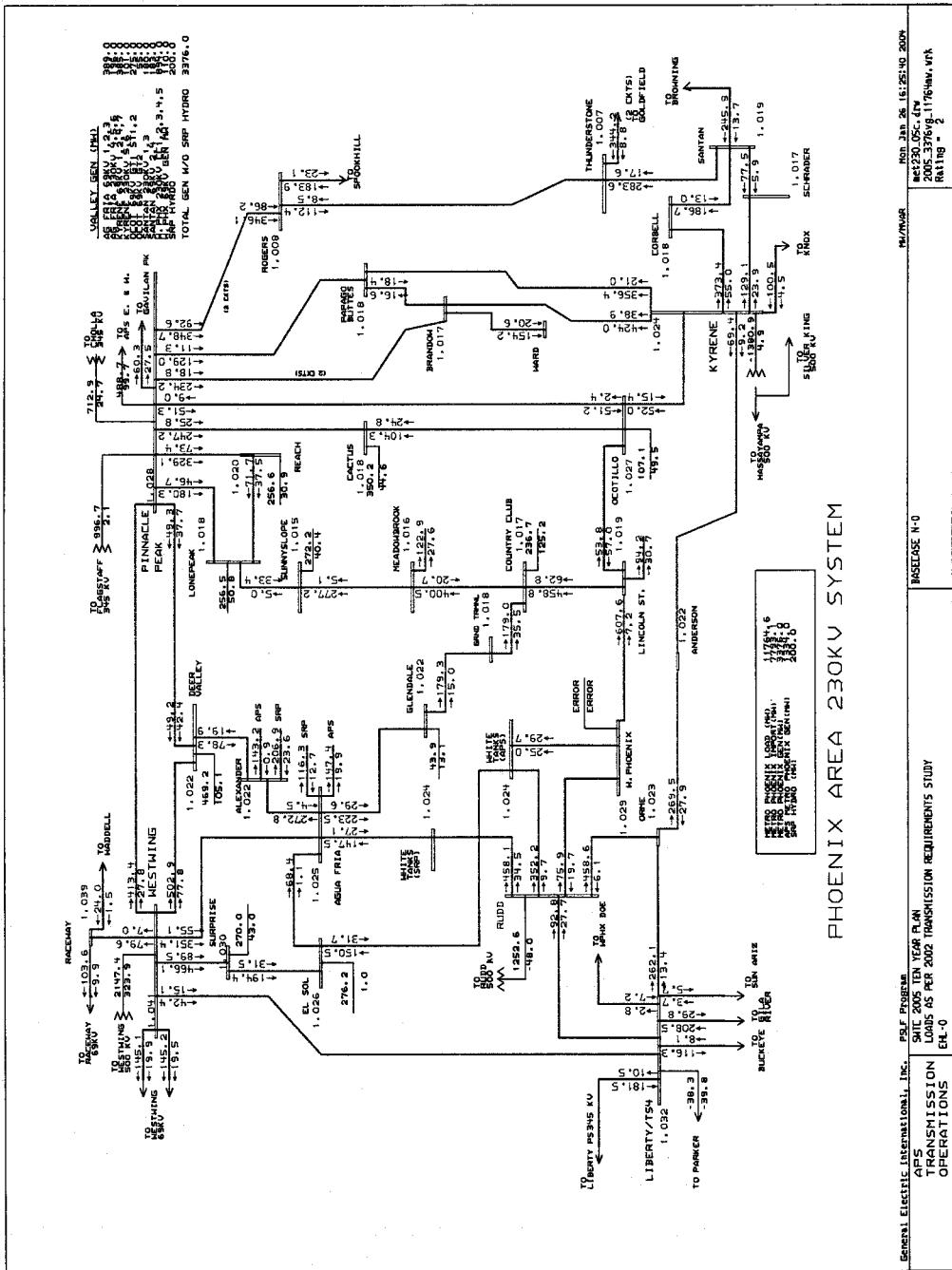
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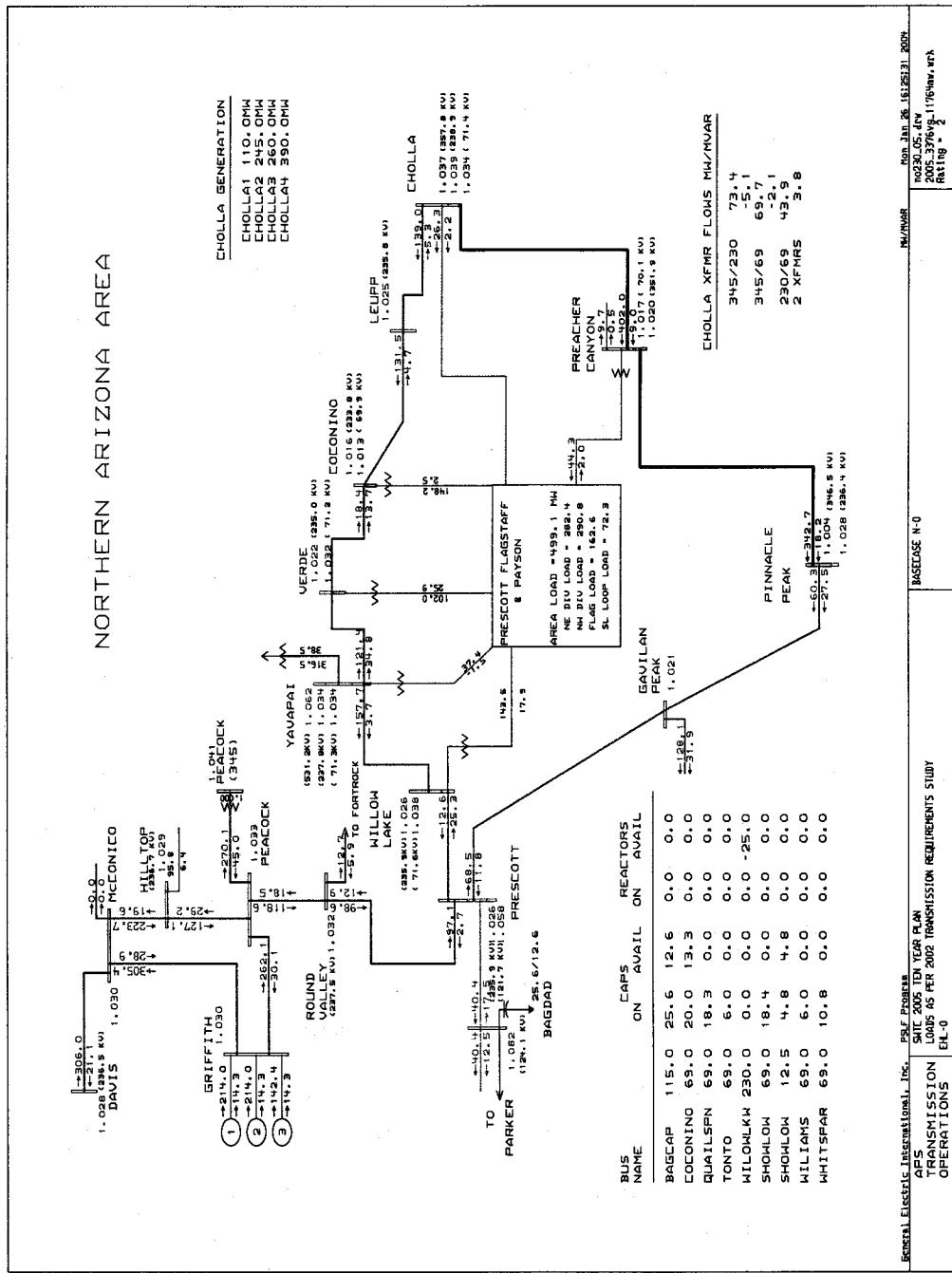












General Electric International, Inc. PSF Processor.  
APS 2005 TEN YEAR PLAN  
TRANSMISSION LOADS AS PER 2002 TRANSMISSION REQUIREMENTS STUDY  
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CHOLLA 3 26.0, OHW  
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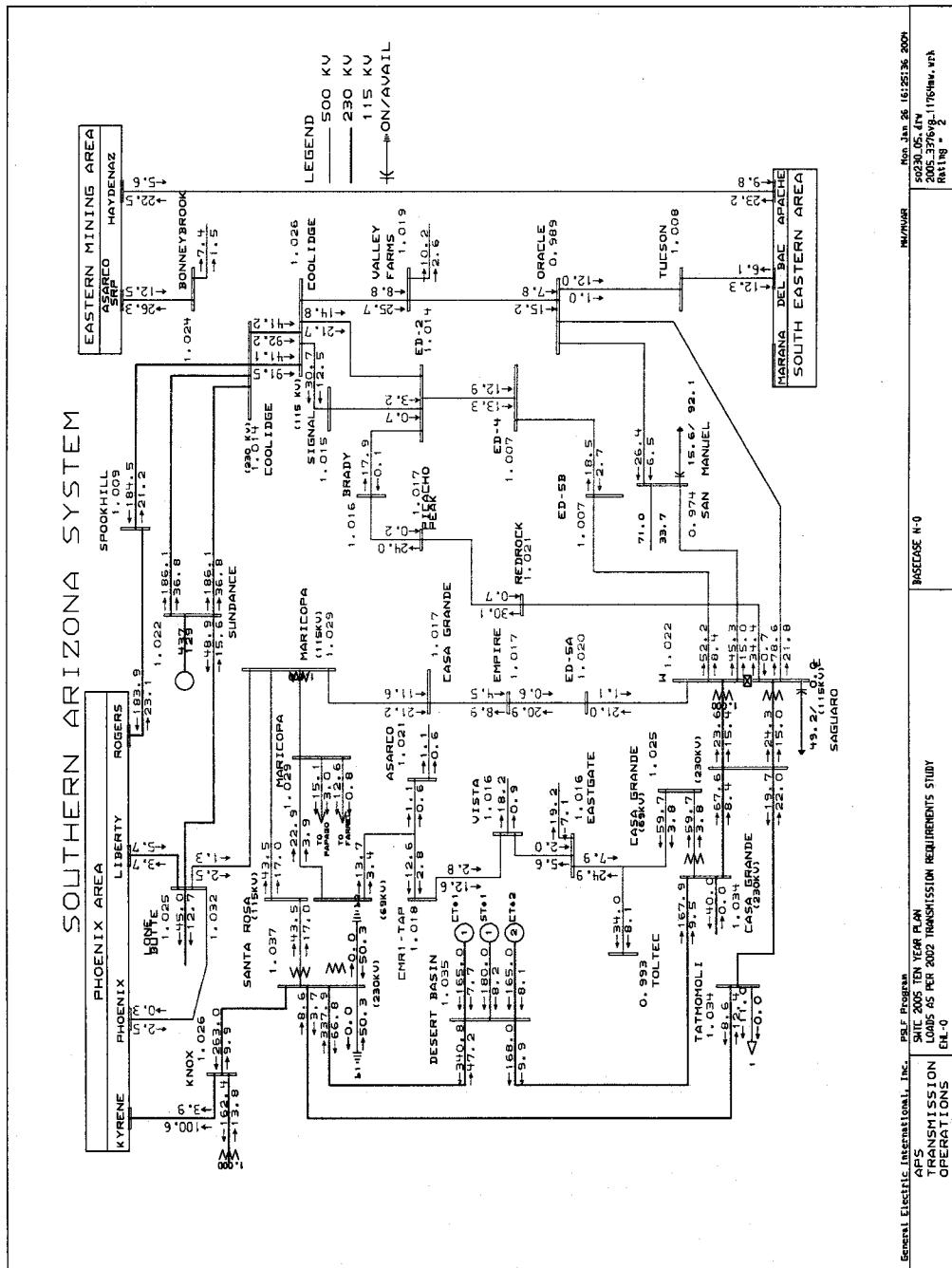
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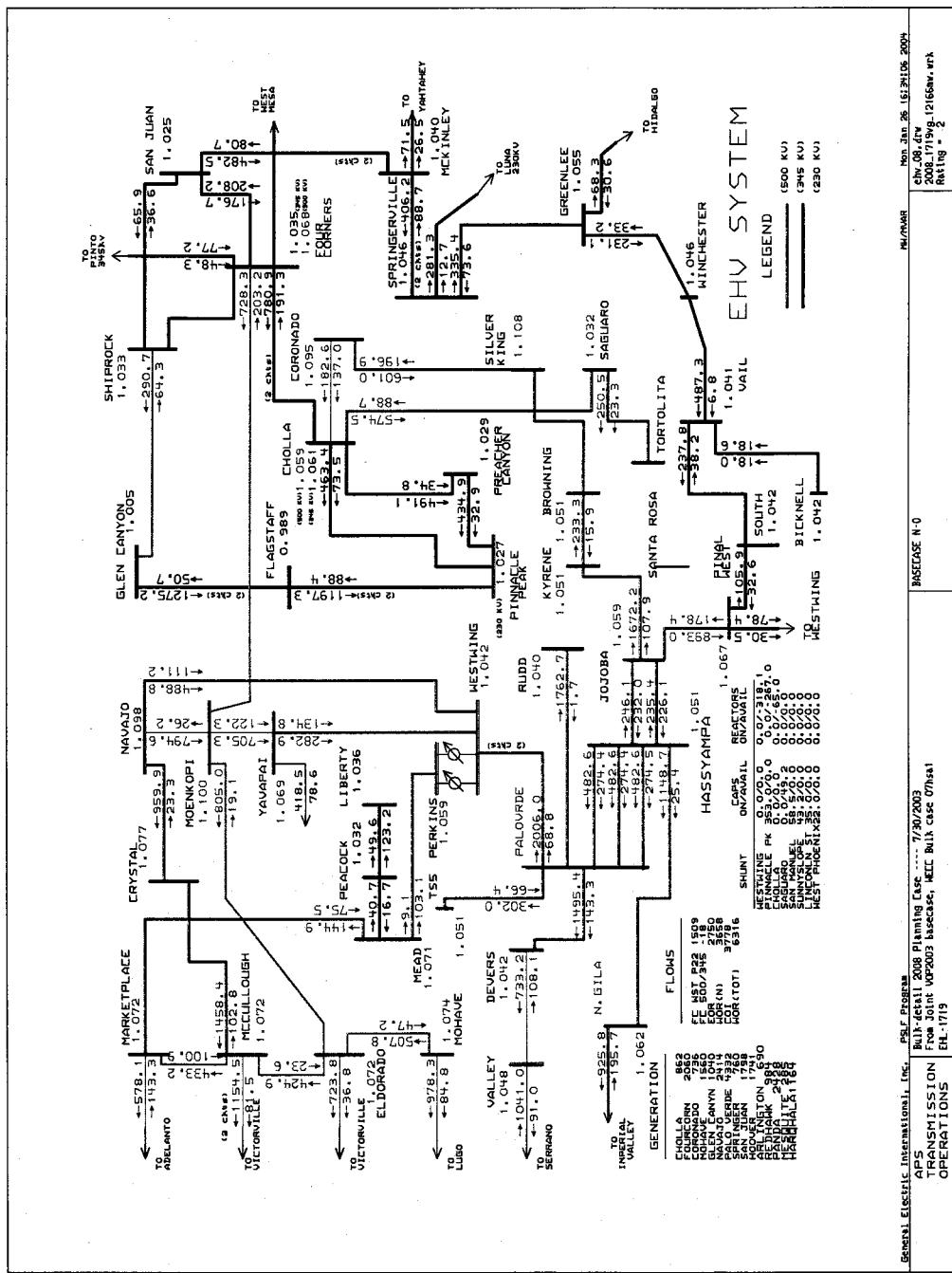
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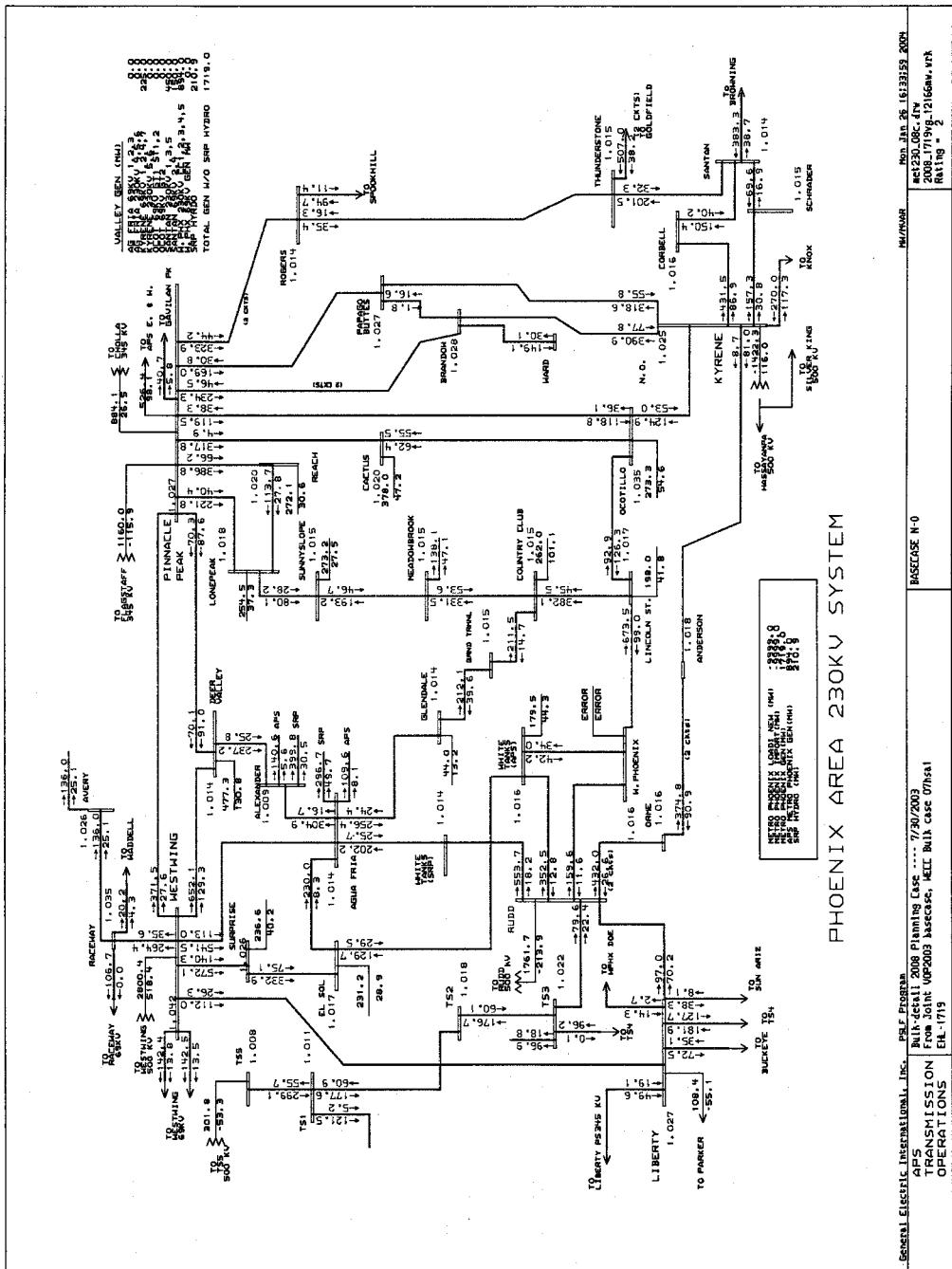
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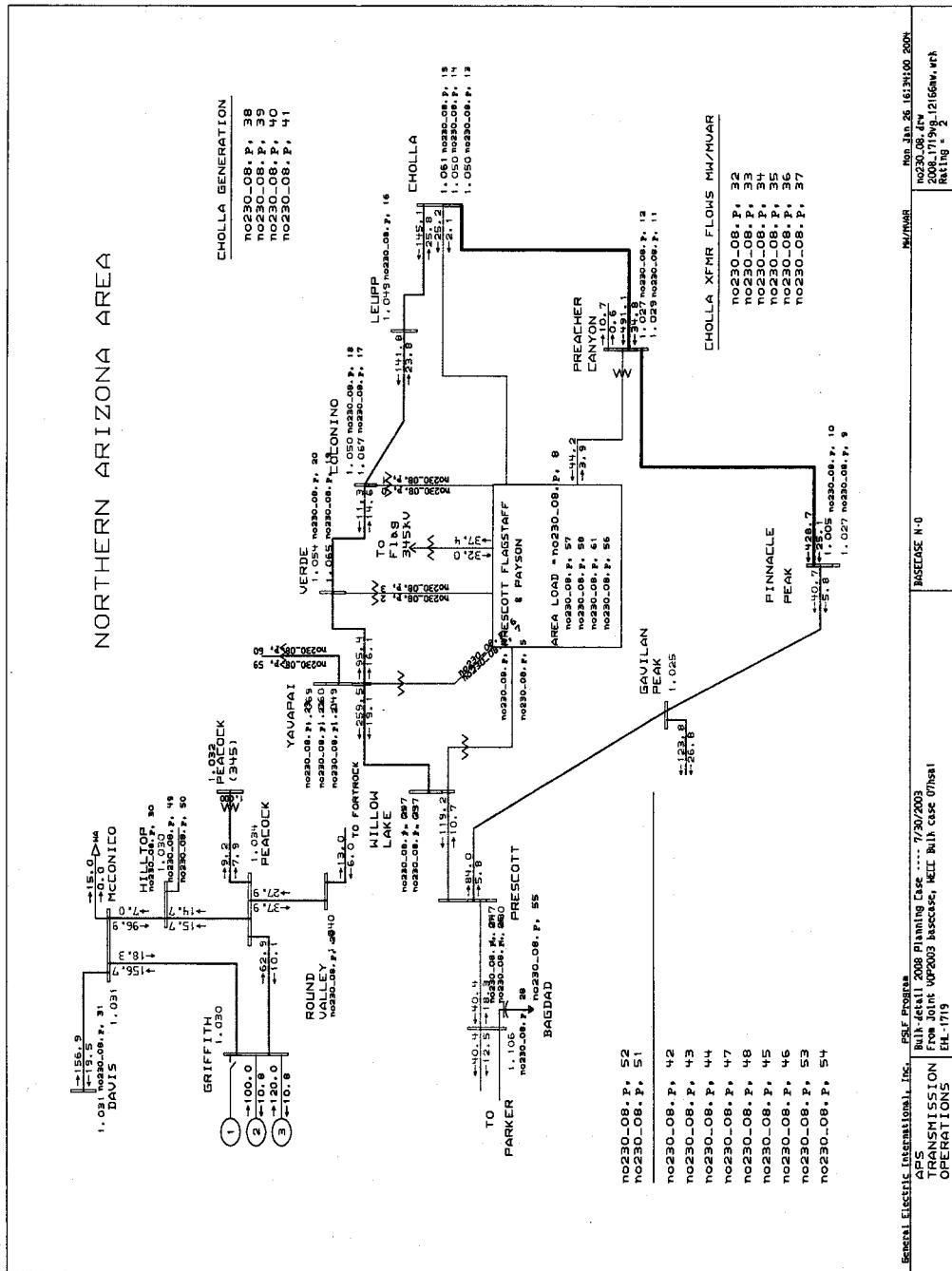
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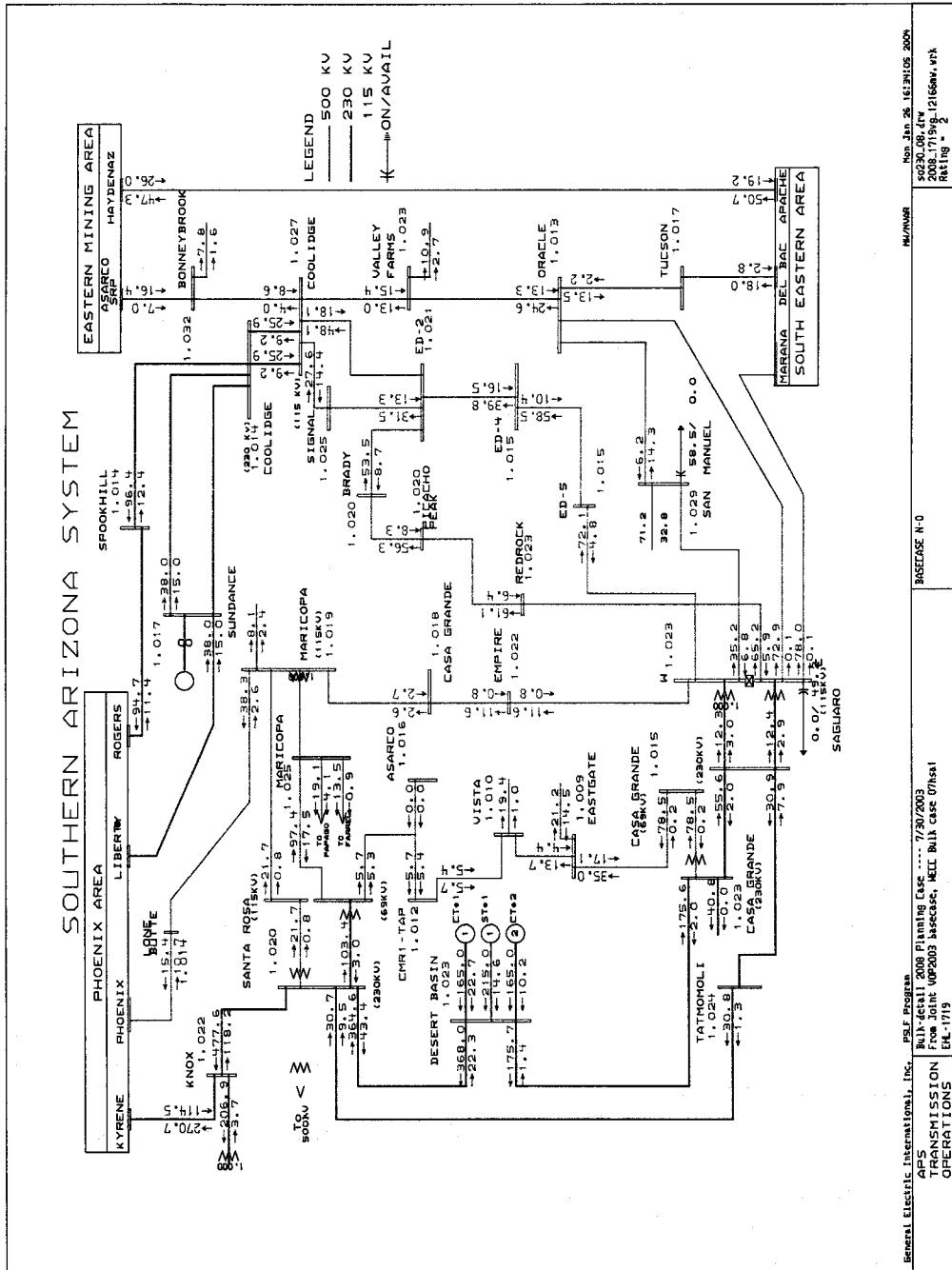
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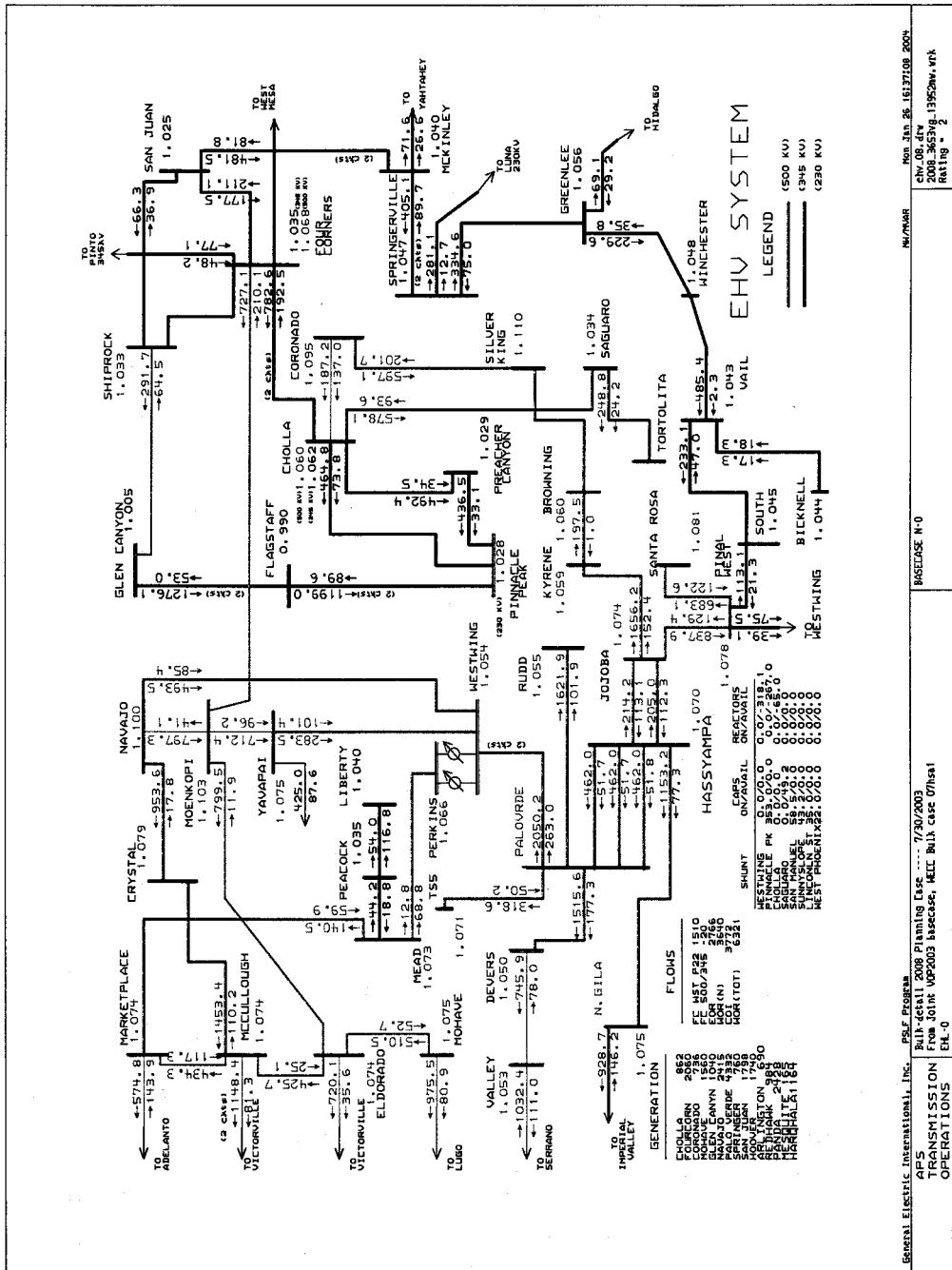


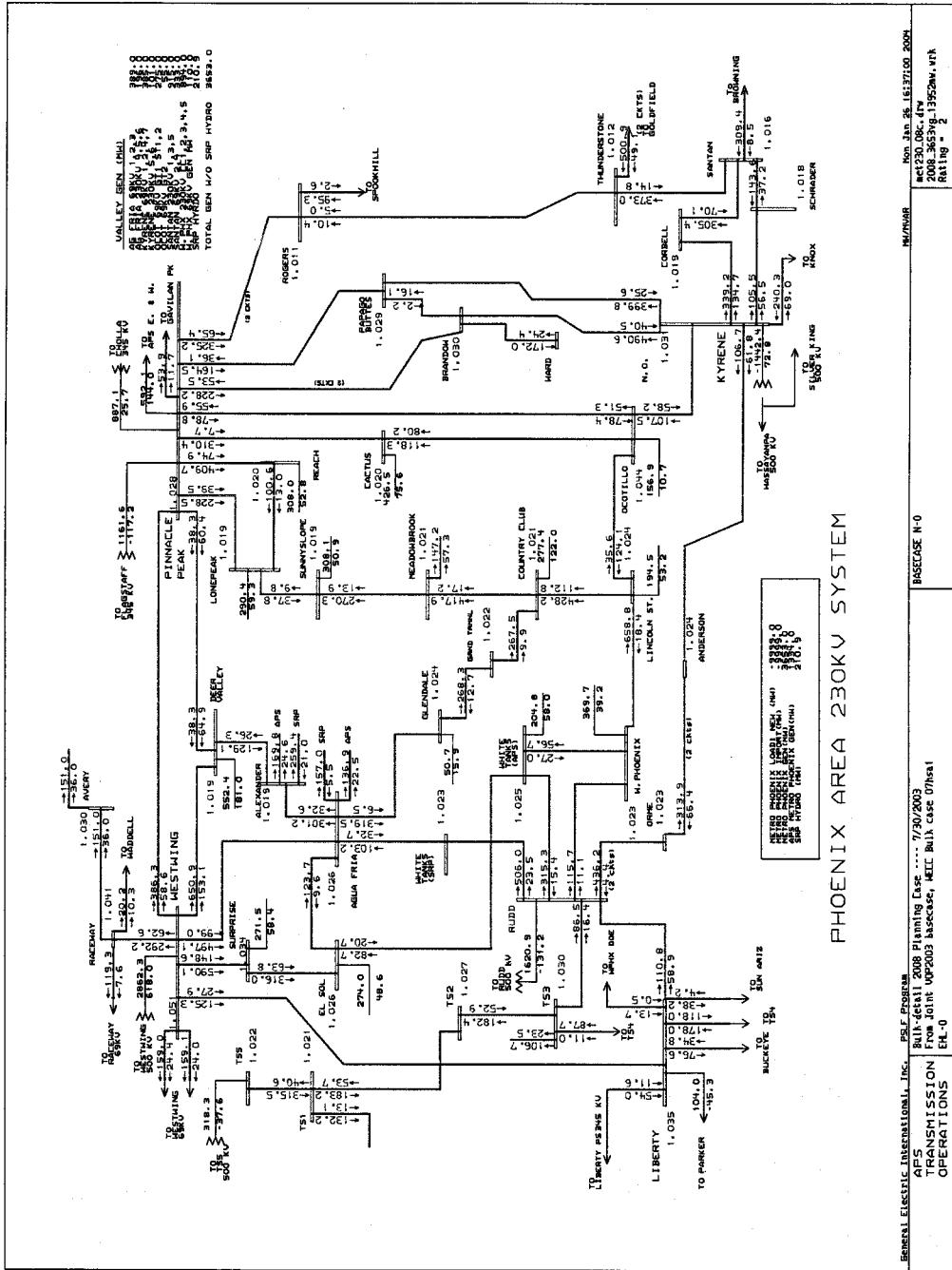


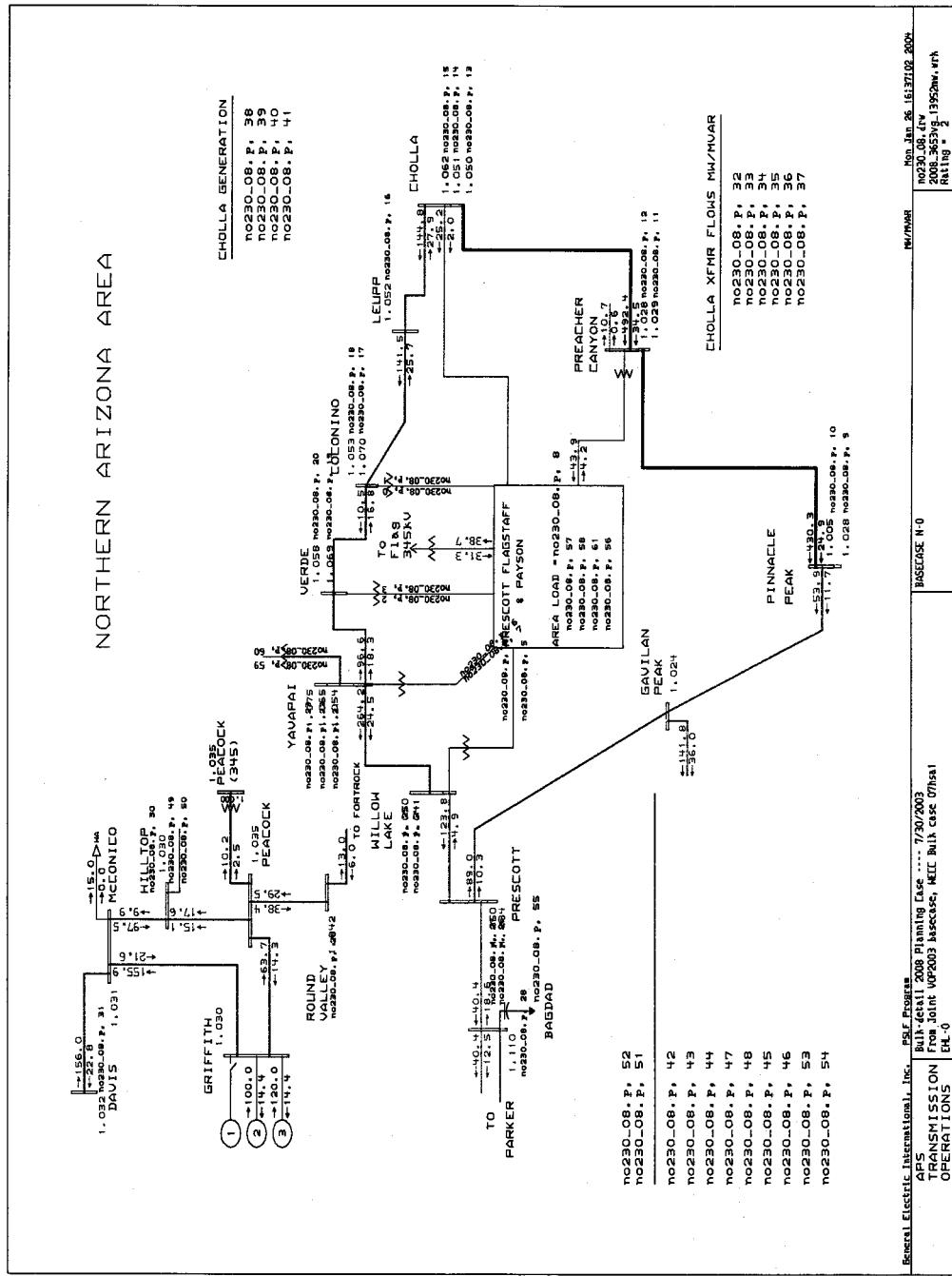


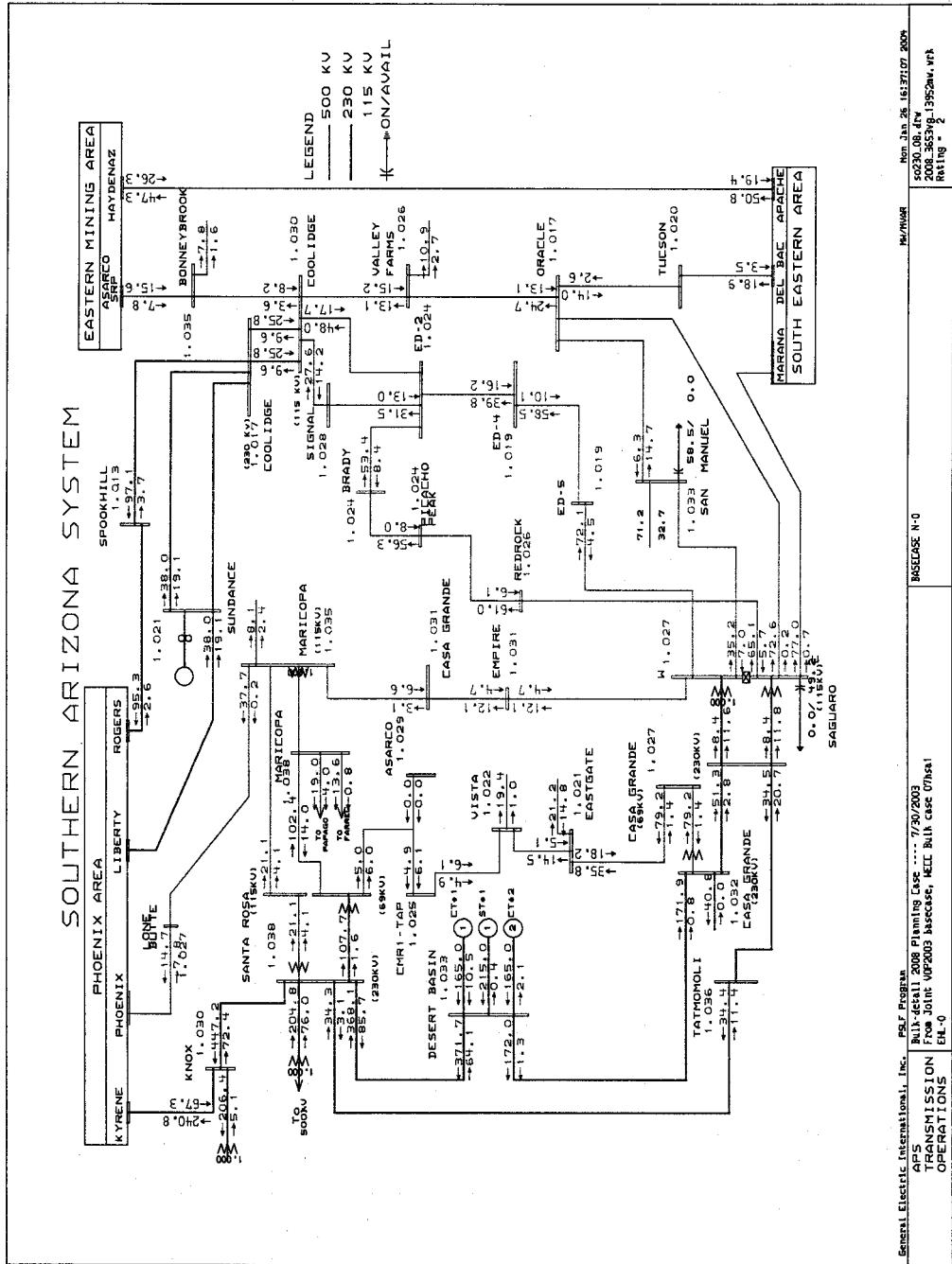


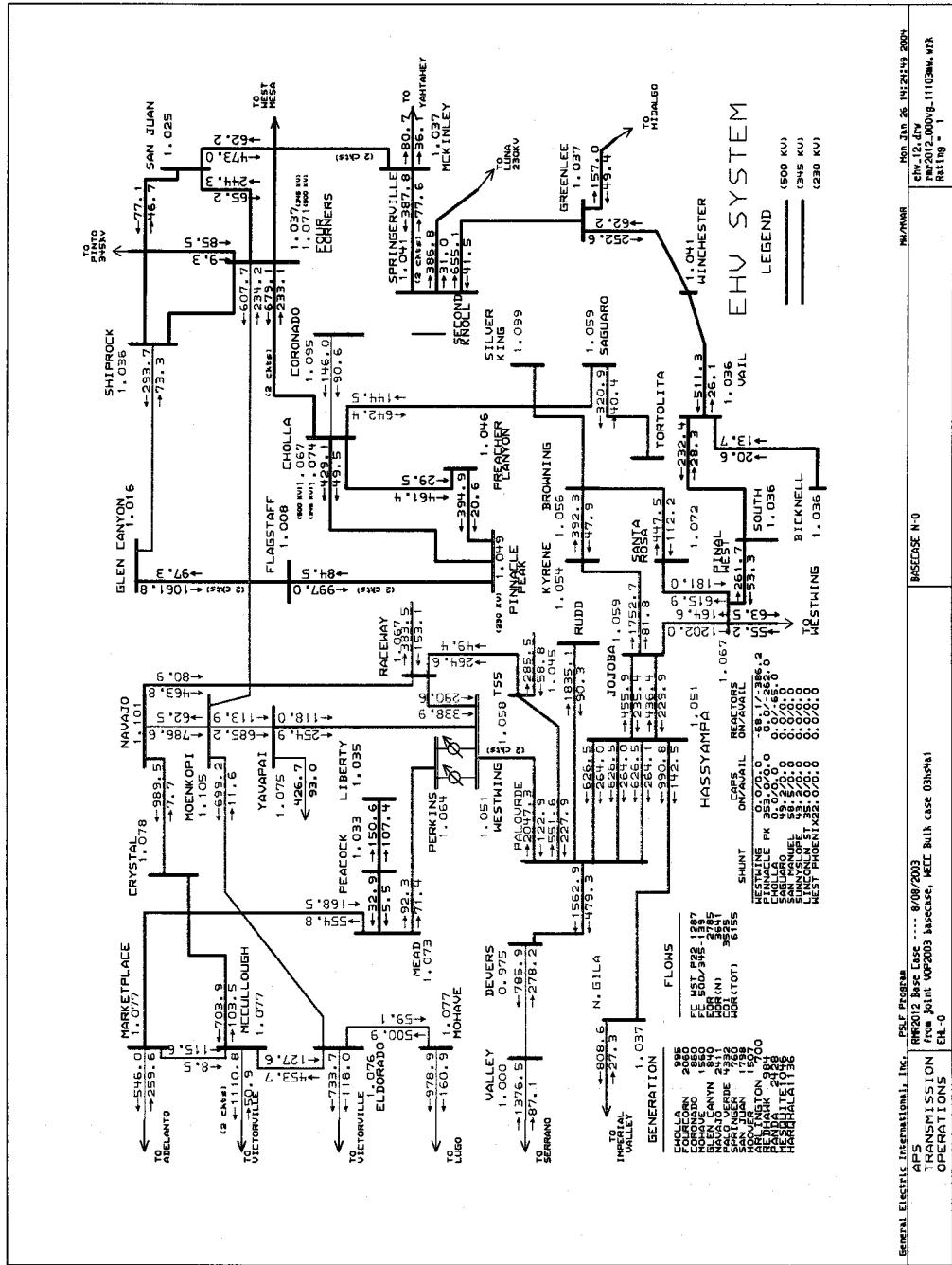






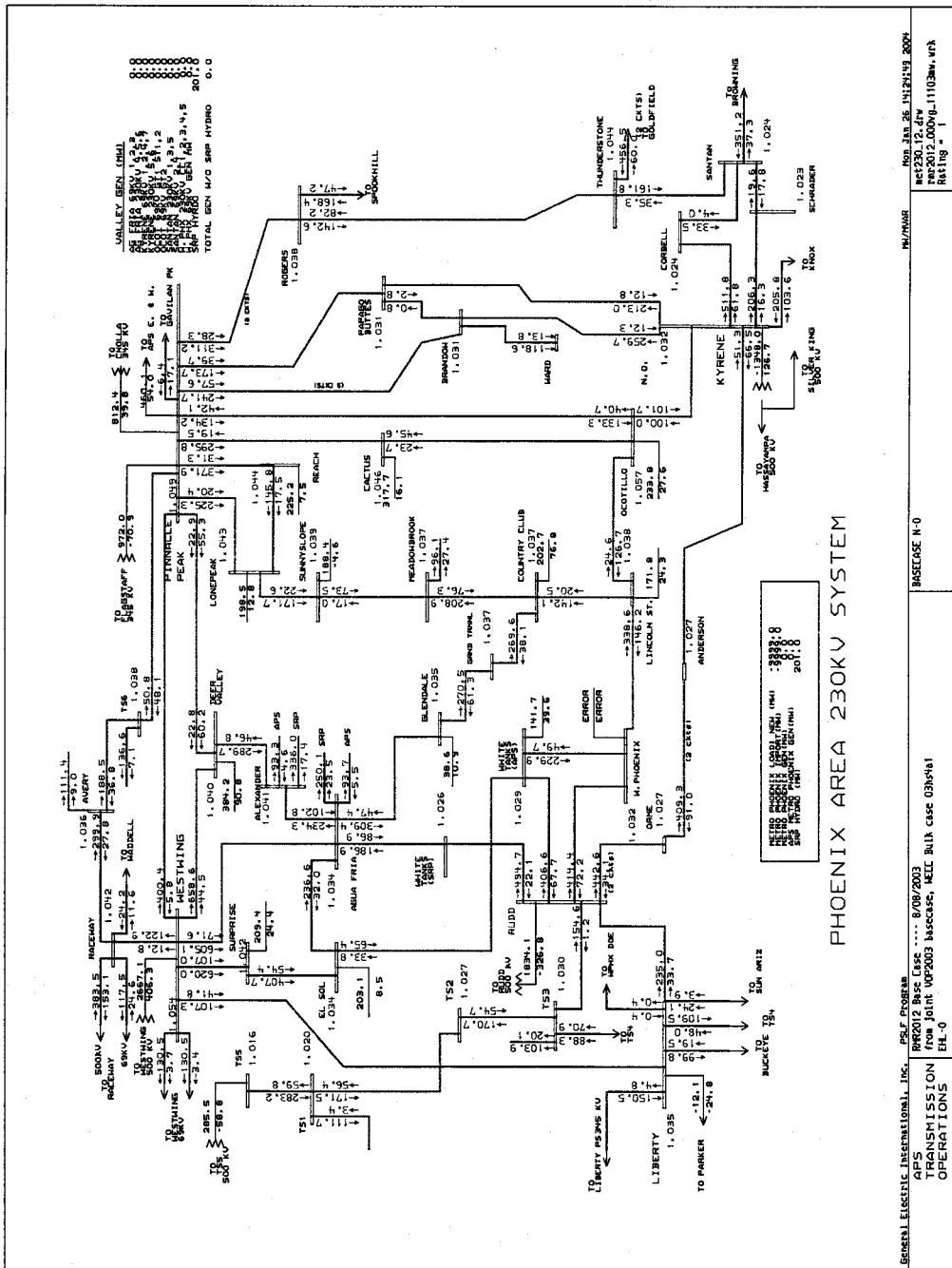


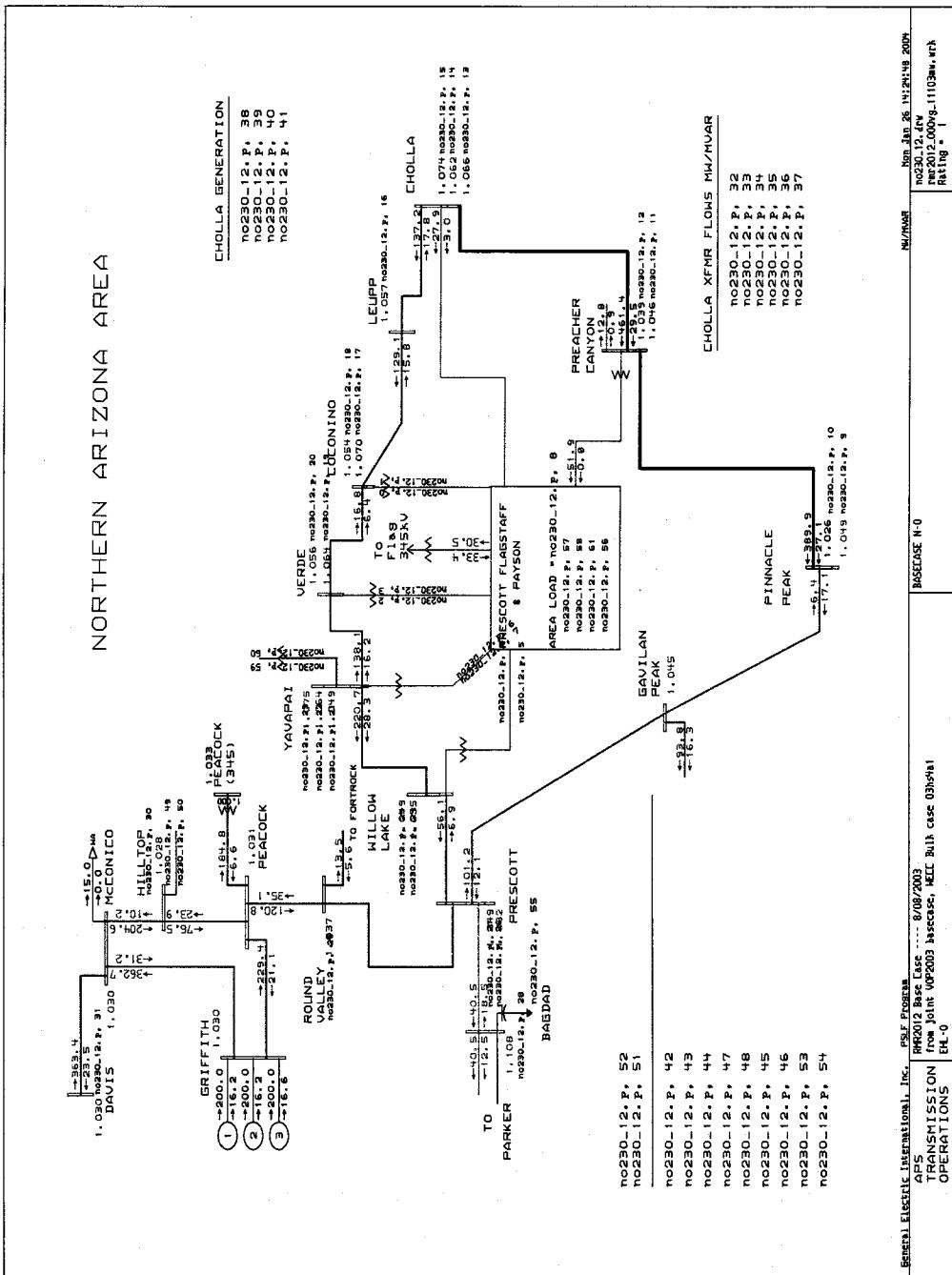


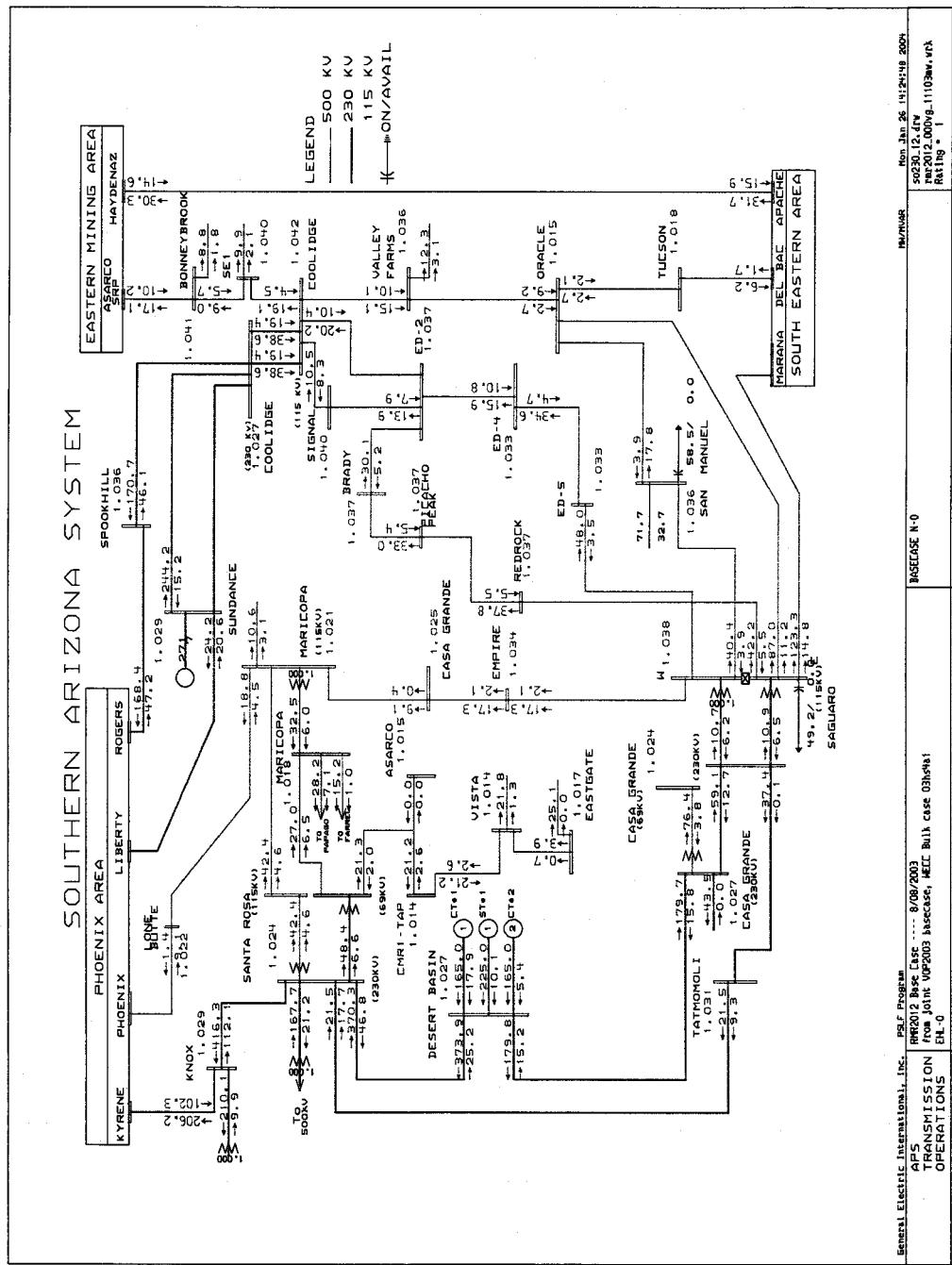


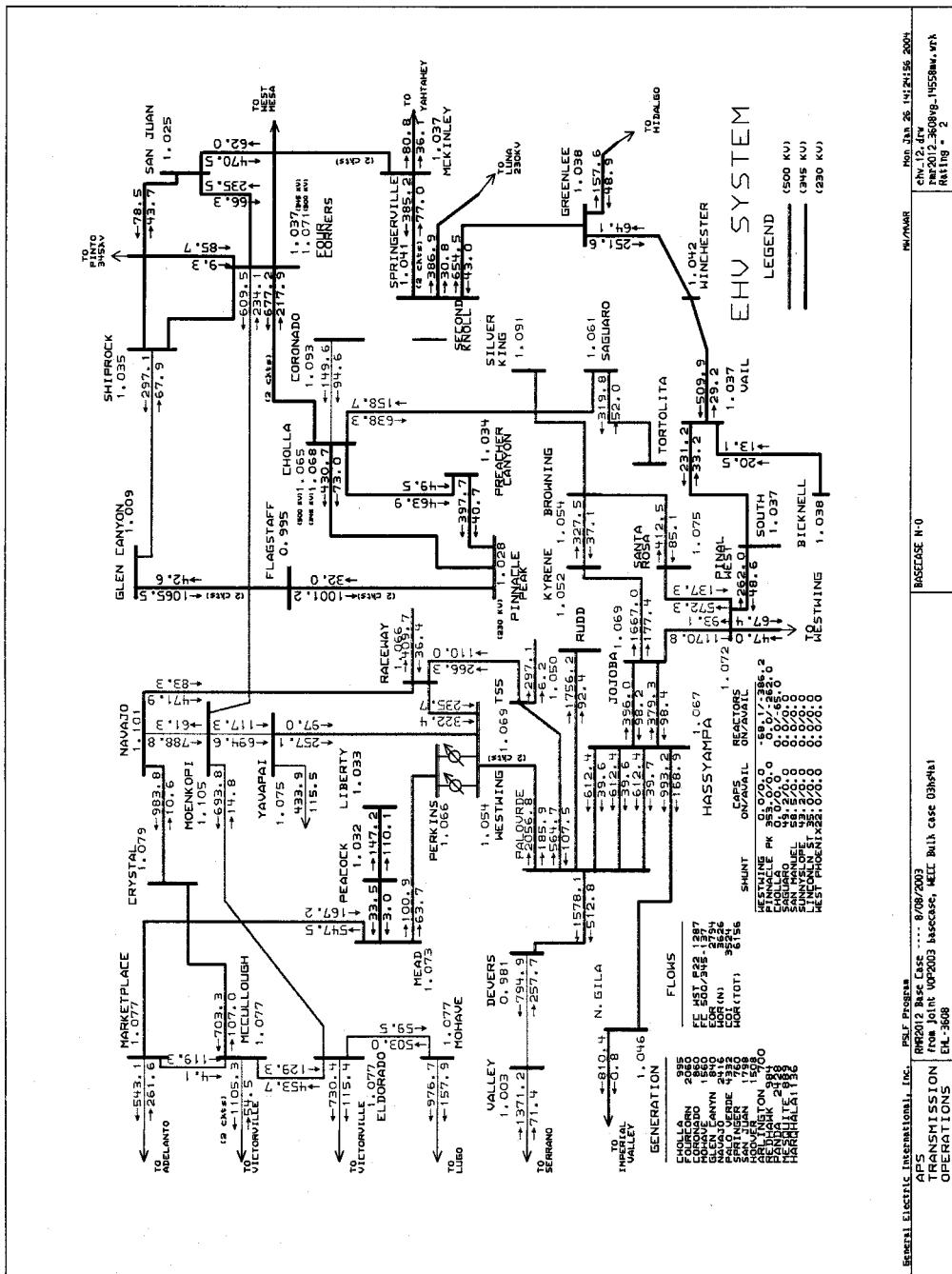
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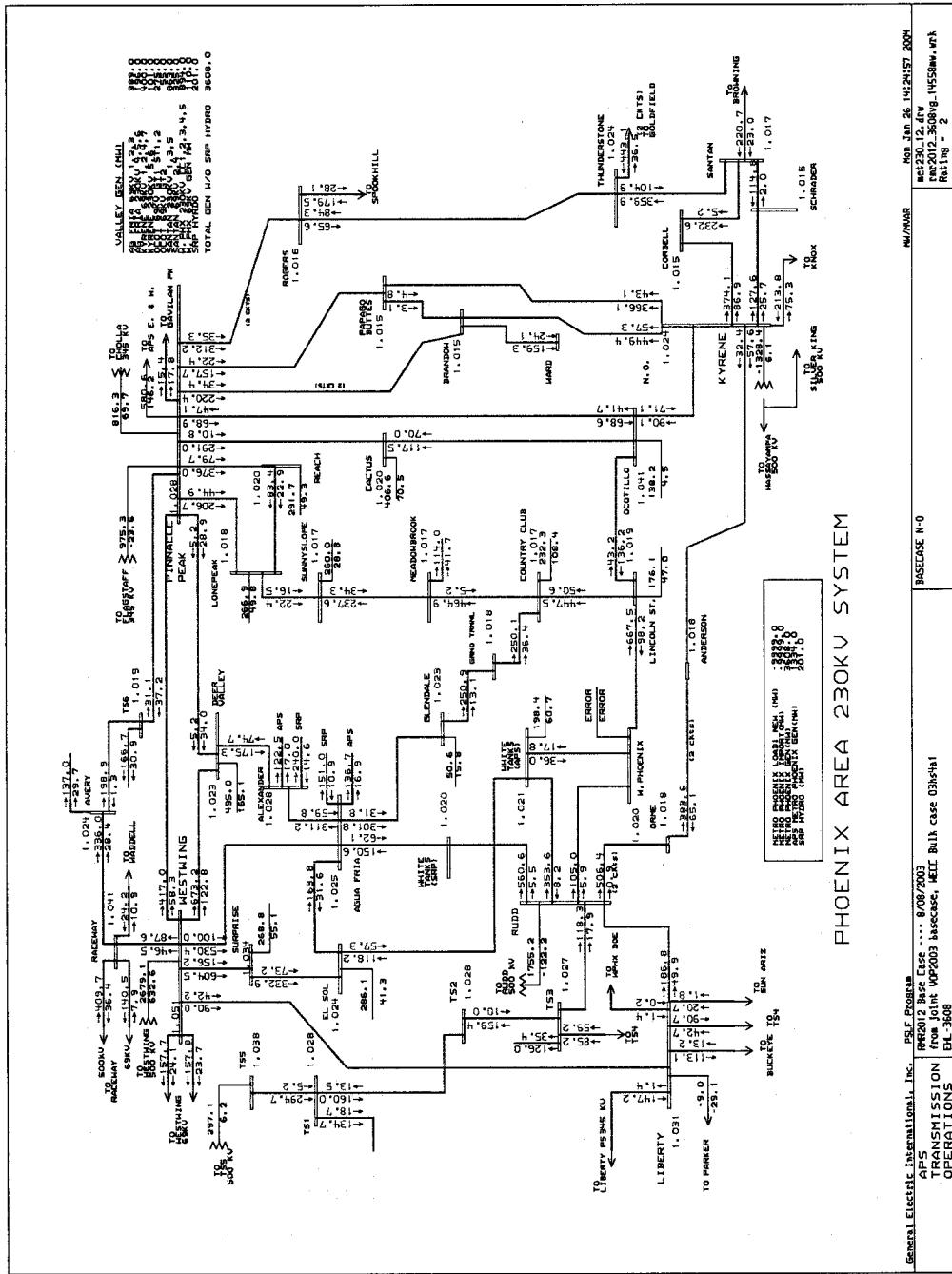
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